NUCLEAR WEAPON EFFECT RESEARCH AT PSR—1983. Acute Radiation Effects on Individual Crewmember Performance

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SECURITY CLASSIFICATION OF THIS PAGE

- SUBJECT TERMS (Continued).
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between dose/time and the task performance estimates provided by supervisors of combat crews.

We focus on soldiers representing four different crews, from the artillery (both gun and fire direction center crews), armor, and antiarmor, because their operations include the prospect of decisive encounters where one of the combatant crews will probably be put out of action. The crews are small, with three or four members, and the encounters are usually brief, typically lasting between 30 and 90 sec. so crew missions, operational scenarios, and crewmembers' tasks can be readily modeled.

Performance data from questionnaires administered to 161 senior noncommissioned officers from the combat crews were evaluated. Twenty-four respondents were excluded because of either lack of experience, background, self-disqualification, or missing questionnaires. Another 21 were rejected because of noncompliance with instructions or unreasonable response patterns, leaving a total of 116, or 73 percent.

A linear regression analysis is performed on respondent data to obtain the parameters for predicting performance of each of the 15 crewmember positions. The logit form is used to model the response data, so as to guarantee that all predicted performance values, including the upper and lower confidence limits, lie within the interval (0, 1), as consistent with the dependent variable (performance) input data.

Performance predictions are mapped onto the dose/time plane with specified boundary conditions by applying numerical techniques to a framework of symptom complexes. Three-dimensional representations of performance as a function of dose and time are developed for 15 crewmember positions by applying a "french curve" algorithm to translate performance data input on a grid of 18 dose by 39 time points into a smooth surface. A similar numerical procedure was used to generate isoperformance contour plots that are 10 percent incremental coplanar projections of the performance surface onto the dose/time plane.

Computed performance, given in both graphic and tabular form, is consistent with the acute symptomatology from medical observations. Also, despite the subjective basis of the performance estimates correlated with dose and time, the computed results represent reasonable expectations. Physically demanding tasks are associated with greater performance degradation; crewmembers with similar tasks across crews indicate correlated degradation when grouped. Since we find it difficult to stipulate a sound comprehensive measure of uncertainty in the results we present, the results should be applied with caution.

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SUMMARY

In this report, quantitative estimates of the performance levels of individual combat crewmembers exposed to prompt ionizing radiation are developed. The data described here are designed to help plan military field operations and training for combat crews in a nuclear weapon environment. The estimates of crewmember performance are expressed graphically and tabulated in terms of two critical values: radiation dose (free-in-air), and time following exposure. Performance estimates are provided for each of the 15 different types of crewmembers selected to represent typical short-term (from 0.5 to 1.5 min) battlefield engagement scenarios for a small combat crew (three to four members). The crewmembers selected for study are from the following four groups: (1) field artillery gun crews, (2) field artillery fire direction center (FDC) crews, (3) tank crews, and (4) antitank guided missile (improved TOW vehicle) crews.

The quantitative estimates of degraded performance are based on two bodies of information developed for the Intermediate Dose Program (IDP). The first comes from the comprehensive symptomatology review of human irradiation experience, and the second comes from the U.S. Army combat crew questionnaires. Symptom descriptions quantified in terms of five levels of severity, and the formation of symptom complexes based on the symptomatology investigation, made it possible to obtain performance judgments from the questionnaires administered to army personnel.

Performance data, derived from the army crew supervisors who were asked to judge how typical crewmembers might be able to perform if they had acute radiation symptoms described to them, are correlated with dose and time. Questionnaire responses are evaluated to improve the quality of the data base used for the regression analyses to develop smoothed, expanded, and consistent performance input data used for mapping the dose-time domain provided by a framework of symptom complexes.

Numerical procedures are applied in order to map and generate the three-dimensional performance surfaces and contour plots as a function of dose and time. Since data available from the symptomatology

investigations are not sufficient to allow uncertainties to be succinctly specified, and the performance levels are developed for particular types of combat crewmembers and scenarios, application of the results obtained is recommended with caution.

PREFACE

This report was prepared as one volume of a set comprising the Pacific-Sierra Research Corporation (PSR) final report for the Defense Nuclear Agency (DNA) under contract DNA001-83-C-0015. The work done under this contract spans a wide range of nuclear weapon effects research covering intermediate-dose radiation, cratering, fire research, analytical models, underground testing, instrumentation, and microwave energy.

This volume reports on material provided for the DNA Intermediate Dose Program (IDP) to assess the effects of nuclear weapon radiation on military troop performance. It also represents one of a series of volumes comprising the DNA IDP report.

Quantitative estimates of combat troop performance are developed, using information and data from other IDP investigations. Along with the IDP Core Group, DNA staff members David L. Auton and Robert W. Young of Science and Technology, Biomedical Effects (STBE) guided this effort. The authors acknowledge the valuable assistance provided by G. Hall, who performed the statistical data analysis and authored Appendix F, "Performance Data Regression Modeling"; and Elizabeth M. Niccum for providing special computer programming assistance in analyzing the questionnaires.

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SECTION 1

INTRODUCTION

This report describes the development of dose/time performance profiles for individual crewmembers exposed to the initial prompt ionizing radiation from a nuclear weapon burst. The individual performance profiles are an integral part of the Defense Nuclear Agency (DNA) Intermediate Dose Program (IDP), whose objective is to estimate the effect of prompt radiation on the battlefield performance of combat crews and units.

Crewmembers representing four different crews were specifically selected for study, because their operations include the prospect of decisive encounters with the enemy. The term "decisive" means that one of the combatant crews will probably be put out of action as a consequence of the encounter. The crews are small, with three or four members, and the encounters are usually brief, typically lasting between 30 and 90 sec. Accordingly, the crew missions, operational scenarios, and members' tasks can be readily modeled. The four crews studied were

- A field artillery gun crew (155 mm self-propelled howitzer).
- A field artillery fire-direction-center (FDC) crew (on manual operation).
- A tank crew (M60A3).
- An antitank guided missile crew in an improved TOW vehicle
 (ITV).*

The procedural methodology for developing the dose/time individual performance relationships follows from preceding efforts involving IDP program objectives and investigation strategy [Intermediate Dose Program Group, 1983]; a comprehensive review and assessment of acute radiation effects and symptomatology in humans [Baum et al., 1983]; the description and quantification of radiation sickness in terms of five

^{*} Hereafter referred to as simply the TOW crew.

levels of severity, and the aggregation of symptom groups into symptom complexes [Anno and Wilson, 1983]; and the gathering of judgment data on military task performance from questionnaires administered to U.S. Army combat crew personnel [Glickman et al., 1983].

The descriptions of the symptom complexes were used on questionnaires administered to senior noncommissioned officers (NCO) to obtain
their estimates on the performance of individual crewmembers. Evaluation of the questionnaire responses is described in Sec. 2. Based on
that evaluation, some respondents were excluded as unqualified because
they did not meet criteria to ensure that the estimates collected were
made by senior NCOs who had recent experience supervising typical crewmembers on current equipment. Other respondents were excluded because
they were unresponsive to the questionnaire.

Performance estimates from those respondents found to be reliable were processed through a regression analysis procedure, described in Sec. 3. The regression analysis (1) fits smooth curves to the data, (2) provides a structure for making consistent performance predictions, (3) interpolates and extrapolates the data to make performance estimates for symptom complexes not included in the questionnaire, and (4) provides a means to assess the importance placed on the various symptom complex components as reflected by the data.

The process we use to construct the map of symptom complexes over time for various doses is described in Sec. 4. It maps predictions of individual performance for the symptom complexes, as determined by the regression analysis, on the dose/time plane. Section 5 discusses the following step, which includes selection of the dose, time, and performance mapping points; the output grid structure; the boundary value specifications; and the procedure for generating performance surface and isoperformance contours.

Finally, Sec. 6 presents graphical representations of individual performance profiles for the 15 members of the crews studied. Plots of performance and isoperformance contours versus dose and time are displayed for each crewmember, as well as groups of crewmembers according to similarity of tasks.

Appendixes to this report contain tabular data, graphs, and additional narratives that are related to the technical discussion and materials presented in various sections of the main body of this report. Because of the large quantity and detailed nature of those data, they are not included in the text itself.

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SECTION 2

EVALUATION OF PERFORMANCE ESTIMATES

In this section, evaluation of the questionnaires [Glickman et al., 1983] is described. The criteria by which some respondents were excluded before their answers were recorded are defined. Those criteria were rank, time in specialty, and number of crewmembers supervised. Then, the method by which respondents with unresponsive estimates were rejected is outlined. The standards for rejection were the occurrence of any of the following patterns: (1) noncompliance with the instructions; (2) a preponderance of answers at the extremes of the performance range; (3) excessive consistency for many tasks within a symptom complex; or (4) many reversals, where performance under more severe symptoms was better than performance under less severe symptoms.

Table 1 lists the number of questionnaires administered to respondents from each type of crew, and the reasons for eliminating respondents from the sample. Each of the items listed in the table is discussed in the present section. We also discuss how the answers were used to evaluate the structure of the questionnaire itself. After the excluded and rejected respondents were eliminated, the performance estimates from respondents remaining in the sample constituted the data used for the regression analysis (Sec. 3). Appendix A lists all performance time estimates from each accepted respondent.

THE RESPONDENTS

The judgments desired were of soldiers who had directed the activities of many crewmembers, who were familiar with current equipment, and who had recent experience supervising soldiers operating that equipment. We therefore asked that the questionnaires be administered to students attending the Advanced Noncommissioned Officers Classes (ANOC) at the Artillery, Armor, and Infantry schools. The exact groups of respondents requested at the Armor and Infantry schools were obtained, but scheduling difficulties prevented the participation of ANOC students at the

Table 1. Disposition of questionnaires.

	Respondent Specialty				
	Gun Crew	FDC Crew	Tank Crew	TÓW Crew	Grand Total
Raspon	idents Po	Med			
Pilot run	8	4	0	5 ^a	12
Full questionnaire	31	24	44	41	140
Post run	0	9	0	0	9
Total administered	39	37	44	41	161
Responde	ents Elim	inated			
Exclusionsb					
Grade <e4< td=""><td>. 0</td><td>4</td><td>0</td><td>0</td><td>4</td></e4<>	. 0	4	0	0	4
Time in specialty <12 months	0	l	0	0	1
Supervised <5 soldiers	6	7	l	1	15
Self-disqualified	0	0	0	2 .	2
Missing manuscript	1	0	1	0	2
Subtotal	7	12	2	3	24
Rejections ^C			*	•	
Noncompliance	1	0	0	0	1
Estimates at extremes	. 1	O	2	0	3
Excessive consistency	. 0	0	1	0	1
Reversals	2	3	1	1	7
Combined causes	. 3	1	4	. 1	9
Subtotal	7	4	8	2	21
Total eliminated	14	16	10	5	45
Respondents remaining	25	21	34	36	116

^aNot recorded.

Artillery school. Instead, a number of NCOs from the training cadres at Fort Sill answered the artillery questionnaires.

At least 24 acceptable respondents were desired for each type of crew. Since it was not expected that all of the respondents would produce acceptable questionnaires, our initial intention was to obtain

b_{Before analysis.}

^cAfter analysis.

estimates from about 30 qualified respondents of each type. The tank and TOW crew samples each contained more than 40 respondents, and each produced more than 30 acceptable questionnaires.

However, at first an adequate number of respondents for artillery crews was not obtained. We started with 31 gun crew and 24 FDC crew respondents from the training cadres. After eliminaring the unacceptable respondents, only 21 from the gun crews and 16 from the FDC crews remained. Because those numbers were low, qualified respondents were added from foot runs of the gun and FDC crews and the questionnaire was administered to a second group of 9 FDC crewmembers. Adding questionnaires from those groups increased the total number of acceptable questionnaires to 25 and 21, respectively (see Table 1). Although the number of acceptable FDC questionnaires was lower than that desired, the pattern of responses gives no cause to reject the body of data as unsound. Therefore, the FDC crew data was included in the total of 116 respondents as input for the regression analysis.

THE QUESTIONNAIRE

The questionnaire and the procedures for its administration are described in Glickman et al. [1983]. Briefly, a standard format was used for each crew; every page was identical except for the symptom description at the top of the page (see Fig. 1 for a typical page from the TOW crew questionnaire). Several tasks were listed, together with the usual time for a well crewmember to perform them (Table 2), and the respondent was asked to indicate how long it would take a typical crewmember to perform each task if that crewmember were suffering the symptoms described at the top of that page.

The tasks were divided into two types: about ten tasks were of the type the respondent had been supervising, and six were ordinary tasks

In order to verify that the questionnaire was understandable to the population from which we intended to draw our sample, we had administered a preliminary version of the questionnaire to several small groups of gun crew and FDC crew supervisors. The questionnaire for this pilot run was almost identical to the final version, with a few differences in language and normal time values, and with six fewer symptom complexes.

DESCRIPTION OF ILLNESS:

415 314

Vomited once or twice; nauseated and may vomit again; exhausted with almost no strength; unsteady upon standing quickly; extremely dry mouth, throat, skin and very painful headache; has difficulty moving; short of breath; burning skin and eyes.

CREW TASKS

÷	The usual	How long do you think it would take a crewmember to do each task if he had these symptoms?			
Tasks CREWNENBER	each task is about:	No increase in time	Amount of time (sec)	Could not do it at all	
SQUAD LEADER - Designate azimuth and target	4 sec				
Command driver to firing position	2 sec		·		
GUNNER - Set supereleva- tion, erect, slew 170° to 10° azimuth	17 sec		·		
Adjust magnification, acquire targets, iden- tify, arm, & fire.	7 sec				
DRIVER - From standstill, drive forward 40 ft. & stop	20 sec				
LOADER - Reload	60 sec				
Rearrange ready rack	60 sec				

Target Tracking Accuracy

Estimate the chance	of staying on target	during the last 6	seconds of flight
usual chance 90%).	z		

ORDINARY TASKS

Climb two flights of stairs briskly	15 sec		
Lift five heavy boxes of books from the floor to a 3 ft high mable	20 sec		

1.	How many flights of stairs could a crewmember climb quickly before becoming breathless?	flights
2.	How long could a crewmember keep walking at a brisk pace before his legs get tired?	minutes
3.	How many heavy boxes could a crewmember keep lifting from the fluor to a table before he would have to stop and rest?	boxes
4.	How long would it take a crewmember to open a simple 3-number combination lock?	seconds

How much confidence do you have in your estimates?

1	2	3	4	5
None	Not Much	Some	A Lot	Certain
<u> </u>		نيد ديستست ا		

Figure 1. Sample page from questionnaire (TOW crew).

Table 2. Crew tasks.

Crew Type ^a	Position	Task Number	Crewmember	Description of Task	Usual Time (sec)
			(D)	Gun Grew	
1	1	-	Chief of section	Receive fire order and call quadrant eleva- tion, deflection, projectile, charge, fuze	e
	7 7	3 5	Gunner	Set deflection Traverse tube and level bubble	7
	m m	. 5	Assistant gunner	Set quadrant elevation Elevate tube and level bubble	7 . 3
	4444	9 C 8 G	Loader	Lift projectile to tray Position and operate hydraulic rammer Place charge and release breech block Insert primer and close firing lock	2 2 1.5
	44	10		Attach lanyard and fire Swab tube and inspect bore	1.5
			P	Fic crew	
2 7 7		3 5 3	Fire direction officer	Announce fire order Review calculations Announce fire mission	4 v v
777	5 5 5	4 5 9	Horizontal control operator	Plot target location on chart Orient range-deflection protractor Read range-deflection protractor	ഗനന
5 5	e e	7 8	Computer	Calculate fuze setting, deflection, and quadrant elevation Announce fire commands to guns	15

Table 2. Crew tasks (Concluded).

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				I	Tank Crew	
	,	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	Tank co	Tank commander	Issue fire command Range the target Depress and lay gun for direction Issue subsequent fire command	28.4
ттт	777	5 6 7	Cunner		Identify target Aim and fire Apply fire adjustment and fire	1 6 7
m m	m m	ω 5	Loader		Arm Load and arm	. 2
3	4	10	Driver		Stop	4
				5	TOW Crew	
44		1 2	Squad leader	leader	Designate azimuth and target Command driver to firing position	5 7
4	2	٣	Gunner		Set superelevation, erect, slew 170 deg to	17c
4	5	4			Adjust magnification, acquire targets,	7
7	æ	5	Driver		From standstill, drive forward 40 ft and stop	20
4 4	4 4	6	Loader		Reload Rearrange ready rack	09
7	2 ^d	∞	Gunner		Target tracking accuracy (probability of staying on target during last 6 sec of flight)	p%06

^aCrew type is indicated by the following numbers: 1, gun crew; 2, FDC crew; 3, tank crew; 4, TOW

 $^{
m b}_{
m Includes}$ 2 sec machine time.

 $^{\text{C}}_{\text{Includes}}$ 15 sec machine time.

To emphasize that difference, the question was formatted differently on the questionnaire and presented in a differderformance on this task is measured in terms of accuracy; therefore, usual performance is expressed in terms of probability of staying on target rather than time to perform the task. ent order from the other gunner tasks (see Fig. 1). familiar to both military and nonmilitary persons. Four of the ordinary tasks did not have stipulated normal values. For cross-calibration purposes, the questions about ordinary tasks with unstipulated norms were to be included on a questionnaire intended to be administered to a group of persons who had experienced radiation sickness from radiotherapy.

Three categories were provided for answers to the questions with stipulated norms: (1) no increase in time (relative to the usual time), (2) amount of time (if longer than usual time), and (3) could not do it at all. All of the questions about crew tasks, with the single exception of the tracking accuracy question on the TOW crew questionnaire, pertained to the time to perform a task. No account was taken of the possible increase in errors that might accompany the increase in time for a sick crewmember to do a task. Although an increase in errors is to be expected of a sick crewmember, we found that concept difficult for the soldiers to accept, especially when coupled with the fact that they viewed many tasks as either being "completed" or "not completed." Since reliable, consistent estimates could not be obtained from the soldiers on that topic without an extensive introductory discussion, the questions were framed about time only.

Performance

Some crewmember tasks include a fixed time for mechanical equipment to perform some function. In the questionnaire, the tasks were presented with the human and equipment times combined because the soldiers had experienced it that way, and discussed it that way when the questionnaire was being developed. An example is shown in Fig. 1. For the gunner's first task, "Set superelevation, erect, slew 170 deg (17 sec)," the ITV turret takes 15 sec to erect and slew, and it takes the gunner 2 sec to initiate the sequence, so the entire sequence takes 17 sec to complete. Our interest focused on the 2 sec portion for human performance. We therefore deducted 15 sec from both the "usual time" and the estimates of "time when sick" when we calculated performance.

When the replies were processed, they could be treated in one of three ways:

- 1. $t t_0$: the difference between "time when sick" and "usual time."
- 2. t/t_o : the ratio of "time when sick" to "usual time."
- 3. t_0/t : the ratio of "usual time" to "time when sick."

Treating the responses as t_0/t enables performance to be expressed in the interval extending from 1.0 to 0, where 1.0 represents "usual time" and 0 represents "could not do it." Using t_0/t also accommodates the indefinite boundary between "amount of time" and "could not do it." It was apparent from the soldiers' answers that that boundary differed widely between respondents. Some respondents did not give any answers larger than 30 times the usual time, whereas others gave answers as large as 300 times the usual time. In terms of the t_0/t scale, however, that difference falls between a performance of 0.03 and 0.003, where the distinction is unimportant.

Symptom Complexes

The symptom description at the top of the questionnaire can be represented by a six-digit symptom complex number, such as 415314. Each place in that code corresponds to one of six symptom categories, and the value of each digit indicates the severity level for one of the symptoms. The symptom categories, in the order that they appear in the symptom complex number, are as follows: upper gastrointestinal distress; lower gastrointestinal distress; fatigability and weakness; hypotension; infection, bleeding, and fever; fluid loss and electrolyte imbalance. Thus, the above sample cole number (415314) indicates the following: no effect for the second and fifth symptom categories (lower gastrointestinal distress, and infection and bleeding); an effect of severity level 4 for the first symptom category (upper gastrointestinal distress), level 5 for the third symptom category (fatigability and weakness), level 3 for the fourth symptom category (hypotension), and level 4 for the sixth category (fluid loss and electrolyte imbalance).

EXCLUSIONS

The first page of the questionnaire (Fig. 2) was designed to collect demographic information about the respondents. The complete body of demographic data is listed in Appendix B, and summarized in Table 3.

A histogram of the demographic responses is shown in Fig. 3. The vertical dotted line denotes the threshold for exclusion used in Glickman et al. [1983]. The preponderance of respondents for tank and TOW crews cluster toward the high end of al! three histograms; "Grade," "Time in specialty," and "Number supervised." Only one respondent for each of those crews (302, 414) failed to meet the criteria. Respondents for the artillery crews (gun crews and FDC crews), on the other hand, cluster more closely toward the exclusion thresholds. Indeed, 18 of those respondents failed to meet the criteria. That difference suggests that the artillery sample was unlike the tank and TOW crew samples and might perhaps make different judgments.

Any respondent who failed to meet one of the criteria was excluded. Some respondents failed to meet more than one criterion. Four were excluded because their rank indicated insufficient responsibility. Two of those four could also have been excluded on the basis of insufficient time in their specialty. One other respondent was excluded on the basis of both insufficient time in his specialty and insufficient supervisory experience.

In all, 15 respondents reported insufficient supervisory experience. But there was one peculiar aspect of responses to the question about supervisory experience; some respondents with 10 years in their specialty, for example, claimed to have supervised only 10 or 20 crewmembers. Most respondents with that much experience claimed to have supervised more than 50 crewmembers. It may be that some respondents interpreted the

The respondent numbers are given here to permit readers to examine the demographic data for each excluded respondent, which are listed in Table 3, and to examine the full set of answers from each of the 21 rejected respondents listed in Appendix D. Each respondent is signified by a three-digit code, with the first digit indicating the type of crew they had supervised (see Table 2). Gun crews are designated as 1, FDC crews as 2, tank crews as 3, and TOW crews as 4. The last two digits indicate the order in which the respondents completed the questionnaire.

To help us understand the characteristics of this group we are asking you to supply some information about your military experience. Please note that all your questionnaire responses will be strictly anonymous and there will be no attempt to link these responses to you as an individual. The answers to the information below will be used only for descriptive purposes. Please supply the following information about yourself:

Your present grade and MOS?	
How long have you been in the Army?	
How long have you been in anti-armor?	
Have you been in combat? Yes No When	
Have you been in anti-armor combat? Yes No	
When	
Have you served as a: When? How long?	•
Squad Leader	
Gunner	
Loader	
Driver	
Approximately how many crewmen have you supervised in Mounted TOW	
2 5 10 20 50 More than 50	
Briefly describe your military duties during the past year:	
,	

Figure 2. Sample of demographic data sheet.

Table 3. Demographic summary.

Respondent	Grade	Time (months)	Number Superviseá	Respondent	Grade	Time (months)	Number Supervised
101	5	36	5	211	1 d	121	5
102a	5	96	5,	212	5	42	5
102 103 ^a , b	5	31	5	213	5	48	
104ª	6	120	10	214	6	84	10
105 ^a	5	51	20	215	4	30	5
106 ^a	5	120	5	216	5	54	10
107 ^a	5	60	10	217°	6	102	2 ^c
108 ^a	5	46	5	218	7	192	>50
109 ^a	6	120	10	219 ^c ,e	4	11 ^e	0°
110	5	72	10	220	5	48	10
111	5	50	20	221	5	12	5
112	5	39	5	222°	5	62	2°
113	5	96	5	223	4	48	5
114	5	48	10	224	4	24	5
115	6	48	10	225	4	25	5
116 ^c				11	•		0°
	5	42	2 ^C	226°	6	108	-
117	4	32		227	6	60	10
118 119	6 7	120 177	10 10	228 229 f	7	156.	<50
120	6	96	50	229° 230°f			
				230			
121 122	5	≈12	10	231 ^c ,g	4	24	2 ^c
122 123 ^c	5	40	5 0 ^c	232 ⁸ 233 ^d ,g,h	4	30	h
	5	84		2330.8.h 234c.g.h	3 d	12	0c,h
124 125 ^c	5 5	72 48	5 0 ^c	2358	4	12	
				11	5	36	5
126	6	24	5	236 ^g	5	48	
127 128	5	46	20	2378 2388	4	30	
128 129 ^c	5 5	14	5 0 ^c	239° • g	4	30	10
130	7	48 156	10	239518	4	30	2 ^C
				301	6	96	20
131	7	144	>50	302°	6	60	0c
132	5	40	5	303	6	96	>50
133	5	36	5	304	6	84	>50
134 135 ^c	5	30	20 0°	305	6	166	>50
	5	30		306	6	108	>50
136 ^c	5	52	0.	307	6	96	10
137	6	84	5	308	7	84	>50
138	5	36	10	309	6	60	>5ŭ
139	6	84	10	310	6	96	20
201a	7,	72	10_	311	6	120	>50
202a,c,d,e	3 ^d	9 e	0_{c}	312	6	108	. 20
203ª, c	4	28	o ^c	313	6	120	50
204 ^a	4	62	5	314	6	108	>50
205	4	28	5	315	6	102	50
06c,d,e	$2^{\mathbf{d}}$	6e	0°	316	6	84	20
07	5	24	5	317	6	96	20
:08	4	30		318	7	90	>50
:09	4	29	5	319	6	108	50
210	6	60	10	320	6	126	>50

Table 3. Demographic summary (Concluded).

Respondent	Grade	Time (months)	Number Supervised	Respondent	Grade	Time (months)	Number Supervised
321	6	133	20	416	7	72	>50
322	7	72	>50	417	6	54	>50
323	6	132	50	418	6	108	>50
324	6	96	>50	419	6	72	>50
325	6	126	>50	420	6	96	50
326 ¹	. 6	78	>50	421	6	84	50
327	6	96	20	422	. 6	72	50
328	6	72	50	423	6	126	50
329	6	120	>50	424	6	36	>50
330	. 6	120	20	425	6	132	>50
331	7	174	50	426	6	104	20
332	6	96	>50	427	6	96	50
333	6	138	>50	428	6	96	50
334	6	160	20	4293	7	72	20.1
335b	6	101	>50	430	7	60	>50
336	6	126	50	431 ^j	6	36	10 j
337	6	132	>50	432	6	60	>50
338	7	135	>50	433	6	84	>50
339	6	120	>50	434	7	72	10
340 ¹	7	132	>50	435	6	84	>50
341	6	120	>50	436	6	72	20
342 ¹	7	132	>50	437	6	84	>50
343	6	126	50	438	6	84	50
344	6	96	20	439	6	48	20
401	6	60	>50	440	6	54	50
402	6	132	>50	441	6	36	>50
403	6	120	10			*-	
404	6	120	50	1			
405	- 6	120	>50	J		•	
406	6	108	50				
407	. 6	68	20				
408	6	72	50	ł			
409	6	48	20				
410	7	204	>50	1			
411	6	84	20	j			
412	6	96	>50	l			
413	6	48	50	1			
414 ^C	6	36	0c				
415	6	102	50	ĺ			

NOTE: Respondent numbers consist of a single-digit crew number (see Table 2) and a two-digit number indicating the order in which respondents finished the questionnaires.

^aPilot questionnaire.

bManuscript missing; respondent excluded.

c<5 supervised; respondent excluded.</pre>

 $^{^{}d}$ <E4; respondent excluded.

 $^{^{\}rm e}$ <12 months; respondent excluded. $^{\rm f}$ Questionnaire not administered.

 $^{^{\}rm g}$ Postrun; symptom complexes in reverse order.

 $^{^{\}mathsf{h}}\mathsf{Disqualified}$ seif--no experience.

iusmc.

JNo ITV experience.

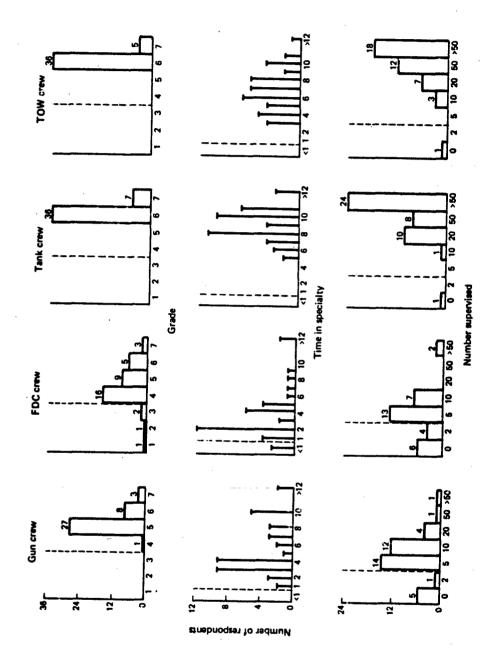


Figure 3. Histograms of demographic responses.

question to be "How many crewmembers have you supervised at any one time?" In that case, a tank platoon sergeant would claim 20. And, indeed, the tank crew respondents do show a bimodal distribution, perhaps due to that interpretation of the question. A bimodal distribution of number supervised also appears for the gun crews and FDC crews. That possible misinterpretation did not have any serious consequences for the tank and TOW crew samples, as they lost only one respondent each. However, the gun crew and FDC crew samples lost 6 and 7 respondents, respectively. Those figures represent a loss of 16 and 21 percent of the gun crew and FDC crew samples, as opposed to 3 percent of the tank and TOW crew samples.

| 1.1 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.

Two of the respondents (429, 431) disqualified themselves. They noted on their demographic sheets that, although they had antiarmor experience, they did not feel qualified to make estimates about the TOW crews because they had had no ITV experience.

In two cases, manuscript questionnaires were missing. Responses from one respondent (103) had been transcribed into the data base. But the computer data could not be checked against the manuscript; thus, that respondent was excluded. In the other case (335), no responses had been entered into the computer, so the respondent was excluded.

REJECTIONS

Unlike the excluded respondents, who were eliminated before their answers were recorded, rejected respondents were eliminated on the basis of the answers themselves. The reasons for rejecting those respondents fall into four categories: (1) noncompliance with the instructions, (2) concentration of answers at the extremes, (3) excessive consistency, and (4) reversals. Some respondents were rejected because of a combination of those factors. The rejected respondents' answers are shown in Appendix D.

Noncompliance

One of the respondents (124) did not comply with the instructions to estimate the amount of time for a sick crewmember to perform each task (see Fig. 1). He marked the first sheet of his questionnaire

correctly, but all of the subsequent sheets contained checkmarks in column 2 instead of numerical estimates. Some respondents occasionally entered task times that were less than the usual time. Those entries were recorded as "no reply." In cases where they were numerous, however, they were considered, together with other nonresponsive answers, as one of the combined causes of rejection.

Extremes

Three respondents (113, 301, 304) submitted estimates that were predominantly at either of the two ends of the performance range: "no increase in time," or, "could not do it at all," with very few estimates in the range of degraded performance between the two extremes. That pattern was inconsistent with the pattern of the other respondents, who produced estimates indicating that they expected many of the symptom complexes to cause performance to be partially degraded.

Excessive Consistency

One respondent (303) was found to respond to many symptom complexes with the usual time for each different task multiplied by the same constant, or with the same constant added to the usual time for many different tasks. That respondent was removed from the sample because his estimates apply to the effect of the symptom complex on performance in general, rather than to the effect of the symptom complex on the performance of particular tasks.

Combined Causes

Eight respondents (115, 121, 218, 307, 309, 316, 338, and 403) were found to have many instances of excessive consistency, but not enough to provide conclusive grounds for rejection. When combined with other causes, each also individually insufficient for rejection, excessive consistency and the other combined causes do provide conclusive grounds for rejection. One respondent (403) was rejected for combined causes, plus reversals. Reversals are computed in a way that precludes adding the percentage of their incidence to the percentage of the incidence of other rejection causes.

Reversals

After removal of the extreme and consistent respondents, the estimates were reviewed to identify those instances where performance improved when sickness intensified. A few such instances should be expected for each respondent because (1) time was not provided for the respondents to cross-check their estimates, (2) the format of the questionnaire did not facilitate cross-checking, and (3) the questionnaire did not suggest cross-checking.

For each respondent, performance estimates were compared with tasks where the symptom complex differed in only one symptom, which we called an adjacent symptom complex. For example, a respondent's estimate for symptom complex 312111 would be compared with his estimates for symptom complexes 212111, 412111, 313111, and if no comparison with 313111 was possible, 314111. If the estimated performance for the adjacent symptom complex was the same, it was not counted. If it was different, it was counted as an "opportunity" (to detect a reversal). If the respondent had estimated that the more serious symptom produced higher performance than the less serious symptom, it was counted as a "reversal." The number of reversals was compared with the number of opportunities to obtain the percentage of reversals.

There are no clear cases where the percentage of reversals by a particular respondent approached or exceeded random guessing (50 percent). Six respondents (106, 138, 232, 238, 438) were rejected because the percentage of reversals indicated that their replies were not consistent with the intended graduation of symptom complexes.

QUESTIONABLE SYMPTOM DESCRIPTIONS

The percentage of reversals was also used as an index to judge the clarity of the symptom complex descriptions. That analysis showed that some symptom complexes produced many more reversals than average. A case in point is symptom complex 411111, which should be considered with care in any further analysis. We sought to resolve that and other uncertainties by revisiting the military facilities where the initial questionnaires were administered, and giving follow-up questionnaires to all of the original respondents still available.

To determine if the order of presentation of the symptom complexes had any effect upon the estimates of the respondents, the number of reversals were plotted against order of presentation. The plot, with lines connecting complexes of similar symptom groupings (Fig. 4), shows a pronounced learning curve with three characteristics: (1) the respondents made 10 percent more reversals on the first page of the questionnaire than they made on the worst of the other pages; (2) the respondents made more reversals the first time they encountered a symptom combination than they did on subsequent encounters, and, in general, the more times they encountered a symptom combination the fewer reversals they made; (3) the ability of the respondents to accommodate new symptom combinations appeared to deteriorate with increasing length of questionnaire.

Although the first symptom complex (411111) usually engendered more reversals than other symptom complexes, the difference between that symptom complex and the next worst complex was insufficient to justify deletion of all replies for complex 411111. In their indication of the confidence that they had in their estimates, the respondents did not show an awareness of the learning curve effect.

INTERPRETATION OF SYMPTOM DESCRIPTIONS

In the follow-up questionnaire, the respondents were asked how they interpreted our symptom descriptions. Figure 5 shows the format used to ask that question, and Figs. 6 through 13 are bar graphs of their answers.

The bar graphs indicate that the different groups of respondents sometimes said they interpreted the symptom descriptions quite differently. The less severe upper gastrointestinal distress symptom in Fig. 6a. for example, was correctly interpreted by about 80 percent of the TOW crew respondents so that "vomited once or twice; nauseated and may vomit again" meant that a crewmember did not vomit during the task in question, but only about 20 percent of the tank crew respondents said they gave the description that interpretation. The more severe upper gastrointestinal distress symptom in Fig. 6b was correctly interpreted by only 25 to 30 percent of the respondents. However, the upper gastrointestinal distress question was the first on the follow-up questionnaire, so we suspect that it is likely to have more errors than subsequent questions.

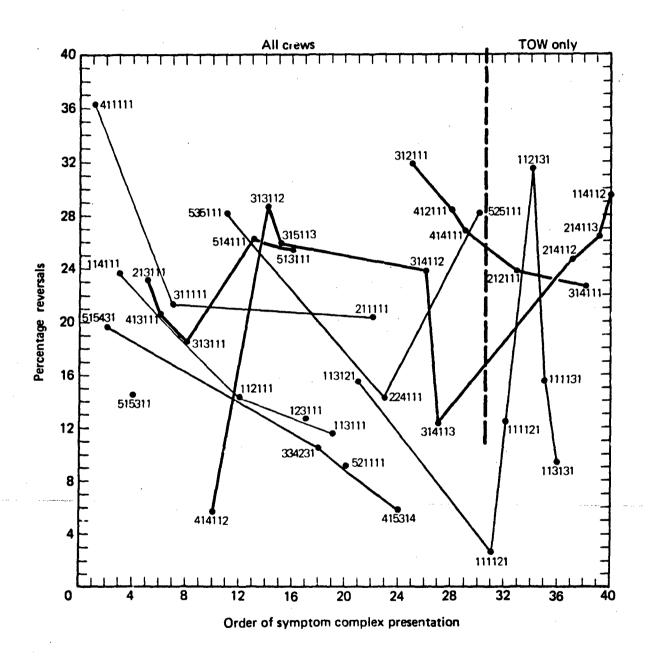


Figure 4. Learning curve.

WHEN WE SAID:	DID THAT MEAN TO YOU: (Check one)
Vonited once or twice; nausea- ted and may vomit again	Vomiting occurred during the task Vomited before and after but not during the task
Vorited several times, in- cluding the dry heaves; severely nauseated and will soon vomit again	Vomiting occurred during the task Vomited before and after, but not during the task
Occasional diarrhea, recently defecated and may again	Defecating during the task Defecated before and after, but not during the task
Frequent diarrhea and cramps, defecated several times and will again soon	During the task: Defecated Had cramps Both
	Before and after, but not during the task: Defecated Had cramps Both
Doesn't want to eat	Must be pretty sick Doesn't matter
Difficulty in stopping any bleeding	Bleeding Not bleeding Doesn't matter

Figure 5. Questions on symptom descriptions.

Unsteady upon standing quickly	Loaders are unsteady
	Loaders are not unsteady
	Tank commanders are unsteady
	Tank commanders are not unsteady
Faints upon standing quickly	Loaders faint
	Loaders do not faint
	Tank commanders faint
	Tank commanders do not faint
Weak and faint	Faints
	If careful, can keep from fainting
	Doesn't faint
	Only loaders faint
May faint with moderate	Faints
exertion	If careful, can keep from fainting
	Poesn't faint
	Only loaders faint
Joints ache	Affects everybody
	Affects only those who have to move around a lot
	Affects only those who have to move heavy objects

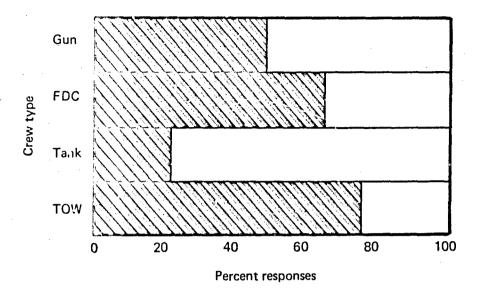
Figure 5. Questions on symptom descriptions (Continued).

Doesn't matter

Aches all over	Affects everybody
	Affects only those who have to move around a lot
	Affects only those who have to move heavy objects
	Doesn't matter
Has difficulty moving	Affects everybody
	Affects only those who have to move around a lot
	Affects only those who have to move heavy objects
	Doesn't matter
Headache	Affects aiming and tracking targets
Headache	Affects aiming and tracking targets Affects calculating
Headache	
Headache	Affects calculating
Headache	Affects calculating Affects attention and concentration
Headache	Affects calculating Affects attention and concentration Affects aggressiveness
Headache Very painful headache	Affects calculating Affects attention and concentration Affects aggressiveness
	Affects calculating Affects attention and concentration Affects aggressiveness Doesn't matter
	Affects calculating Affects attention and concentration Affects aggressiveness Doesn't matter Affects aiming and tracking targets
	Affects calculating Affects attention and concentration Affects aggressiveness Doesn't matter Affects aiming and tracking targets Affects calculating
	Affects calculating Affects attention and concentration Affects aggressiveness Doesn't matter Affects aiming and tracking targets Affects calculating Affects attention and concentration

Figure 5. Questions on symptom descriptions (Concluded).

a. Vomited once or twice



b. Vomited several times

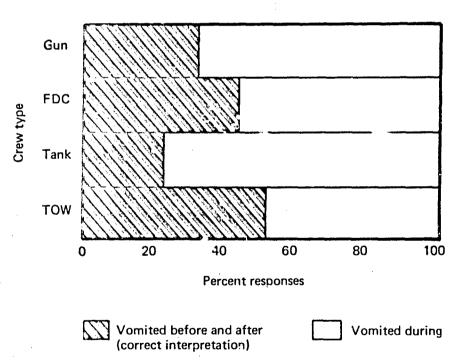


Figure 6. Interpretation of upper gastric symptoms.

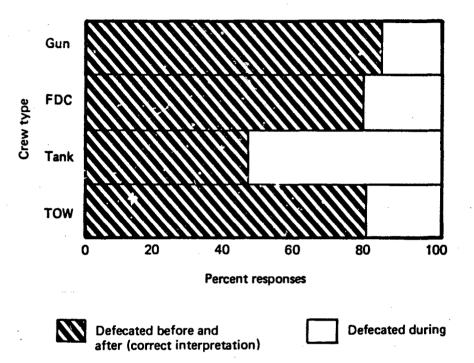
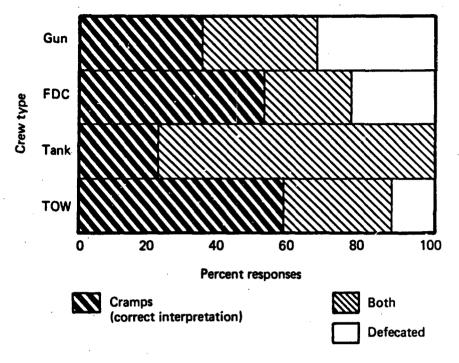


Figure 7. Interpretation of lower gastric symptoms: occasional diarrhea.

a. During the task



b. Before and after, but not during

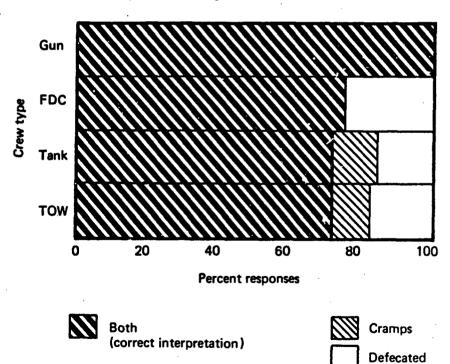
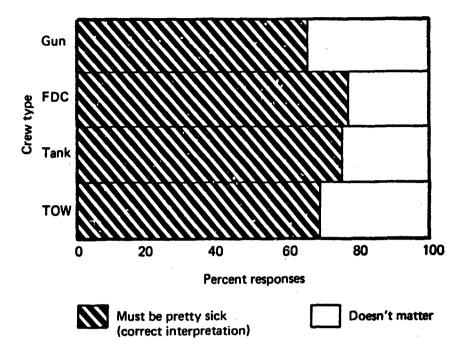


Figure 8. Interpretation of lower gastric symptoms: frequent diarrhea and cramps, defecated several times and will again soon.

39

a. Doesn't want to eat



b. Difficulty stopping any bleeding

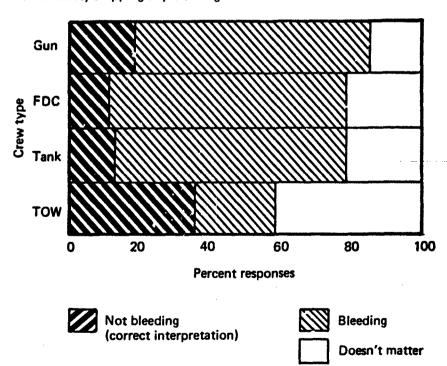


Figure S. Interpretation of anorexia and bleeding symptoms.

The less severe lower gastrointestinal distress symptom (Fig. 7) was correctly interpreted by about 80 percent of the respondents, for all crews except the tank crew, where about 45 percent of the respondents interpreted the description correctly. The more severe lower gastrointestinal distress symptoms were correctly interpreted by 20 to 60 percent of the respondents for the period during the task (Fig. 8a). On the other hand, for the period before and after the task (Fig. 8b), the symptom was correctly interpreted by 75 to 100 percent of the respondents.

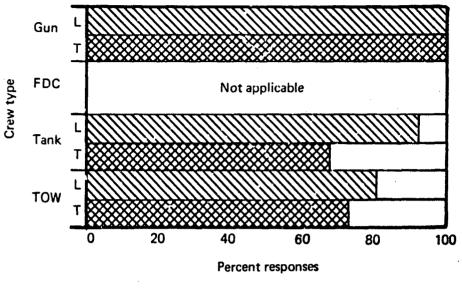
Figure 9 shows that 60 to 75 percent of the respondents interpreted anorexia as we had intended, but only 15 to 35 percent of the respondents correctly interpreted "difficulty in stopping any bleeding."

Correct interpretation of the less severe hypotension symptoms (Figs. 10a and b) varies from about 60 to 100 percent, except for the TOW crew respondents' interpretation of tank commanders (i.e., TOW squad leaders) fainting upon standing quickly (Fig. 10b). Correct interpretation of the more severe hypotension symptoms (Figs. 10c and d) fell between 60 and 85 percent for respondents from all crews.

Between 45 and 85 percent of the respondents correctly interpreted the reduction in loss of mobility that accompanies infections (Fig. 11). The other respondents usually said there would be some effect, but many FDC crew respondents (20 to 40 percent) said that mobility difficulties would not matter. That answer may reflect the sedentary nature of operations within the FDC during those times that the FDC is directing fire rather than moving from place to place.

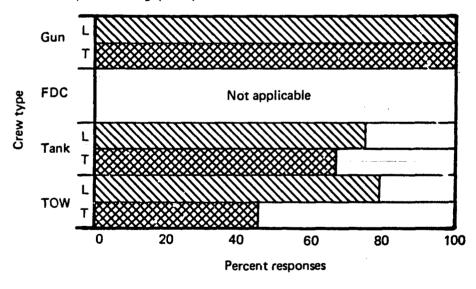
Unlike the interpretation of the effects of hypotension, which appears to be crew-related, the general effect of headache (Fig. 12) is interpreted by the respondents to affect performance of all crews, but particular effects (Fig. 13) are assessed to apply less to activities that the crew does not perform. For example, the gun crew does aiming but no calculating, and the FDC crew does calculating but no aiming and tracking. Respondents from those crews estimated that there would be a significant (40 to 65 percent) headache effect on the kinds of activities their own crew performed, and little or no headache effect (0 to 2 percent) on the kinds of activities their crew did not perform.

a. Unsteady upon standing quickly





b. Faints upon standing quickly



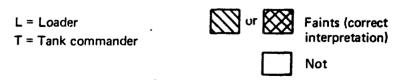
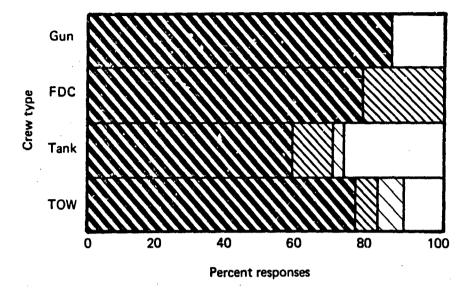


Figure 10. Interpretation of hypotension symptoms.

c. Weak and faint



d. May faint with moderate exertion

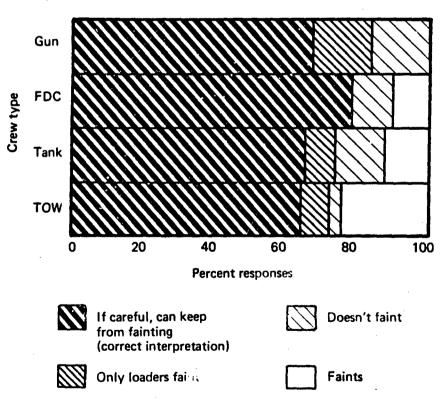
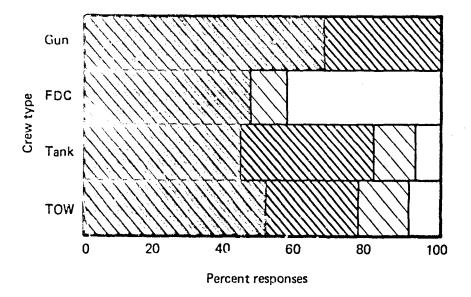
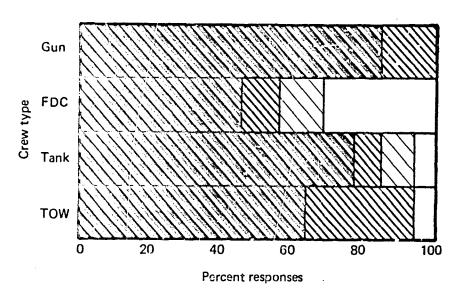


Figure 10. Interpretation of hypotension symptoms (Concluded).

a. Joints ache



b. Aches all over



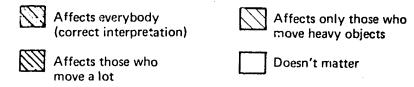
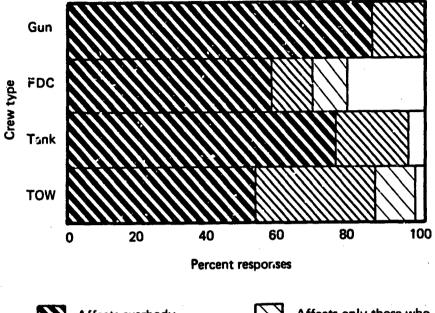


Figure 11. Interpretation of infection symptoms (mobility).

c. Difficulty moving



Affects everbody (correct interpretation)

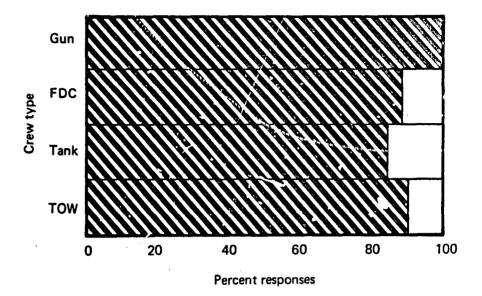
Affects those who move a lot

Affects only those who move heavy objects

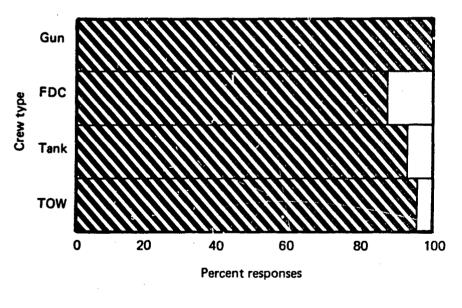
Doesn't matter

Figure 11. Interpretation of infection symptoms (Concluded).

a. Headache



b. Very painful headache



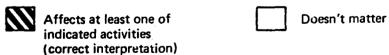
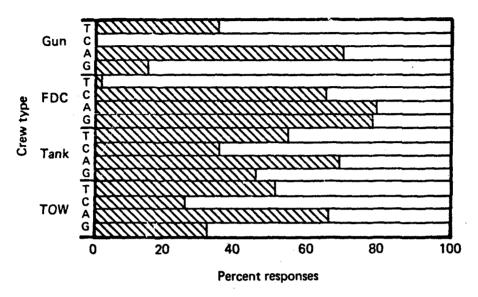
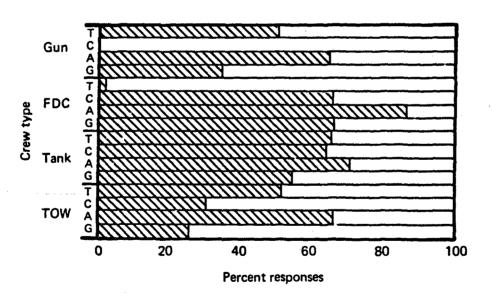


Figure 12. Interpretation of headache symptoms.

a. Headache



b. Very painful headache



T = Aiming and tracking C = Calculating	Affects that category
A = Attention and concentration	
G = Aggressiveness	Does not affect that categor

Figure 13. Activities affected by headache.

Unfortunately, the number of respondents who answered the follow-up questionnaire for the artillery (6 for the gun crew and 10 for the FDC crew) was much smaller than for the tank and TOW crews (27 and 40). Consequently, the follow-up questionnaire does not permit a confident assessment of the effect of symptom interpretations upon the answers of the artillery respondents.

Also, that part of the follow-up questionnaire required the respondents to recall the opinions they had acted upon some 2 months previously when they filled in the questionnaire. It may be that the interpretations were less obvious to the respondents when the symptom descriptions were embedded in the fabric of the questionnaires than they were when explicitly described by the follow-up questionnaire.

TASKS WITH UNSTIPULATED NORMS

Six of the tasks in the original questionnaire were ordinary (non-military) tasks, as opposed to combat crew tasks. The ordinary tasks concerned climbing stairs, walking, carrying boxes, and opening combination locks (see Fig. 1). Four of those ordinary tasks had no "usual" reference times stipulated. In administering the questionnaire to TOW crewmembers, we asked them to stipulate their own estimates of "usual" values for the performance of a typical crewmember when unaffected by sickness. We then compared their estimates for best performance of those ordinary tasks by a sick crewmember with their estimates for performance by a well crewmember. Figure 14 shows how the responses were typically distributed. About one-third of the estimates of best performance when sick were equal to performance when well, which is reasonable. Such a finding indicates that about one-third of the respondents believed that at least one of the symptom complexes would cause no deterioration in normal performance.

Somewhat less than one-half of the respondents estimated that best performance when sick would not exceed performance when well. That too is reasonable. But somewhat more than one-quarter of the respondents estimated that sick performance, for at least one symptom complex, would exceed well performance. A possible explanation is that those respondents did not recall the precise estimate of well performance that they

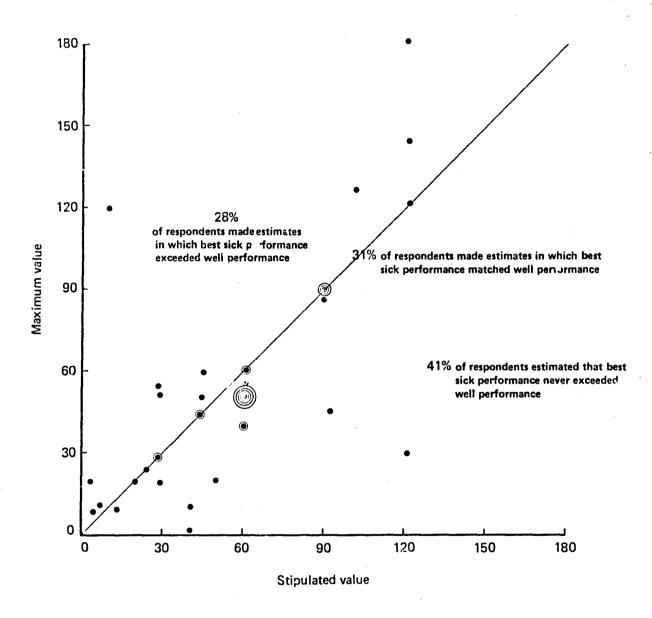


Figure 14. Tasks with unstipulated norms: "How long could a crewmember keep walking . . .?"

specified at the beginning of the questionnaire. Such a lack of recall may have permitted them to make subsequent estimates of sick performance that exceeded their estimates of well performance.

That kind of reversal did not occur in significant numbers for the two ordinary tasks for which the usual times were stipulated on the questionnaire. We thus conclude that: (1) up to 25 percent reversals should be anticipated and be regarded as normal, and (2) the use of questions with unstipulated norms should be avoided.

SINGLE SYMPTOM

The regression analysis of Sec. 3 was intended to fill the gaps in the sequence of symptom complexes because there was not time to ask the soldiers to estimate performance for all of the probable complexes. The estimates that we did obtain from the soldiers can be plotted to show how patterns of performance change with the increase in severity of a single symptom in a complex. This subsection explains that process, and shows that the soldiers estimated that, in most cases, performance declines fairly uniformly as symptom intensity increases, so that a linear regression to fill the gaps between estimates is a reasonable procedure for most of the individual tasks treated here.

The symptom complexes are descriptions of discrete sickness states. Each symptom level is intended to be more severe than the preceding level, but was not intended to be a regular increment along some scale. Also, the scales do not imply that performance at any particular symptom level is necessarily worse than that at the preceding symptom level. It was expected that in some instances performance might remain constant as symptom intensity increased, particularly in cases where the increase in severity occurs in a symptom that does not have a strong influence on the task being plotted. In fact, the soldiers estimated that this would happen in several instances.

Furthermore, it was expected that, in some instances, performance might decline more drastically from one symptom level to the next than for the preceding or following symptom level. And, in fact, the soldiers estimated that this would happen in several instances, as shown in Appendix C. Those plots compare performance estimates for two or three

symptom complexes where symptom severity levels differ in only one symptom, and severity levels for all other symptoms in the complex are held constant. Figure 15 is an example of a single-symptom plot showing the estimated performance of a typical tank crew loader for symptom complexes 411111, 412111, 413111, and 414111. Because the severity level for only one symptom category (fatigability and weakness) changes in this comparison, performance should either decrease or remain the same as the level of fatigability and weakness increases. And it does just that in this case, as in most of the plots in Appendix C. Figure 16, an example of the format used in Appendix C, shows the single-symptom plots for both the tasks performed by the tank crew loader.

VARIANCE

If our description of symptoms was ambiguous, we should expect to see some consistency in the occurrence of wide interquartile ranges for one symptom complex at many tasks. Such consistency occasionally occurs. The most pronounced cases are listed in Table 4. However, there is no occurrence of consistently wide interquartile ranges for all tasks with any of the symptom complexes, so we can conclude that the symptom descriptions do not contain serious ambiguity.

DATA BASE FOR PERFORMANCE ESTIMATES

The performance data base used for the performance regression analyses, described in Sec. 3, is corposed of the soldiers' estimates, with the exclusion and rejection of the respondents identified in this section. We believe that the data base represents the aggregate professional estimate of soldiers who are expert in supervising crewmembers performing the tasks described on the questionnaire, and that the most serious of the spurious estimates have been filtered out of the data.

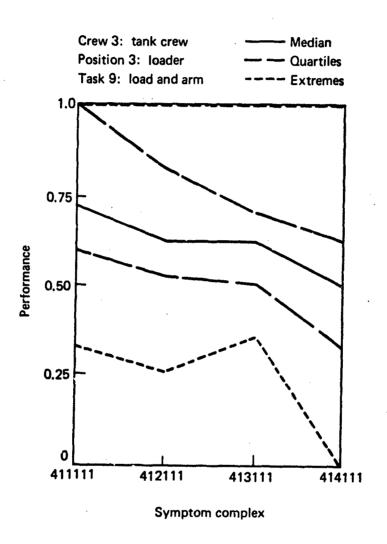


Figure 15. Example of single symptom description.

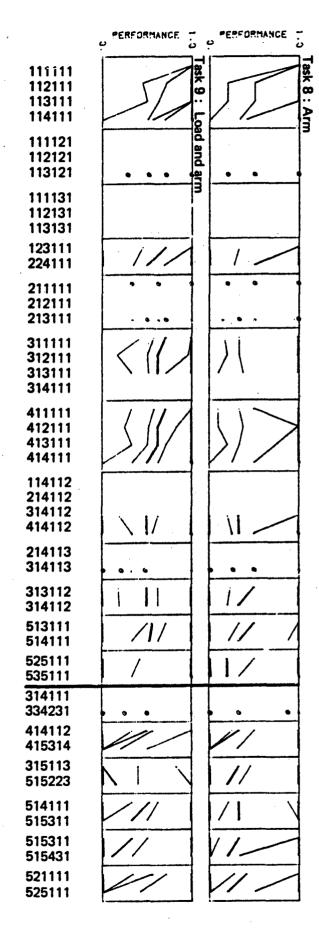


Figure 16. Example of a series of single symptom plots for all tasks in one crew position.

Table 4. Widest interquartile ranges.

Symptom Complex	Crew	Task	Median t _O /t	Interquartile Range
111131	4	3	0.40	0.87
113111	ì	6	0.50	0.78
114111	3	1	0.42	0.80
	-	5	0.42	0.75
114112	4	5	0.57	0.80
123111	i	7	0.50	0.73
	-	11	0.60	0.70
211111	1	6	0.40	0.80
		9	0.75	0.70
213111	3	1	0.50	0.73
		5	0.50	0.73
2141;3	4	5	0.50	0.80
224111	1	7	0.60	0.75
	3	1	0.33	0.77
		3	0.46	0.73
		5	0.33	0.84
		8	0.50	0.73
311111	3	5	0.50	0.75
312111	3	1	0.33	0.75
	4	3	0.40	0.80
313111	2	8	0.60	0.70
	4	3	0.40	0.80
313112	3	8	0.50	0.77
314112	3	8	0.33	0.80
314113	1	2	0.48	0.72
	_	4	0.48	0.70
	3	6	0.52	0.72
		7	0.48	0.74
22/221		10	0.45	0.77
334231	1	2	0.47	0.70
	3	4	0.47	0.70
	3	6 7	0.52	0.75
		8	0.46 0.33	0.70 0.88
411111	. 4	4	0.40	0.80
412111	i	i	0.55	0.70
,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	•	10	0.75	0.70
414111	1	7	0.60	0.70
*****	3	i	0.33	0.80
	•	5	0.33	0.80
		8	0.50	0.75
414112	. 4	3	0.50	0.72
513111	1	7	0.60	0.83
		10	0.50	0.77
	3	1	0.33	0.82
		5	0.33	0.80
514111	1	7	0.38	0.77
515311	3	8	0.33	0.90
521111	1	7	0.75	0.71
		8	0.45	0.27
		10	0.75	0.70
	3	5	0.33	0.80
		8	0.42	0.73
	4	3	0.40	0.87
515223	2	3	0.60	0.85
525111	1	2 3	0.48	0.70
			0.47	0.70
	•	4	0.52	0.72
•	3	6	0.40	0.83
	,	7	0.31	0.70
626111	4	5	0.51	0.80
535111	3	6	0.40	0.73

SECTION 3

PERFORMANCE REGRESSION ANALYSIS

This section describes the procedure used to develop linear least squares regression models based upon the army questionnaire data discussed in Sec. 2. The models provide the means to (1) fit smooth curves to the original data, (2) generate consistent predictions of performance, (3) interpolate and extrapolate performance for symptom complexes other than those from the questionnaire data, and (4) assess the relative importance of each of the specific symptoms in the complexes.

Since the original data consist of estimates of time required to complete a task, a consistent method of converting those estimates to relative performance values is needed. Additionally, a procedure had to be developed that combines data for several different tasks into a single set of estimates for a given crew position. The regression analysis used here fits selected models to the data. It provides relationships for estimating performance and the associated variances in fitting the data. The performance values that we calculate with the models can then be applied to a dose/time mapping framework (Sec. 4) to yield predictions of overall performance as a function of dose and time.

As discussed in Sec. 2, army personnel were asked to answer questions regarding the length of time it would take crewmembers to perform normal combat tasks if experiencing specific physiological symptoms. Each given combination of those symptoms is referred to as a symptom complex. Questionnaires presented to members of artillery gun crews, artillery FDC crews, and tank crews contained 30 different symptom complex descriptions; the mounted TOW crew questionnaire contained ten additional symptom complex descriptions. Table 5 gives summary information on the structure of the questionnaire data used in the regression analysis. A more detailed summary of task descriptions, reference performance times, and numbering is provided in Table 2.

Regression analysis of the performance data was done with the SAS [Ray et al., 1982] and STATLIB [Brelsford and Relles, 1981] software

Table 5. Combat crew summary for regression analysis.

Combat Crew ^a	Number of Respon- dents	Number of Symptom Complexes	Crew Position ^a	Tasks
lArtillery, gun	25	30	1Chief of section 2Gunner 3Assistant gunner 4Loader	1 2, 3 4, 5 6, 7, 8, 9, 10, 11
2Artillery, fire direction center	21	30	1Fire direction officer 2Horizontal control operator 3Computer	1, 2, 3 4, 5, 6 7, 8
3Armor, tank	34	30	1Tank commander 2Gunner 3Loader 4Driver	1, 2, 3, 4 5, 6, 7 8, 9
4Antiarmor, mounted TOW	36	40	1Squad leader 2Gunner 3Driver 4Loader	1, 2 3, 4 5 6, 7

^aNumbers refer to indices used in computer codes.

systems. Those software systems provide comprehensive diagnostic options that guide selection of the model appropriate for the questionnaire data. A discussion detailing the regression analysis procedure is given in Appendix F.

INPUT DATA

Since the fundamental response variable obtained from the question-naires was the estimated time t required to complete a task against a stated reference time \mathbf{t}_0 , the basic index chosen as a measure of performance was the ratio of the reference time to the estimated time $(\mathbf{t}_0/\mathbf{t})$ to perform a particular task when experiencing acute radiation symptoms. If we make the following index assignments, ignoring any particular

bSee Table 8 for task descriptions.

combat crew: i for respondent, j for task, and k for symptom complex, then $\mathbf{t_{ijk}}$, given in Appendix A. represents the performance time estimate provided by the *ith* respondent for the *jth* task, given the *kth* symptom complex; $\mathbf{t_{0j}}$ (given in Table 2) is the reference time for performing the *jth* task. Recalling from the response options provided in the questionnaire (discussed in Sec. 2 above), values for task performance are assigned based on the assumptions shown in Table 6.

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Table 6. Performance index.

Questionnaire Response	t _{Oj} /t _{ijk}
Could not do it at all (assumes $t_{ijk} = \infty$)	U
Increase in time (i.e., $t_{0j} < t_{ijk} < \infty$)	$0 < (t_{0j}/t_{ijk}) < 1$
No increase in time (assumes t ijk = t 0j)	1

In performing the regression analysis for tasks, values of the performance measure specified f the dependent variable include averaging over respondents. Averaging the data guarantees that the performance dependent variables for the task and positions lie between zero and one, but are not equal to either one or zero, shown in Appendix E. That condition makes it possible to apply the logit transformation for the dependent variable in modeling the data for the regression analysis. The logit model, which is a logarithmic transformation of the dependent variable, is attractive for application to the fractional type of data we have, since the relationships guarantee that all predicted performance values lie within the interval (0, 1).

For the jth task, the performance measure is the average over N respondents for a particular crew, i.e.,

$$\bar{P}_{jk} = \frac{1}{N} \sum_{i=1}^{N} \left(\frac{t_{0j}}{t_{ijk}} \right) ,$$
 (1)

where, based on the assumptions above, $0 < (t_{0j}/t_{ijk}) < 1$. Values of \overline{P}_{jk} are given in Appendix E, where $0 < \overline{P}_{jk} < 1$.

For a given crew position, where a crewmember may perform more than a single task (see Table 5), the measure of performance is assumed to be the ratio of the sum of reference task performance times to the sum of average estimated times to perform the tasks when experiencing acute radiation symptoms, or

$$\overline{P}_{k} = \frac{\sum_{j=1}^{J} t_{0j}}{\sum_{j=1}^{J} \overline{t}_{jk}}, \quad 0 < \overline{P}_{k} < 1, \quad (2)$$

where the estimated time to perform the task (with symptoms) is

$$\overline{t}_{jk} = \left(\frac{t_{0j}}{\overline{p}_{jk}}\right), \qquad 1 < \overline{t}_{jk} < \infty.$$
(3)

The \overline{P}_k values, given in Appendix E, are input for analyzing the relationships that predict individual performance for each crewmember position.

LINEAR REGRESSION MODELING

We limited regression analysis to linear models, assuming that performance can be expressed as some function of a linear combination of the factor (explanatory) variables, i.e., symptom severity levels. The six basic symptom complex variables are designated as follows:

 x_1 = Upper gastrointestinal distress (UG),

x₂ = Lower gastrointestinal distress (LG),

 x_3 = Fatigability and weakness (FW),

 x_{h} = Hypotension (HY),

 x_5 = Infection, bleeding, and fever (IB),

 x_6 = Fluid loss and electrolyte imbalance (FL),

where each x-variable takes on integer values (corresponding to severity level) from 1 to 5. The implicit assumption is made that, given one of the six symptom categories above, severity can be represented in integer multiples. Whether or not that assumption is precisely true was not determined with the linear regression models employed here. It would require complex generalized nonlinear regression analysis, which is beyond the scope of the present effort. Moreover, limitation on the number of symptom complexes allowed in the questionnaires and the selection guidelines followed, based on dose and time considerations, evolved a data set that probably lacks the quantity and type of information required for such an analysis.

Considering only 30 to 40 complexes and possibly a large number of independent parameters p, would place a severe limitation on the number of degrees of freedom available (30 to 40 minus p). More balance in the data is also required, and entails expanding the variety of severity levels across symptom complexes. The symptom complexes selected for the combat crew questionnaires and the data that the present analysis is based on, favors the UG, LG, and FW symptom categories where severity level integers that are greater than one appear more frequently than HY, IB, and to a lesser extent, FL.

In addition to the data limitations and additional complexity required, we did not employ nonlinear regression modeling because we judged that the data could be reasonably represented by a linear model. That model may be expressed as follows.

If performance measure is designated by P_k , which corresponds to the kth symptom complex, e.g., for either crewmember position \overline{P}_k or task \overline{P}_{jk} , the linear regression model can be expressed as

$$P_k = x_k'\beta + \varepsilon_k$$
, $1 \le k \le K$, (4)

where $\mathbf{x}_k' = (1, \mathbf{x}_{k1}, \mathbf{x}_{k2}, \dots, \mathbf{x}_{k6})$ is a vector of integers $(1 \le \mathbf{x}_{k\ell} \le 5)$ denoting symptom severity level for the kth symptom complex and ℓth symptom category. The weight $\beta' = (\beta_0, \beta_1, \dots, \beta_6)$ is a vector of regression coefficients β_ℓ that are estimated. Both \mathbf{x}_k' and β' (transpose of β) each contain seven (p = 7) components corresponding to the six symptom categories discussed above plus the intercept. If additional parameters are to be estimated such as may be required for quadratic models that include squared $(\mathbf{x}_{k\ell}^2)$ and cross-product $(\mathbf{x}_{km}\mathbf{x}_{kn})$ terms, then the vector lengths may be larger than seven.

Linear quadratic model forms were applied to the data to investigate how well a prediction relationship, including squared and cross-product terms, could represent the data. Based on that analysis (discussed in Appendix F, "Transforming Factor Variables"), we concluded that a quadratic form cannot be developed to model the data for predicting individual performance. The main problem uncovered from the regression diagnostics was multicollinearity (i.e., linear combinations formed by the independent variables). Certain quadratic and cross-product terms form linear combinations with the original six symptom categories, resulting in a noninvertible (X'X) matrix. That difficulty arises primarily from the lack of balance in the data set mentioned above.

In linear regression modeling, a usual assumption is that the error terms $\varepsilon_k = P_k - x_k'\beta$ (actual values minus conditional mean values) are independent, have a common variance, and are normally distributed with a mean equal to zero, i.e., var $(\varepsilon_k) = \sigma^2$. The present regression analysis generally indicated the residuals to be normally distributed.

Writing the linear regression model in matrix notation, we have

$$Y = X\beta + \varepsilon$$
, (5)

where

$$X = \begin{bmatrix} x_1 \\ x_2 \\ \vdots \\ x_k \end{bmatrix} = \begin{bmatrix} 1, x_{11}, x_{12}, & \dots & x_{16} \\ 1, x_{21}, x_{22}, & \dots & x_{26} \\ \vdots & \vdots & & \vdots \\ 1, x_{k1}, x_{k2}, & \dots & x_{k6} \end{bmatrix},$$

$$Y = \begin{bmatrix} P_1 \\ P_2 \\ \vdots \\ P_k \end{bmatrix}, \quad \beta = \begin{bmatrix} \beta_0 \\ \beta_1 \\ \vdots \\ \beta_6 \end{bmatrix}, \quad \varepsilon = \begin{bmatrix} \varepsilon_1 \\ \varepsilon_2 \\ \vdots \\ \varepsilon_k \end{bmatrix}.$$

The β -parameter estimates are given by

$$\hat{\beta} = (X'X)^{-1}X'Y , \qquad (6)$$

and the covariance of β is given by

$$\operatorname{cov} \hat{\beta} = \hat{\sigma}^2(X^*X)^{-1} , \qquad (7)$$

where the estimate of the variance of the errors (or mean square error of residuals) for p parameters is

$$\hat{\sigma}^2 = \frac{(Y - X\hat{\beta})'(Y - X\hat{\beta})}{K - p}$$
 (8)

CONFIDENCE BOUNDS

Two types of confidence bounds can be constructed about the regression line for predicted performance values (Appendix F, "General Linear Model"). One is based on the variance $\hat{\sigma}_m^2$ of the expected value of performance for any given symptom complex \mathbf{x}_k , which reflects the uncertainty in the β -parameter estimates; $\hat{\sigma}_m^2$ is often referred to as the variance of the predicted value of the conditional mean. Another is based on the

variance $\hat{\sigma}_0^2$ of the input performance data relative to the expected values of performance, i.e., relative to the regression line. Often, $\hat{\sigma}_0^2$ is referred to as the variance of the predicted value of a further observed value, i.e., additional performance input data.

Upper and lower 95 percent confidence bounds for the expected performance values predicted by the regression relationships are given as

$$L_{95,m} = x_k^! \hat{\beta} \pm 2.08 \hat{\sigma}_m$$
 (9)

where 2.08 is the 95 percent cutoff of the t-distribution for a sample size of 30 or 40 (i.e., the number of symptom complexes used in the analysis). The quantities \mathbf{x}_k^{\prime} and \mathbf{x}_k are row and column vectors, respectively, each containing unity for the first element followed by six integer values $(\mathbf{x}_1, \mathbf{x}_2, \ldots, \mathbf{x}_6)$ designating symptom severity levels for a kth symptom complex.

The prediction of a further observation for a given symptom complex \mathbf{x}_k^{\bullet} would also have a value of $\mathbf{x}_k^{\bullet}\hat{\boldsymbol{\beta}}$. However, the variance is

$$\hat{\sigma}_{0}^{2} = \hat{\sigma}_{m}^{2} + \hat{\sigma}^{2}$$

$$= \hat{\sigma}^{2} [1 + x_{k}^{*} (X^{*}X)^{-1} x_{k}] .$$
(10)

Upper and lower 95 percent confidence bounds for a further observed value are

$$L_{95,0} = x_k \hat{\beta} \pm 2.08 \hat{\sigma}_0^2$$
 (11)

The $L_{95,0}$ confidence bounds will be wider than the $L_{95,m}$ confidence bounds and should contain about 95 percent of the observed values (input data) whereas a smaller percentage of the observed values will be included within the $L_{95,m}$ bounds.

CORRELATION OF RESPONSES

Estimates of the effects of correlation between responses from the questionnaire data were made using STATLIB [Brelsford and Relles, 1981]. Analysis of the data (discussed in Appendix F, "Correlation among Mode! Error Terms") showed significant positive correlation with estimated correlation coefficients ranging from $\rho=0.2$ to 0.4. The correlation coefficient ρ is a measure of individual response bias of the respondents. So, for example, with 35 individuals, each providing judgments of performance on a common set of 30 different symptom complex descriptions, some will offer consistently low values, some consistently high values, and others somewhere in between. On the other hand, purely independent responses would result in a zero correlation ($\rho=0$).

It can be shown theoretically that least squares linear regression yields β -parameter estimates $(\hat{\beta})$ that are unbiased. Therefore, ordinary least squares regression analysis is suitable for estimating \$\beta\$. However, when $\rho \neq 0$, estimates of the variance σ^2 are biased downward (see Appendix F. "Correlation among Model Error Terms"). Because of the strong assumption of normality for the joint distribution of 30 error terms (i.e., jointly correlated with one another) required by STATLIB, it was not possible to precisely determine the extent of the downward bias with the generalized least squares regression model package. That package was not designed to give robust estimates of σ for the expanded data set (i.e., when not averaged over individual respondents) from the questionnaires. Furthermore, we are unaware of any existing package designed to develop reliable estimates of σ for the kind of data set developed from the questionnaires. However, from theoretical considerations an inflation factor can be developed to estimate an adjustment from the upper and lower confidence limits. Since it can be shown that o, as determined by ordinary least squares regression (which assumes $\rho \neq 0$), has a downward b is by a factor of $\sqrt{1-\rho}$, multiplication of $\hat{\sigma}$ by $1/\sqrt{1-\rho}$ corrects the bias when $\rho \neq 0$. Since we estimated values ranging from ρ = 0.2 to 0.4. a factor of from 1.12 to 1.29 can be used to increase the upper and lower confidence limits,

$$L_{95,m}(\text{adjusted}) = \chi_{k}^{\dagger} \hat{\beta} \pm \left(\frac{1}{\sqrt{1-\rho}}\right) 2.08 \hat{\sigma}_{m},$$

$$L_{95,0}(\text{adjusted}) = \chi_{k}^{\dagger} \hat{\beta} \pm \left(\frac{1}{\sqrt{1-\rho}}\right) 2.08 \hat{\sigma}_{0}.$$
(12)

The magnitude of such an adjustment is not large; it extends the upper and lower bounds by about 12 to 30 percent.

INDIVIDUAL PERFORMANCE PREDICTIONS

Predictions of individual performance were made using the logit form of the linear regression model. Preliminary analyses were performed on the data using two alternative forms of the linear regression model, and with seven first power terms (intercept plus six symptom categories) for the independent variables (\mathbf{x}_k^i) . The analyses indicated no significant difference between the two forms in fitting the data, one where the logit transformation, \mathcal{U}_{i} [P/(1 - P)] is made on the dependent variable (performance), and the other where it is not made. However, predictions of performance using the logit form guarantee that all predicted performance values including the upper and lower confidence limits lie within the interval (0, 1), which is consistent with the input data set. Predictions using the form where the dependent variable is not transformed can yield values outside that interval. Accordingly, the logit form was applied to the data for the regression analysis.

Making the logit transformation of the dependent variable $\mathbf{F}_{\mathbf{k}}$ (performance response) gives the form

$$\mathcal{L}_{\kappa} \frac{P_{k}}{1 - P_{k}} = \tilde{\kappa}_{k}^{*} \beta + \varepsilon_{k} , \qquad 1 \le k \le K , \qquad (13)$$

where $\Omega_k[P_k/(1-P_k)]$ was regressed on the \mathbf{x}_k^t variables to obtain estimates $\hat{\boldsymbol{\beta}}$ of the $\boldsymbol{\beta}$ -parameters. Using the data given in Appendix E, regression parameters were obtained for crewmember positions given in Tables 7 through 10 for the gun, FDC, tank, and TOW crews, respectively. The

Table 7. Gun crew regression parameters.

9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	1110	HIEF UF SECTION	Z		GUNNER	
SVIATOM	BETA PARAMETER	STANDARD	STUDENT	BETA PAKAMFIER	STANDARD FRRUR	STUDENT
	2,808356		10.916	474696 F		15 327
	-0.225827		3	14641	2 10 1 2 4 0 1 5 4 0 1 5 4 0 1 5 4 0 1 5 6	1000 NO
LOWER GASTRO	-0.365274		•	17071		10 0 0 N
FATIGUE/WEAK	-0.1A1312		305.7-	•	111531.0	074.0
HYPOTENSION	-0.066167		015.0-	•	100000000000000000000000000000000000000	7 / 0 - 7
_	-0.352418	0.158464	•	•	7000 7000	16.11
FLUID LUSS	-0.434346		-4.686	-0.439715	0.077863	-5.647
	SAILABED	11 D 12 + C		•		
	3				3	
		= 0.559175		RMS ERKOK		
		,		1610	F 64	
	ASSI	SSISTANT GUNNER	x		LUADER	
		4	STUDENT	BETA	STANDARD	STUDENT
MULAWAS	PARAMETER	ERKOK	-	PARAMETER	FARUR	-
INTERCEPT	3.113833	0.190724	16.326	7.518392	25678 0	
HPPER GASTRO	-0.174983	e	-3.658	-0-146/18	0.0000000	
LOWER GASTRO	-0.366702	c	626-5-	-0.293360	0.0000 0.0000	
FAT IGUE / WE AK	-0.256687	C	-5.556	-0.300109	0.045670	100.00
HYPOTENSION	-0.170065	ċ	-1.354	PASSP1.0-	0.074187	, 1
INFECT/BLEED	-0.215799	0.117	-1.837	0.785970	01000	n .
FLUID LUSS	-0.435395	0.068709	-6.337	-0.4398AB	05304	• œ
	CHARLE S	73000	•	0		
	AMS FRRDR			K SUCAKED		
		1 1 1 M		7 2 2	= 0.194126 = 27	

Table 8. FDC crew regression parameters.

	-					
	FTRE DI	DIRECTION OFF	OFFICER	HORIZUNTAL	CANTROL	UPERATUR
SYMPIOM	BETA Parameter	STANDARU	STIIDENT	BETA PAKAMETEK	STANDARD	STUDENT
INTERCEPT	3,442455	0.346776	166.6	2.461669	19185	12.831
LOWER GASTRO	-0.674508	0.067091	-3.419	•	3711	-5.108
	CACADO - 01	0.107688	-5.101	778778-0-	99860	-3.682
	-0.069726	.08400	-0.830	.0.097654	74647	-2.101
AND LENGTON	-0.168636	7	-0.965	-0.134423	39866	٠, ~
INFECTIVBLEED	.2409	.21358	-1.128	-0.097338	11817	•
- LUIU LUSS	-0.484706	0.124928	-3.880	-0,320938	9690	9
	R SUNARED	= 0.7757) ()	
	AC FROOD	· C		מאאסני	/40°0	
	7 C	101/540/101		ž (
	1	۱		190	63	
		COMPUTER				
SYMPION	BFIA PARAMETER	STANDARD	STUDENT			
INTERCFPT	2.875132	0.189877	15, 102			
UPPER GASTRO	231	0.034736	コーマ・マー			
LOWER GASTRO	-0.422774	0.092693	5			
FAT IGUE /WEAK	-0.073737	0.045997	•			
HYPUTENSTON	-0.214650	0.095642	-2.244			
INFECT/BLEED	-0.052900	0.116950	-0.452			
FLUID LOSS	-0.352097	0.068404	14			
	R SQUARED #	CC				
		~~				

Table 9. Tank crew regression parameters.

	TANK	COMMANDER			GUNNER	
SYMPTOM	BETA PARAMETER	STANDARU ERROR	STHEENT	BETA PARAMETER	STANDARD	STUDENT T
TNTERCEPT	3,739408	0.252659	14.800	4.150500	0.240619	17.249
HPPEP GASTRO	-0.304504	940	-6.239	-0.307994	0.046553	-6.616
DWER GASTRU	960667-0-	0.123342	-4.046	-0.583071	0.117464	-4.904
FATIGUE/WEAK	-0.237838	.061	-3.886	-0.183404	0.058288	-4.146
HYPOTENSTON	-0.179232	127	-1.408	-0.212194	0,121226	-1.750
TNFECT/BLEFD	•	,	-0.282	0.032174	\rightarrow	.21
FLUID LOSS	-0.476924	.	-5.240	-0.544823	0.086684	-6.285
	HIARED	= 0.9110		•		
	RMS FRROR	= 0.333085		KMS ERKOR UGF	= 0,317712	
		LOADER			DRIVER	·
		< (STUDENT	RETA	STANDARD	STUDENT
SYMPION	PARAMETER	ERKOR	-	PAKAME IER	* X X X	-
TNTEQUEPT	3,353334	0.210557	i i	3.815458	0.226685	
HPPER GASTRO	-0.225547	0.040737	-5.537	-0.2107A2	0.043857	
DWFR GASTRO	-0.448A39			-0.506874	0.110462	
FATIGUE/WEAK	-0.300574	0.051006	1	-0.309476	0.054913	-5.636
TYPOTENSTON		٠		-0.184998	0.114206	
TNEECT/BLEFU	0.006172	C	-0.048	-0.012518	0.139621	-0.048
FLUIN LUSS	-0.520462	C	-6.861	-0.439561	0.081664	-5.363
	R SUILARED	= 0.9367		R SAUAKEL	= U.9729	
	MS FK	_		RMS CRKOK) 	a.
	106	25		という	10	

Table 10. TOW crew regression parameters.

の対象を含めている。

	ns	SUIIAN LEADER			GUNNER	
SYMPION	BF TA PARAMETER	STANDARU	STUDENT	RETA PARAMFIFK	STANDARD	STUDENT
TNTERCEPT	3.861755	0.277212	15,929	3.568425	27692	12.806
IPPER GASTRU	-0.229213	0.034150	31	-0.242815	0530	-4.573
UMER GASIRO	-0.2+8831	0.136572	-1.969	-0.233592	0 136431	-1.712
FAT IGUF/WEAK	-0.348488	0.064496	-5.716	-0.377513	0.064430	-5. A.O
47 PUTENSTON	0.051657	0.132217	0.391	0.001518	0 132081	0.011
INFECT/BLEFD	-0.396030	0.111644	-3.547	4100000-0-	0.111528	-3.587
LUIN LOSS	-0.507480	700860°u	-5.178	-0.462964	0.097901	-4.933
	R SUNARED	9598-0 =		S SOUARED	10.47.21	
	RMS FRROR			- 5) :	
	NGF				> ~	
		101750				
		עה 1 "בה			LUAUFR	
	BEIA	STANDAPD	STHOFMT	RETA	STANDARD	STIINE 1
SYMPIOM	PARAMETER	ERROR	.	PARAMETER	FRROR	-
TWTERCEPT	5,122940	0.324222	15.801	4.261434	016666 0	14.542
PPER GASTRU	-0.2440A	0.062164	-3.942	-0.25126b	720050 0	-0.485
UWEP GASTRU	-0.299380	0.159732	-1.674	-0.265417	0.143963	-1.844
ATIGUF/WEAK	-0.486197	0.075434	-6.445	-0.523545	0.067987	449-1-
HYPOTENSION	0.127268	0.154679	0.873	0.057344	2759710	0.411
NFECT/BLEFO	-0.508780	0.150577	-3.896	-0.390862	0.117686	, M
LUIP LUSS	-0.612157	0.114622	-5,341	-0.627272	0.103306	
		= 0.8723		K. SOUAKED	# T C O	
	S.	C		MS ERKOR	; -	
	L OC	35 11				

standard error of the β 's listed in the tables is the square root of the diagonals of the variance-covariance matrix of β

$$\sqrt{(\cos \hat{\beta})_{ii}} = \hat{\sigma} \sqrt{(X'X)_{ii}^{-1}}. \tag{14}$$

Also given in those tables, for each crew type and symptom category, is a Student's t-statistic. That statistic is the ratio of the estimated β -parameter to the standard error. The Student's t values are a measure of each symptom category's importance. For the data analyzed with 23 to 33 degrees of freedom, values of |t| less than about two indicate that the symptom category becomes nonsignificant. The regression analysis indicates that all crews considered both the FL and UG symptom categories as important (i.e., where $|t| \ge 2$), with FL the most important. The HY and IB categories were considered the least important compared with the others. Table 11 is a summary by crew position of the symptom categories judged to be the least significant (i.e., where $|t| \le 2$).

The $\ensuremath{\text{R}}^2$ values are a global measure of goodness of fit of the data given by

$$R^{2} = 1 - \frac{\sum_{k=1}^{K} (P_{k} - \hat{P}_{k})^{2}}{\sum_{k=1}^{K} (P_{k} - \overline{P})^{2}},$$
 (15)

where P_k and \widehat{P} are performance input and average performance input data, respectively, and \hat{P}_k are predicted values. The R^2 values are all quite large, indicating a good fit of the regression model with the data. The RMS error is the square root of the estimated variance of the residuals, indicated in the text above as $\widehat{\sigma}$.

The regression diagnostics do not indicate any significant problem with collinearity (a linear combination formed by two independent variables). The seven eigenvalues of the normalized (X'X) matrix are listed

Table 11. Least significant symptom categories.

		Sym	otom	Catego	Category	
Crew	Crew Position	LG	FW	нү	IB	
Gun	Chief of section Gunner Assistant gunner Loader			x √ √	√	
FDC	Fire direction officer Horizontal control operator Computer		× ,	× ✓	√ x x	
Tank	Tank commander Gunner Loader Driver			√ √ √	x x x x	
TOW	Squad leader Gunner Driver Loader	√ √ √		x x x x		

NOTE:
$$x = Student's |t| < 1$$
,
 $\sqrt{=1} \le Student's |t| < 2$.

in Table 12 with the *condition index*, which is obtained by dividing the square root of the top eigenvalue $\sqrt{6.203}$ by the square root of the others (including itself). All values of the condition index are much less than about 30, which indicates no significant collinearity relationship.

Applying the inverse transformation to the logit regression relationship yields the formula for predicting expected values of performance \hat{P}_k for the kth symptom complex given by

$$\hat{P}_{k} = \frac{1}{1 + \exp(-x_{k}'\hat{\beta})}.$$
 (16)

Table 12. Eigenvalue condition indexes.

Eigenvalue	Condition Index
(v _i)	$\left(\sqrt{v_1/v_i}\right)$
6.203	1.0
0.282040	4.690
0.215428	5.366
0.134011	6.803
0.073825	9.166
0.051828	10.940
0.039971	12.457

The upper and lower 95 percent confidence bounds for the predicted expected values of performance are given by

$$UL_{95,m} = \frac{1}{\{1 + \exp \left[-\left(\frac{x_{t}}{\beta} + 2.08\hat{\sigma}_{m}\right)\right]\}},$$
 (17)

and

$$LL_{95,m} = \frac{1}{\{1 + \exp \left[-\left(x_k^{\dagger} \hat{\beta} - 2.08 \hat{\sigma}_m\right)\right]\}}$$
 (18)

The upper and lower 95 percent confidence bounds for further predicted observed values of performance are given by

$$UL_{95,0} = \frac{1}{\{1 + \exp \left[-\frac{(x_k'\hat{\beta} + 2.08\hat{\sigma}_0)\}}{}\right]\}},$$
 (19)

and

$$^{LL}_{95,0} = \frac{1}{\{1 + \exp \left[- \left(x_{k}^{\dagger} \hat{\beta} - 2.08 \hat{\sigma}_{0}^{\dagger} \right) \right] \}}$$
 (20)

Tables 13 through 27 list the predicted expected and actual (observed) data performance values for crewmember positions, the upper and lower 95 percent confidence bounds $\mathrm{UL}_{95,m}$ and $\mathrm{LL}_{95,m}$, for each of 30 symptom complexes $(\mathbf{x}_k^{\mathsf{T}})$ for the artillery (gun and FDC) and tank crews; and each of 40 symptom complexes for the TOW crew. The listing order in the tables is arranged from highest to lowest value of performance predicted by the regression formula. The values of $(1-P_k)$ termed performance degradation are also listed.

Figures 17 through 31 are plots of the crewmember performance data given in Tables 13 through 27. Performance P_k is plotted against $(1 - P_k)$, which yields the straight line shown. For purposes of illustration, values of performance predicted by the regression relationship lie along the straight line at coordinates $[(1 - \hat{P}_k), \hat{P}_k]$ for each kth symptom complex. The actual data values are given by the asterisks, which have coordinates [(1 - \hat{P}_{ν}), P_{ν}]. The unevenly spaced tick marks along the top edge of the abscissa correspond to each of the ordered symptom complexes listed in Tables 13 through 27. The two sets of error bars each designate upper and lower 95 percent confidence bounds for the prediction of performance along the regression line. The solid line bars are for the expected mean performance values that correspond to the $UL_{95,m}$ and $LL_{95,m}$ bounds. The wider dotted line bars are for further data observations that correspond to the ${\rm UL}_{95.0}$ and ${\rm LL}_{95.0}$ bounds. The plots indicate a substantial portion of the data included even within the narrower predicted mean value confidence bounds. A much larger portion of the data is included within the wider 95 percent confidence bounds as would be expected for further observed values of performance (i.e., additional data). Expanding the confidence limits by 12 to 30 percent by multiplying them by the inflation factor $1/\sqrt{1-\rho}$ to account for correlated response data, where estimates are $\rho = 0.2$ to 0.4, would include essentially all of the data. However, the extent to which variation in response data about the regression line can be attributed to either nonlinearities that might exist in the symptom severity levels (integer values 1 through 5 were assumed) or simply variations in performance judgment, cannot be ascertained for reasons previously discussed (see p. 59).

Table 13. Gun crew individual performance: chief of section.

	·		·			
	SYMPTOM	PERFORMANCE	PREDICTED	ACTUAL	CONFIDENCE	LEVELS
	CUMPI EX	DEGRADATION	VALUE	VALUE	LUW 95%	HIGH 95%
1	112111	v.2685	0.73145	0.81306	0.67478	0.79134
Š	211111	0.2774	0.72256	0.67100	0.66149	0.78126
3		0.3057	0.69432	0.81107	0.63454	0.77626
4	311111	0.3249	0.67510	0.69600	0.61140	0.74819
5	114111	0.3455	0.65454	0.69100	0.57861	0.73302 0.72334
5	213111	0,3556	9.64441	0.60500	0.59741	0.68879
7	312111	0.3659	0.63415	0.61200	0.58877	
Ą	411111	0.3762	0.62376	0.53000	0.54979	0.67726 0.69237
9	113121	0.3851	0.61490	0.55500	0.52196	0.70016
10	123111	0.3881	0.61185	0.64200	0.52799	0.68958
11	313111	0.4088	0.59115	0.65800	0.54948	0.63155
12	412111	0.4196	0.58035	0.55700	0.52531	0.63347
13	413111	0.4643	0.53567	0.55900	0.48626	0.58438
14	224111	0.4880	0.51199	0.36200	0.43957	0.58391
15	414111	0.5096	0.49040	0.49100	0.42870	0.55239
16	313112	0.5164	0.48360	0.46900	0.43661	0.53088
17	513:11	0.5207	0.47928	0.51500	0.41373	0.54555
18	521111	0.5214	0.47862	0.53000	0.37414	0.58501
19	314112	0.5614	0.43858	0.39400	0.39014	0.48822
20	514111	0.5657	0.43432	0.40900	0.36244	0.50908
21	414112	0.6160	0.38397	0.36800	0.33381	0.43672
55	515311	0.6406	0.35942	0.38700	0.25578	0.47812
23	314113	0.6640	0.33598	0.25200	0.26982	0.40927
24	525111	0.6923	0.30772	0.28700	0.24104	0.38348
25	315113	0.7032	0.29680	0.25502	0.23130	0.37188
56	535111	0.7642	0.23577	0.26096	0.16219	0.32966
27	334231	0.7882	0.21182	0.22097	0.13424	0.31762
58	515431	0.7940	0.20603	0.15499	0.12909	0.31245
59	415314	0.8396	0.16043	0.15499	0.09850	0.25049
30	515223	0.8498	0.15020	0.28900	0.10603	0.20850

Table 14. Gun crew individual performance: gunner.

	SYMPTOM	PERFORMANCE	PREDICTED	ACTUAL	CONFIDENC	E LEVELS
	COMPLEX	DEGRADATION	VALUE	VALUE	LOW 95%	HIGH 95
1	211111	0.1680	0.83202	0.82807	0.79560	0.8630
5	112111	0.1821	0.81787	0.81593	0.78126	0.8494
3	311111	0.1894	0.81061	0.87303	0.77206	0.8439
4	411111	0.2128	0.78718	0.73100	0.74097	0.8269
5	113111	0.2215	0.77851	0.85705	0.73711	0.8148
6	312111	0.2299	0.77012	0.70900	0.74039	0.7973
7	213111	0.2479	0.75213	0.78600	0.71957	0.7821
R	113121	0.2541	0.74593	0.70000	0.68077	0.8015
9	412111	0.2567	0.74326	0.72800	0.70586	0.7773
10	114111	0.2666	0.73341	0.73000	0.67723	0.7827
1 1	313111	0.2761	0.72391	0.78194	0.69445	0.7515
12	123111	0.2901	0.70989	0.70700	0.64719	0.7654
13	413111	0.3063	0.69374	0.69400	0.65733	0.7278
4	521111	0.3101	0.68988	0.69800	0.60807	0.7613
15	513111	0.3382	0.66180	0.64300	0.61020	0.7098
16	414111	0.3606	0.63938	0.60000	0.58994	0.6860
17	313112	0.3719	0.62814	0.63100	0.59030	0.6644
18	224111	0.3767	0.62330	0.54000	0.56445	0.6787
9	514111	0.3950	0.60500	0.59200	0.54336	0.6634
30	314112	0.4306	0.56937	0.50900	0.52782	0.6099
21.	414112	0.4668	0.53319	0.53500	0.48740	0.5784
55	314113	0.5400	0.45998	0.41700	0.39545	0.5258
23	515311	0.5412	0.45884	0,53400	0.35964	0.5614
24	525111	0.5450	0.45504	0.40600	0.38636	0.5254
?5	315113	0.6000	0.40001	0.40400	0.33410	0.4697
26	334231	0.6313	0.36874	0.38400	0.26910	0.4809
27	535111	0.6323	0.36771	0.41400	0.28215	0.4625
8	515431	0.6678	0.33221	0.27500	0.23704	0.4433
29	515223	0.7410	0.25903	0.39900	0.20005	0.3282
50	415314	0.7922	0.20784	0.16995	0.14088	0.2956

Table 15. Gun crew individual performance: assistant gunner.

	SYMPTOM	PERFORMANCE	PREDICTED	ACTUAL	CONFIDENC	E LEVELS
		DEGRADATION	VALUE	VALUE	LOW 95%	I I
1	211111	0.1917	0.80830	0.80298	0.7/312	0.83916
5	112111	0.2112	0.78885	0.78801	0.75325	0.82039
3	311111	0.2135	0.78651	0.83202	0.74988	0.81906
4	411111	0.2370	0.76296	0.74895	0.71963	0.80155
5	113111	0.2571	0.74288	0.82201	0.70301	0.77903
6	312111	0.2596	0.74039	0.70000	0.71215	0.76656
7	213111	0.2838	0.71623	0.71100	0.68518	0.74536
8	412111	0.2865	0.71352	0.70900	0.67860	0.74612
9	113121	0.3005	0.69952	0.67500	0.63721	0.75528
10	114111	0.3091	0.69086	0.69000	0.63771	0.73943
11	313111	0.3120	0.68802	0.76296	0.66032	0.71443
12	123111	0.3331	0.66688	0.67000	55808.0	0.72080
13	521111	0.3390	0,66096	0.65800	0.58652	0.72821
14	413111	0.3417	0.65833	0.65200	0.62462	0.69052
15	51311!	0.3726	0.62736	0.58200	0.58029	0.67212
16	414111	0.4015	0.59849	0.56100	0.55349	0.64189
17	313112	0.4121	0.58794	0.57500	0.55358	0.62147
18	224111	0.4250	0.57504	0.50100	0.52169	0.62670
19	514111	0.4343	0.56567	0.54400	0.51035	0.61940
20	314112	0.4753	0.52467	0.47900	0.48767	0.56141
21	414112	0.5091	0.49095	0.49000	0.45066	0.53136
22	515311	0.5628	0.43718	0.51500	0.35067	0.52769
23	314113	0.5834	0.41663	0.37100	0.36133	0.47411
24	525111	0.5888	0.41116	0.37000	0.35245	0,47251
25	315113	0.6441	0.35588	0.35900	0.30065	0.41522
95	535111	0.6739	0.32610	0.37700	0.25502	0.40609
27	334231	0.6815	0.31845	0.32100	0.23722	0,41251
28	515#31	0.6930	0.30698	0.25200	0.22618	0.40155
29	515223	0.7701	0.22988	0.36100	0.18168	0.28631
30	415314	9.8060	0.19404	0.16097	0.13729	0.26718

Table 16. Gun crew individual performance: loader.

	SYMPTOM	PERFORMANCE	PREDICTED	ACTUAL	CONFIDENC	E LEVELS
	COMPLEX	DEGRADATION	VALUE	VALUE	LUW 95%	HIGH 95%
1	211111	0.3186	0.68137	0.65000	0.64467	0.71595
5	311111	0.3513	0.64871	0.65300	0.61163	0.68408
3	112111	0.3528	0.64718	0.69000	0.61091	0.68184
4	411111	0.3854	0.61459	0.56500	0.57241	0.65518
5	312111	0.4223	0.57768	0.55600	0.55078	0.60412
6	113111	0.4239	0.57605	0.69700	0.53813	0,61309
7	412111	0.4585	0.54154	0.52000	0.50974	0.57300
8	213111	0.4601	0.53988	0.54200	0.51136	0.56814
9	113121	0.4824	0.51764	0.47300	0.46334	0.57154
10	521111	0.4934	0.50664	0.55000	0.44548	0.56760
11	123111	0.4967	0.50330	0.50200	0.45435	0.55220
12	313111	0.4967	0.50329	0.55900	0.47895	0.52760
13	114111	0.4984	0.50162	0.45200	0.45566	0.54755
1 "	413111	0.5333	0.46666	0.49600	0.43860	0.49492
15	513111	0.5696	0.43038	0.3960v	0.39357	0.46798
16	313112	0.6051	0.39490	0.38700	0.36933	0.42107
17	224111	0.6067	0.39326	0.33000	0.35432	0.43361
18	414111	0.6068	0.39325	0.37000	0.35984	0.42768
19	514111	0.6412	0.35884	0.36200	0.32029	0.39930
20	314112	0.6741	0.32589	0.34460	0.30128	0.35149
21	414112	0.7055	0.29451	0.29500	0.26924	0.32112
22	314113	0.7626	0.23740	0.22305	0.20636	0.27153
23	525111	0.7639	0.23613	0.22794	0.20327	0.27259
24	515311	0.7811	0.21892	0.24899	0.17480	0.27072
25	535111	0.8126	0.18740	0.18694	0.15008	0.23148
26	315113	0.8126	0.18740	0.17902	0.15963	0.21874
27	334231	0.8236	0.17639	0.18801	0.13517	0.22671
28	515431	0.8742	0.12576	0.10997	0.09449	0.16548
29	515223	0.8995	0.10047	0.13401	0.08166	0.12314
30	415314	0.9202	0.07980	0.06998	0.05925	0.10679

Table 17. FDC crew individual performance: fire direction officer.

						
	SYMPTUM	PERFORMANCE	PREDICTED	ACTUAL	CONFIDENC	E LEVELS
	COMPLEX	DEGRADATION	VALUE	VALUE	LOW 95%	HTGH 95%
1	112111	0.1606	0.83943	0.90602	0.78381	0.88298
ڿ	113111	0.1701	0.82991	0.94401	0.77259	0.87512
3	114111	0.1802	0.81980	0.77903	0.74668	0.87534
4	211111	0.1832	0.81683	0.70200	0.75176	0.86784
5	213111	0.2051	0.79495	0.80799	0.74763	0.83548
6	113121	0.2069	0.79315	0.70400	0.69666	0.86483
7	311111	0.2201	0.77989	0.77799	0.70899	0.83753
Я	312111	0.2322	0.76781	0.69300	0.71870	0.81046
9	313111	0.2449	0.75510	0.78701	0.71025	0.79495
10	123111	0.2573	0.74269	0.77903	0.64507	0.82083
11	411111	0.2619	0.73808	0.69700	0.65112	0.80969
12	412111	0.2756	0.72438	0.76692	0.66058	0.78023
13	413111	0.2898	0.71025	0.82201	0.65246	0.76188
14	414111	0.3043	0.69569	0.69800	0.62048	0.76170
15	224111	0.3185	0.68150	0.48200	0.59113	0.76006
16	513111	0.3391	0.66088	0.60900	0.57668	0.73595
17	313112	0.3450	0.65503	0.65000	0.59534	0.71021
18	514111	0.3549	0.54508	0.62500	0.54795	0.73165
19	314112	0.3609	0.63911	0.54900	0.57498	0.69864
20	414112	0.4153	0.58471	0.62700	0.51199	0.65392
21	521111	0.4300	0.56998	0.59700	0.42644	0.70264
55	515311	0.4525	0.54748	0.50900	0.38453	0.70085
23	314113	0.4783	0.52169	0.42800	0.41659	0.62490
24	315113	0.4957	0.50427	0.47300	0.39196	0.61615
25	525111	0.4993	0.50072	0.49400	0.38934	0.61202
56	515431	0.6130	0.38696	0.35300	58855.0	0.57320
27	535111	0.6276	0.37238	0.41100	0.24031	0.52661
28	334231	0.6557	0.34430	0.37000	0.20021	0.52407
59	515223	0.7008	0.29917	0.42400	0.19957	0.42227
30	415314	0.7377	0.26231	0.27100	0.14332	0.43034

Table 18. FDC crew individual performance: horizontal control operator.

	SYMPTOM	PERFORMANCE	PREDICTED	ACTUAL	CONFIDER	CE LEVELS
		DEGRADATION	VALUE	VALILE	LUW 95%	HTGH 95%
1	112111	0.2352	0.76477	0.79803	0.72642	0.79951
Ş	211111	0.2522	0.74782	0.69700	0.70539	0.78600
3	113111	0.2531	0.74687	0.86105	0.70708	0.78279
a	113121.	0.2721	0.72795	0.65300	0.66837	0.78040
5	114111	0.2721	0.72789	0.74307	0.67782	0.77277
6	311111	0.2895	0.71047	0.67400	0.66602	0.75120
7	213111	0.2907	0.70930	0.69200	0.67763	0.73904
Я	312111	0.3100	0.68998	0.68500	0.65869	0.71962
9	123111	0.3257	0.67628	0.69300	0.61797	0.72959
10	411111	0.3300	0.66997	0.67200	0.61777	0.71830
11	313111	0.5313	0.66871	0.64400	0.64002	0.69620
12	412111	0.3520	0.64803	0.69300	0.60925	0.68495
13	413111	0.3746	0.62545	0.67200	0.59029	0.65933
14	224111	0.3895	0.61051	0.46100	10.5578A	0.63793
15	414111	U.3977	0.60231	0.59600	0.55715	0.64579
16	313112	0.405A	0.59422	0.62400	0.55978	0.62776
17	513111	0.4199	0.58009	0.53300	0.53122	0.62743
18	314112	0.4295	0.57048	0.55800	0.53365	0.60654
19	514111	0.4439	0.55613	0.55000	0.50034	0.61055
50	521111	0.4567	0.54329	0.55400	0.46350	0.62092
21	414112	0.4765	0.52353	0.56900	0.46286	0.56788
55	314113	0.5093	0.49072	0.45300	0.43255	0.54915
23	315113	0.5336	0.46636	0.43900	0.40440	0.52937
24	515311	0.5352	0.46480	0.44000	0.37598	0.55592
25	525111	0.5540	0.44596	0.46700	0.30518	0.50839
36	334231	0.6021	0.39793	0.43100	0.30496	0.49890
27	515431	0.6154	0.38459	0.37900	1.29155	0.48691
28	535111	0.6369	0.36312	0.37800	0.28707	0.44668
39	515223	0.6783	0.32175	0.35000	0.26057	0.38979
50	415714	0.7138	0.28615	0.28700	0.20899	0.37823

Table 19. FDC crew individual performance: computer.

	SYMPTOM	PERFORMANCE	PREDICTED	ACTUAL	CONFIDENC	E LEVELS
	COMPLEX	DEGRADATION	VALUE	VALUE	LOW 95%	HIGH 95%
1	112111	0.1790	0.82098	0.86704	0.78951	0.84864
5	113111	0.1902	0.80984	0.88205	0.77747	0.83849
3	211111	0.1925	0.80752	0.74193	0.77242	0.83835
4	113121	0.1985	0.80155	0.78701	0.75325	0.84251
5	114111	0.2018	0.79319	0.76906	0.75731	0.83383
6	213111	0.2164	0.78364	0.77903	0.75750	0.80752
7	311111	0.2189	0.78108	0.76296	0.74403	0.81412
8	312111	0.2318	0.76817	0.74706	0.74212	0.79233
9	313111	0.2451	0.75491	0.76206	0.73085	0.77730
10	411111	0.2479	0.75213	0.72500	0.70767	0.79167
11	412111	0.2610	0.73808	0.75399	0.70505	0.76852
12	123111	0.2639	0.73614	0.73100	0.68422	0.78245
1.3	413111	0.2764	0.72357	0.82201	0.69343	0.75176
14	414111	0.2914	0.70858	0.69300	0.66928	0.74498
15	513111	0.3100	0.68995	0.66000	0.64654	0.73026
16	224111	0.3121	0.68791	0.56800	0.64007	0.73204
17	313112	0.3160	0.68405	0.72200	0.65311	0.71344
18	514111	0.3260	0.67396	0.64000	0.62348	0.72071
19	314112	0.3321	0.66790	0.66200	0.63442	0.69976
20	414112	0.3690	0.63097	0.64900	0.59274	0.66763
21	521111	0.3718	0.62822	0.64200	0.55182	0.69871
22	314113	0.4142	0.58580	0.55500	0.52864	0.64073
23	315113	0.4322	0.56780	0.53700	0.50578	0.62777
24	525111	0.4428	0.55716	0.55800	0.49541	0.61720
25	515311	0.4444	0.55555	0.56800	0.46537	0.64221
95	515431	0.5243	0.47569	0.44400	0.37502	0.57837
27	334231	0.5288	0.47123	0.50400	0.37270	0.57206
28	535111	0.5481	0.45187	0.47900	0.36882	0.53770
29	515223	0.5792	0.42084	0.44100	0.35120	0.49379
30	415314	0.6617	0.33831	0.34600	0.25275	0,43583

Table 20. Tank crew individual performance: tank commander.

	_	PERFORMANCE DEGRADATION	PREDICTED VALUE	ACTUAL VALUE	CONFIDENC	E LEVELS HIGH 95%
	70 1 (21		V-16-16			
1	112111	0.1468	0.85321	0.89003	0.81653	0.88360
2	211111	0.1554	0.84462	0.85705	0.80392	0.87825
3	113111	0.1792	0.82083	0.90203	0.77868	0.85644
4	113121	0.1857	0.81427	0.84198	0.75120	0.86436
5	311111	0.1996	0.80043	0.77206	0.75325	0.84051
- 6	114111	0.2169	0.78313	0.68500	0.72476	0.83216
7	213111	0.2283	0.77171	0,73808	0.73517	0.80440
А	312111	0.2403	0.75969	0.72000	0.72380	0.79233
9	411111	0.2527	0.74725	0.68000	0.68659	0.79979
10	123111	U.2644	0.73556	0.76296	0.66515	0.79576
11	313111	0.2863	0.71367	0.75306	0.67835	0.74649
15	412111	0.3001	0.69986	0.75306	0.65197	0.74384
13	413111	0.3523	0.64766	0.69200	0.60216	0.69064
14	224111	0.3820	0.61795	0.56700	0.54865	0.68277
15	313112	0.3926	0.60739	0.52300	0.56229	0.65073
16	414111	0.4083	0.59169	0.63300	0.53163	0.64913
17	513111	0.4245	0.57549	0.60300	0.51085	0.63764
18	521111	0.4302	0.56976	0.56300	0.46496	0.66865
19	314112	0.4505	0.54947	0.46900	0.50058	0.59743
20	514111	0.4834	0.51661	0,48800	0.44307	0.58943
21	414112	0.5265	0.47353	0.48800	0.42060	0.52707
22	314113	0.5692	0.43085	0.33500	0.35732	0.50756
23	315113	0.6263	0.37373	0.35400	0.29973	0.45416
24	515311	0.6295	0.37055	0.37800	0.26678	0.48791
25	334231	0.6433	0.35671	0.31700	0.24435	0.48747
26	525111	0.6616	0.33839	0.27300	0.26894	0.41569
27	515431	0.6893	0.31072	0.26096	0.20636	0.43865
28	535111	0.7631	0.23685	0.31200	0.16410	0.32925
50	515223	0.7938	0.20620	0.33200	0.14931	0.27758
30	415314	0.8397	0.16030	0.17393	0.09930	0.24843

Table 21. Tank crew individual performance: gunner.

	SYMPTOM	PERFORMANCE	PREDICTED	ACTUAL	CONFIDENC	E LEVELS
	COMPLEX	DEGRADATION	VALUE	VALUE	LOW 95%	HIGH 95%
1	112111	0.1027	0.89734	0.94202	0.87147	0.91849
5	211111	0.1148	0.88524	0.87900	0.85508	0.90987
3	113121	0.1174	0.88257	0.89798	0.84037	0.91467
4	113111	0.1209	0.87911	0.92498	0.84980	0.90344
5	114111	0.1417	0.85827	0.79899	0.81757	0.89110
6	311111	0.1499	0.85005	0.82506	0.81382	0.88027
7	213111	0.1576	0.84237	0.81306	0.81593	0.86565
8	312111	0.1748	0.82520	0.78194	0.79786	0.84954
9	411111	0.1936	0.80643	0.75194	0.75786	0.84723
10	123111	0.1977	0.80234	0.82807	0.74649	0.84839
11	313111	0.2029	0.79706	0.81995	0.77012	0.82171
12	412111	0.2237	0.77626	0.81199	0.73788	0.81031
13	413111	0.2573	0.74269	0.78398	0.70585	0.77643
14	224111	0.2870	0.71298	0.65500	0.65427	0.76531
15	414111	0.2938	0.70620	0.71700	0.65574	0.75213
16	313112	0.3050	0.69499	0.62900	0.65623	0.73126
17	513111	0.3203	0.67970	0.70800	0.62339	0.73126
18	314112	0.3452	0.65479	0.57000	0.61142	0.69573
19	514111	0.3615	0.63853	0.64500	0.57148	0.70059
20	521111	0.3691	0.63091	0.64300	0.53369	0.71855
21	414112	0.4177	0.58229	0.58200	0.53197	0.63095
55	314113	0.4762	0.52382	0.45500	0.45052	0.59610
23	515711	0.5097	0.49030	0.51800	0.37816	0.60343
24	315113	0.5220	0.47800	0.47000	0.40021	0.55687
25	334231	0.5322	0.46779	0.43400	0.34461	0.59504
26	515431	0.5465	0.45347	0.39400	0.32948	0.58353
27	525†11	0.5492	0.45079	0.37500	0.37478	0.52917
8 5	535111	0.6858	0,31420	0.38600	0.22846	0.41474
29	515223	0.7077	0.29233	0.43000	0.22149	0.37498
30	415314	0.7966	0.20343	0.20702	0.13147	0.30107

Table 22. Tank crew individual performance: loader.

		PERFORMANCE	PREDICTED	ACTUAL	CONFIDENC	T
	COMPLEX	DEGRADATION	VALUE	VALUE	1_0W 95%	HIGH 95%
1	211111	0.1908	0.80923	0.81503	0.77030	0.84290
5	112111	0.2026	0.79738	0.84104	0.75896	0.83090
3	311111	0.2281	0.77189	0.74097	0.72941	0.80954
4	113111	0.2556	0.74441	0.83603	0.70044	0.78398
5	113121	0.2567	0.74326	0.74193	0.67962	0.79803
6	411111	0.2702	0.72983	0.70400	0.67777	0.77626
7	312111	0.2852	0.71478	0.66600	0.68185	0.74555
- 8	213111	0.3008	0.69924	0.66300	0.66376	0.73243
Q	114111	0.3168	0.68323	0.59400	0.62366	0.73730
10	412111	0.3333	0.66667	0.68100	0.62498	0.70591
11	123111	0.3497	0.65031	0.68300	0.58411	0.71118
12	313111	0.3502	0.64980	0.68300	0.61749	0.68079
13	413111	0.4031	0.59691	0.64200	0.55741	0.63519
14	521111	0.4208	0.57917	0.54400	0.49208	0.66159
15	513111	0.4583	0.54167	0.60700	0.48742	0.59495
16	313112	0.4756	0.52440	0.44400	0.48569	0.56282
17	224111	0.4764	0.52355	0.51800	0.46412	0.58233
18	414111	0.4770	0.52299	0.52100	0.47214	0.57337
19	514111	0.5333	0.46667	0.49200	0.40625	0.52809
20	314112	0.5505	0.44945	0.43400	0.40941	0.49016
21	414112	0.6055	0.39450	0.44600	0.35273	0.43787
55	314113	0.6733	0.32666	0.25407	0.27278	0.38553
24	334231	0.6843	0.31566	0.33500	0.22741	0.41966
24	515711	0.6893	0.31071	0.32600	0.23183	0.40239
25	525111	0.7074	0.29257	0.24694	0.23903	0.35253
26	515431	0.7292	S27032	0.20603	0.19016	0.37004
27	315113	0.7358	0.26425	0.20505	Ú.21400	0.32149
28	535111	0.7912	0.20883	0.21501	0.15277	0.27887
29	515223	0.8406	0.15936	0.24694	0.12036	0.20817
30	415314	0.8941	0.10593	0.12100	0.06978	0.15776

Table 23. Tank crew individual performance: driver.

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	SYMPTOM	PERFORMANCE	PREDICTED	ACTUAL	CONFIDENC	E LEVELS
`	COMPL EX	DEGRADATION	VALUE	VALUE	LOW 95%	HIGH 95%
1	211111	0.1255	0.87446	0.86796	0.84396	0.89971
5	112111	0.1368	0.86319	0.89604	0.83230	0.88904
3	311111	0.1506	0.84941	0.87501	0.81533	0.87815
4	113111	0.1777	0.82230	0.91003	0.78516	0.85433
5	113121	0.1795	0.82054	0.81802	0.76585	0.86471
6	411111	0.1796	0.82039	0.78108	0.77730	0.85668
7	312111	0.1947	0.80534	0.75101	0.77765	0.83048
8	213111	0.2105	0.78951	0.79803	0.75878	0.81728
9	114111	0.2274	0.77259	0.67200	0.71896	0.81862
10	412111	0.2297	0.77030	0.77206	0.73361	0.80313
11	313111	0.2477	0,75232	0.77294	0.72332	0.77920
12	123111	0.2639	0.73614	0.71700	0.67335	0.79051
13	413111	0.2890	0.71098	0.76296	0.67388	0.74536
14	521111	0.3097	0.69028	0.65200	0.60432	0.76477
15	513111	0.3342	0.66583	0.69000	0.61190	0.71574
16	313112	0.3382	0.66181	0.57600	0.62354	0.69808
17	414111	0.3565	0.64352	0.63500	0.59183	0.69207
18	224111	0.3763	0.62372	0.62400	0.56195	0.68171
19	514111	0.4062	0,59385	0.63500	0.52874	0.65582
20	314112	0.4105	0.58950	0.53600	0.54633	0.63134
21	414112	0.4623	0.53771	0.56500	0.48970	0.58502
55	314113	0.5194	0.48059	0.44000	0.41228	0.54964
23	515311	0.5743	0.42566	0.39800	0.32485	0.53306
24	315113	0.5956	0.40441	0.32800	0.33507	0.47778
25	334231	0.6039	0.39606	0.39000	0.28782	0.51553
56	525111	0.6074	0.39259	9.35100	0.32464	0.46496
27	515431	0.6246	0.37538	0.33200	0.26835	0.49609
28	535111	0.7198	0.28023	0.33300	0.20522	0.36995
29	515223	0.7322	0.26776	0.36400	0.20457	0.34198
30	415314	0.8033	0.19671	0.22794	0.13011	0.28604

Table 24. TOW crew individual performance: squad leader.

		PERFORMANCE DEGRADATION	PREDICTED VALUE	ACTUAL VALUE	CONFIDENC LOW 95%	E LEVELS HIGH 95%
	211111	0.1395	0.07147	0 97000	A 0.75 (1.0	0.000//7
5	112111	0.1285	0.87147	0.87900	0.83548	0.90043
3	111121	0.1450 0.1484	0.85495 0.85157	0.89898 0.93401	0.81847	0.88514
4	311111	U.1566			0.81275	0.88350
5	212111		0.84343	0.82607	0.80187	0.87761
		0.1758	0.82419	0.83299	0.79167	0.85246
6 7	411111	0.1992 0.1970	0.81077	0.74307	0.75639	0.85545
, 8	113111		0.80298	0.86796	0.75768	0.84158
9	112121	0.2013	0.79867	0.89100	0.75969	0.83272
10	111131	0.2057	0.79429	0.67600	0.72351	0.85056
11	312111 213111	0.2115 0.2358	0.78852	0.71000	0.75343	0.81965
12	123111	0.2431	0.76423 0.75694	0.79101	0.72684	0.79803
13	412111	0.2524	0.74763	0.76602 0.76995	0.68373	0.81787
14	114111	0.2617	0.74703		0.69955	0.79051
15	113121	0.2672	0.73282	0.71800 0.81306	0.67164	0.79543
16	112131	0.2725	0.72750	0.61500	0.68240 0.64910	0.77799
17	521111	0.2775	0.72252	0.72200		
18	313111	0.2795	0.72050	0.69600	0.62251 0.68359	0.80440 0.75473
19	413111	0.3279	0.67210	0.69900	0.62280	0.71788
20	113131	0.3513	0.64869	0.64800	0.55545	0.73184
21	314111	0.3597	0.64066	0.58000	0.58381	0.69382
55	224111	0.3685	0.63148	0.60500	0.55730	0.69992
23	114112	0.3707	0.62929	0.48900	0.56305	0.69100
24	513111	0.3802	0.61975	0.59200	0.54876	0.68596
25	313112	0.3919	0.60813	0.51300	0.56269	0.65176
26	414111	0.4136	0.58638	0.64800	0.52120	0.64867
27	214112	0.4256	0.57443	0.45200	0.52189	0.62535
28	514111	0.4701	0.52992	0.54200	0.44894	0.60934
29	314112	0.4823	0.51768	0.49800	0.46926	0.56577
30	515311	0.5363	0.46367	0.40200	0.35061	0.58059
31	414112	0.5395	0.46047	0.49500	0.40379	0.51818
32	214113	U.5517	0.44831	0.34300	0.37157	0.52758
33	314113	0.6075	0.39252	0.40200	0.32116	0.46879
34	525111	0.6266	0.37338	0.37800	0.29553	0.45836
35	334231	0.6682	0.33183	0.28700	0.22426	0.46033
36	535111	0.6871	0.31289	0.36500	0.21806	0.42659
37	315113	0.691i	0.30887	0.32500	0.24269	0.38383
38	515431	0.7081	0.29194	0.26698	0.18422	0.42943
39	415314	0.8083	0.19170	0,21098	0.11899	0.29406
40	515223	0.8331	0.16687	0.31800	0.11816	0.23041

Table 25. TOW crew individual performance: gunner.

	SYMPTOM	PERFORMANCE	PREDICTED	ACTUAL	CONFIDENC	E LEVELS
	COMPLEX	DEGRADATION	VALUE	VALUE	LOW 95%	HIGH 95%
1	211111	0.1694	0.83062	0.85296	0.78617	0.86738
جَ	112111	0.1891	0.81092	0.86495	0.76638	0.84851
3	111121	0.1926	0.80737	0.91396	0.76024	0.84710
4	311111	0.2064	0.79364	0.75007	0.74307	0.83658
5	212111	0.2292	0.77083	0.74193	0.73184	0.80565
6	411111	0.2488	0.75120	0.65800	0.68619	0.80643
7	113111	0.2539	0.74612	0.83005	0.69283	0.79298
8	112121	0.2581	0.74193	0.86295	0.69607	0.78279
9	111131	0.2625	0.73750	0.61300	0.65581	0.80550
10	312111	0.2749	0.72510	0.63800	0.68391	0.76278
11	123111	0.3006	0.69940	0.71900	0.61758	0.77030
15	213111	0.3025	0.69745	0.62700	0.65429	0.73730
13	412111	0.3258	0.67417	0.75007	0.61919	0.72474
14	114111	0.3317	0.66830	0.59600	0.59382	0.73517
15	113121	0.3367	0.66329	0.76799	0.60677	0.71550
16	112131	0.3418	0.65825	0.55700	0.57175	0.73536
17	521111	0.3479	0.65208	0.63300	0.54287	0.74725
18	313111	0.3561	0.64391	0.65600	0.60252	0.68326
19	413111	0.4135	0.58651	0,60400	0.53333	0.63775
20	113131	0.4309	0.56905	0.57600	0.47198	0.66109
21	224111	0.4442	0.55579	0.53900	0.47903	0.62998
22	114112	0.4458	0.55417	0.42500	0.48555	0.62079
53	314111	0.4465	0.55351	0.49100	0.49384	0.61169
24	313112	0.4727	0.52733	0.45400	0.48058	0.57360
25	513111	0.4733	0.52666	0.51100	0.45369	0.59851
26	214112	0.5063	0.49368	0.41600	0.44093	0.54658
27	414111	0.5070	0.49302	0.54500	0.42755	0.55872
28	314112	0.5666	0.43338	0.41200	0.38657	0.48140
29	514111	0.5673	0.43272	0.46700	0.35545	0.51341
30	214113	0.6244	0.37561	0.25597	0.30452	0.45249
31	414112	0.6250	0.37498	0.41500	0.32259	0.43047
32	515711	0.6559	0.34406	0.28200	0.24675	0.45638
33	314113	0.6794	0.32059	0.31600	0.25693	0.39183
34 35	525111	0.7072	0.29279	0.33700	0.22583	0.37019
36	334231 535111	0.7410	0.25903	0.20899	0.16924	0.37509
37	535111 315113	0.7531 0.7557	0.24694	0.28700	0.16714	0.34862
38	515113	0.7337 0.8091	0.24435	0.27800	0.18847	0.31071
30	415314	0.8642	0.19093	0.17902	0.11456	0.30099
40	515223	0.8822	0.13576	0.18005	0.08211	0.21602
~ v	313663	V.00EC	0.11784	0.16995	0.08211	0.16645

Table 26. TOW crew individual performance: driver.

	·					
		PERFORMANCE	PREDICTED	ACTUAL	CONFIDENC	
	COMPL EX	DEGRADATION	VALUE	VALUE	LOW 95%	HIGH 951
1	211111	0.0544	0.94558	0.94501	0.92539	0.96053
2	112111	0.0683	0.93169	0.96401	0.90888	0.94912
3	311111	0.0685	0.93150	0.92601	0.90687	0.95003
4	111121	0.0697	0.93028	0.97301	0.90585	0.94868
5	212111	0.0856	0.91443	0.88205	0.89321	0.93176
6	411111	0.0858	0.91420	0.92301	0.87964	0.93952
7	113111	0.1065	0.89350	0.91698	0.86021	0.91961
8	312111	0.1068	0.89321	0.85396	0.86898	0.91341
ġ	112121	0.1087	0.89129	0.94799	0.86283	0.91451
10	111131	0.1109	0.88914	0.78006	0.83576	0.92663
11	213111	0.1322	0.86784	0.85594	0.83916	0.89216
12	412111	0.1324	0.86761	0.89302	0.83174	0.89678
13	123111	0.1385	0.86152	0.87303	0.80218	0.90508
14	521111	0.1392	0.86081	0.77609	0.78381	0.91349
15	114111	0.1623	0.83767	0.78600	0.77989	0.88247
16	313111	0.1627	0.83726	0.90097	0.80721	0.86354
17	113121	0.1655	0.83452	0.89501	0.79117	0.87034
18	112131	0.1685	0.83146	0.77101	0.76242	0.88340
19	413111	0.1988	0.80123	0.82707	0.75786	0.83849
20	314111	0.2401	0.75988	0.70100	0.70504	0.80721
21	513111	0.2407	0.75933	0.72900	0.69142	0.81638
55	113131	0.2481	0.75194	0.75306	0.65758	0.82721
23	224111	0.2503	0.74970	0.78499	0.67618	0.81123
24	114112	0.2633	0.73672	0.52800	0.66955	0.79429
25	313112	0.2639	0.73614	0.64100	0.69143	0.77643
26	414111	0.2875	0.71248	0.74097	0.64531	0.77136
27	214112	0.3134	0.68657	0.57400	0.63083	0.73730
28	514111	0.3401	0.65995	0.70000	0.57034	0.73943
29	314112	0.3683	0.63175	0.58600	0.57761	0.68276
30 21	515311	0.3938	0.60621	0.53000	0.47023	0.72751
31	414112	0.4267	0.57330	0.58600	0.50622	0.63778
32	214113	0.4571	0.54289	0.45500	0.45019 0.39245	0.57253
33 34	314113 525111	0.5181 0.5306	0.48190 0.46941	0.45500 0.46800	0.36986	0.57146
34 35	334231	0.5835	0.41650	0.39100	0.30408	0.57334
36	535111	0.6039	0.39606	0.45700	0.26973	0.53797
36 37	515431	0.6128	0.38725	0.34400	0.23ª12	0.56093
38	315113	0.6361	0.36386	0.44200	0.27948	0.4575
39	415314	0.7615	0.23849	0.30100	0.13955	0.37704
40	515223	0.8067	0.19325	0.31500	0.13022	0.27715

Table 27. TOW crew individual performance: loader.

		PERFORMANCE DEGRADATION	PREDICTED VALUE	ACTUAL VALUE	CONFIDENC LOW 95%	E LEVELS HIGH 95%
1	211111	0.1177	0.88226	0.87599	0.84684	0.91036
Ž	111121	0.1330	0.86704	0.93002	0.82935	0.89743
3	311111	0.1464	0.85358	0.83299	0.81169	0.88745
4	112111	0.1491	0.85094	0.87203	0.81153	0.88340
5	411111	0.1806	0.81936	0.78499	0.76351	0.86436
6	212111	0.1838	0.81623	0.78801	0.78074	0.84710
7	111131	0.1848	0.81518	0.69900	0.74536	0.86921
8	112121	0.2057	0.79429	0.85705	0.75250	0.83076
9	312111	0.2244	0.77556	0.76495	0.73711	0.80984
10	113111	0.2281	0.77189	0.88205	0.71903	0.81728
11	521111	0.2699	0.73010	0.68700	0.62566	0.81412
12	412111	0.2712	0.72879	0.75602	0.67572	0.77609
13	213111	0.2753	0.72465	0.70300	0.68125	0.76423
14	112131	0.2768	0.72323	0.62000	0.63964	0.79364
15	123111	0.2782	0.72182	0,74801	0.63835	0.79233
16	113121	0.3041	0.69594	0.82405	0.63884	0.74763
17	313111	0.3282	0.67181	0.73000	0.62954	0.71148
18	114111	0.3328	0.66721	0.55800	0.58835	0.73769
19	413111	0.3858	0.61423	0.68600	0.55901	0.66666
20	113131	0.3924	0.60759	0.62800	0.50637	0.70034
21	513111	0.4467	0.55326	0.56700	0.47632	0.62774
22	314111	0.4519	0.54811	0.50100	0.48508	0.60964
23	224111	0.4554	0.54461	0.60600	0.46353	0.62338
24	313112	0.4765	0.52351	0.44600	0.47418	0.57239
25	114112	0.4817	0.51832	0.34400	0.44590	0.58998
26	414111	0.5146	0.48545	0.52500	0.41661	0.55484
27	214112	0.5444	0.45563	0.37700	0.40088	0.51147
28	514111	0.5768	0.42324	0.46800	0.34258	0.50821
29	314112	0.6057	0.39431	0.39700	0.34670	0.44402
30	414112	0.6638	0.33615	0.39800	0.28410	0.39252
31	515311	0.6722	0.32780	0.23505	0.22899	0.44475
35	214113	0.6900	0.30998	0.19093	0.24324	0.38578
33	314113	0.7410	0.25903	0.20702	0.20101	0.32676
34	334231	0.7431	0.25693	0.25105	0.16356	0.37943
35	525111	0.7499	0.25011	0.17393	0.18725	0.32554
36	535111	0.7964	0.20359	0.23308	0.13227	0.30022
37	515431	0.8089	0.19108	0.16798	0.11135	0.30828
38	315113	0.8285	0.17150	0.21199	0.12731	0.22706
39	415314	0.9117	0.08835	0.13000	0.05083	0.14931
40	515223	0.9177	0.08234	0.13599	0.05546	0.12057

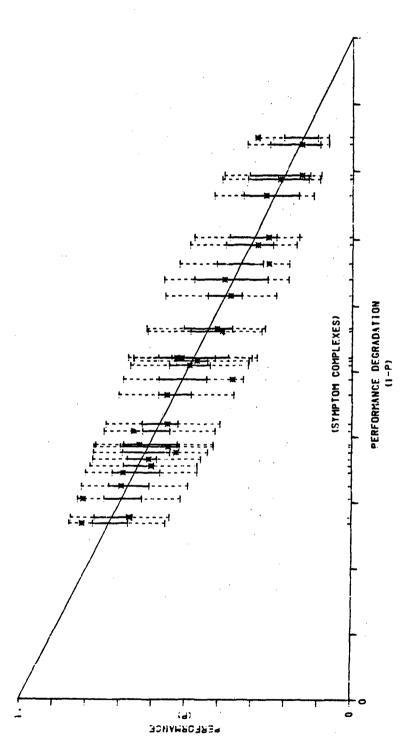


Figure 17. Gun crew individual performance: chief of section.

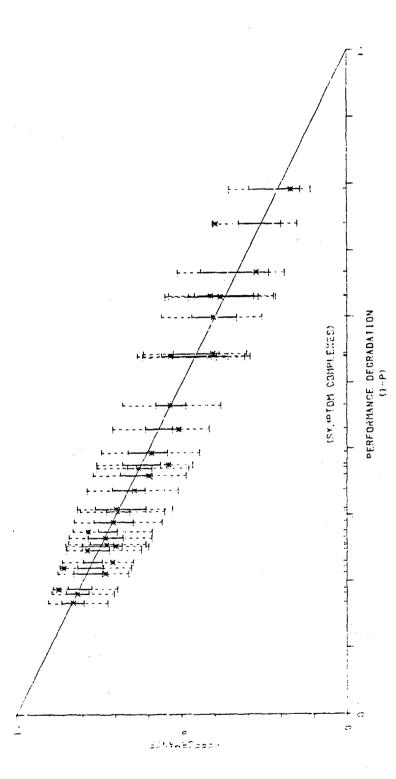


Figure 18. Gun crew individual performance: gunner.

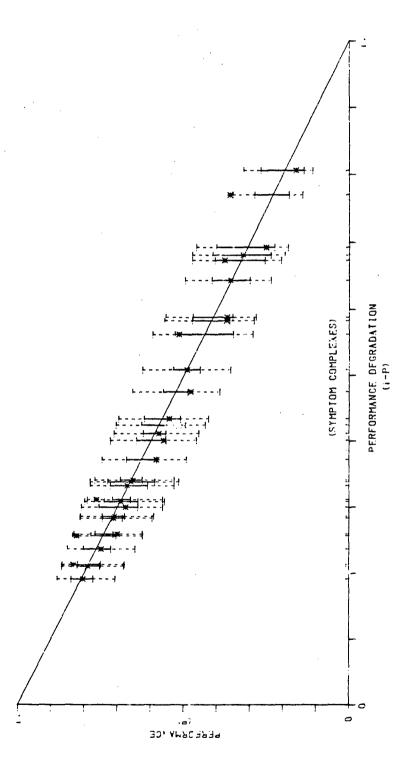


Figure 19. Gun crew individual performance: assistant gunner.

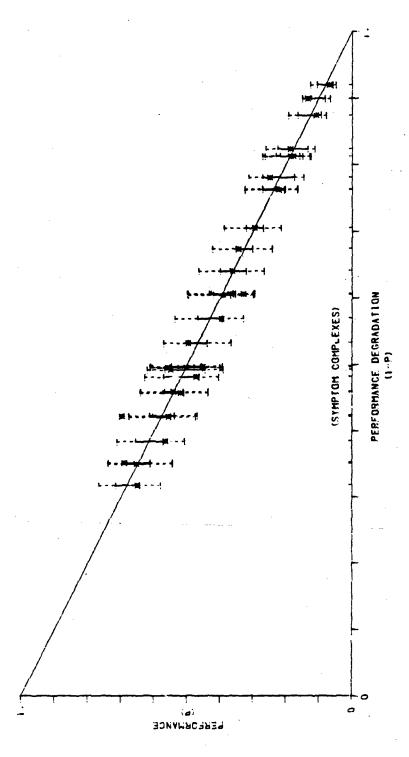


figure 20. Gun crew individual performance: loader.

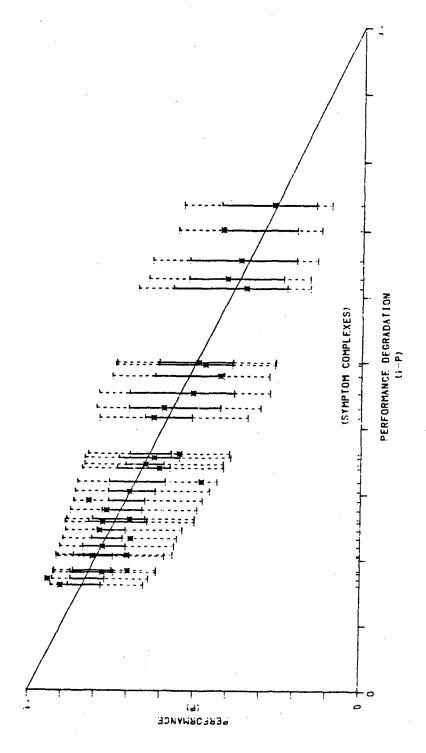


Figure 21. FDC crew individual performance: fire direction officer.

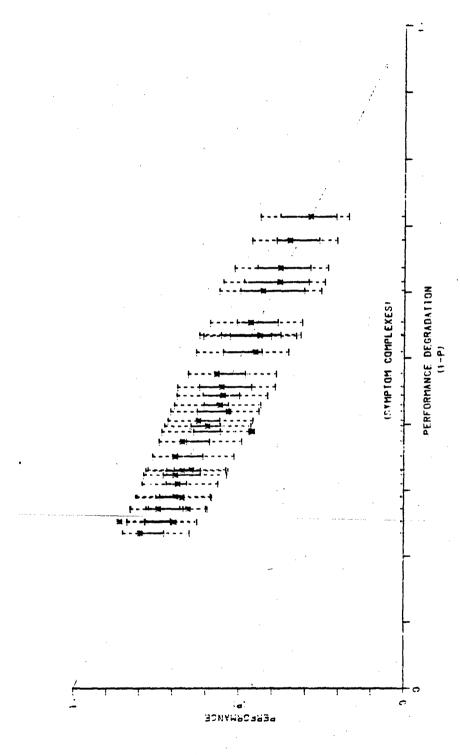


Figure 22. FUC crew individual performance: horizontal control operator.

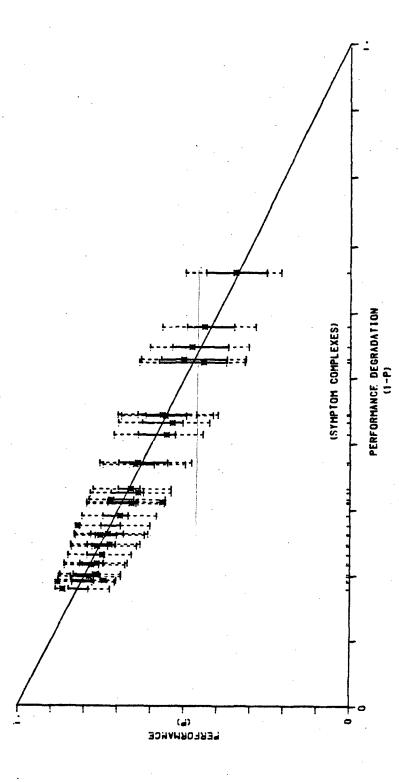


Figure 23. FDC crew individual performance: computer.

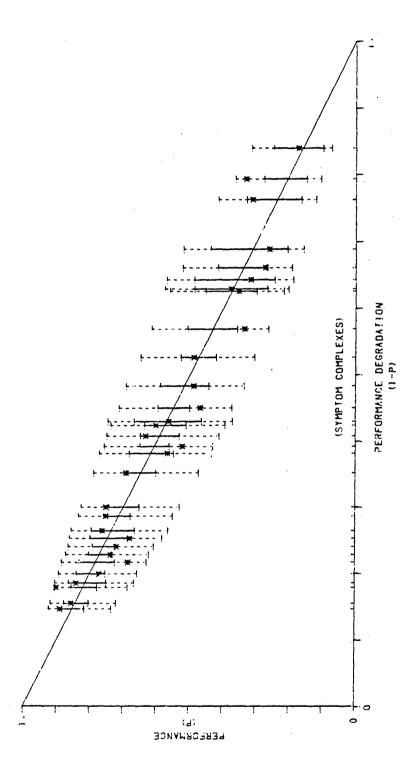


Figure 24. Tank crew atividual performance: tank commander.

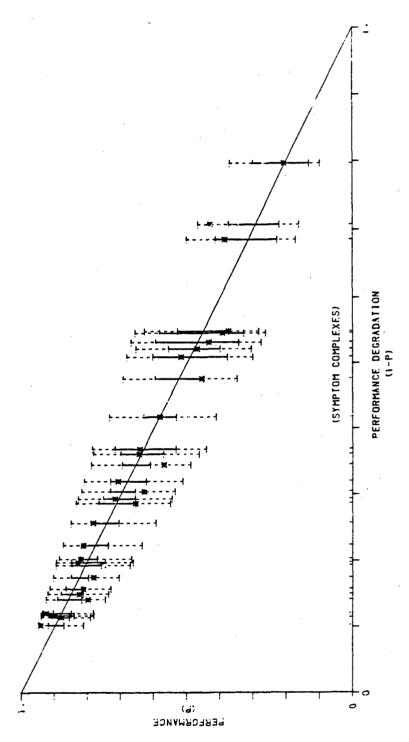


Figure 25. Tank crew individual performance: gunner.

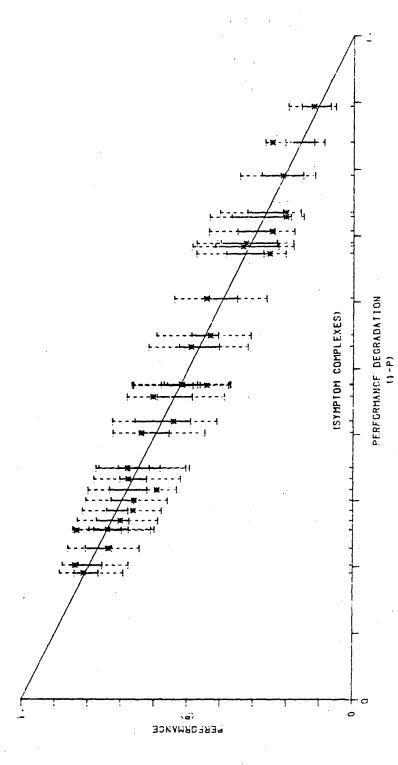


Figure 26. Tank crew individual performance: loader.

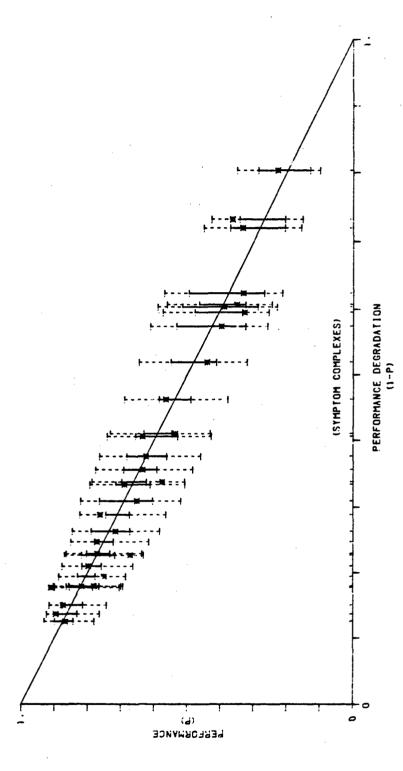


Figure 27. Tank crew individual performance: driver.

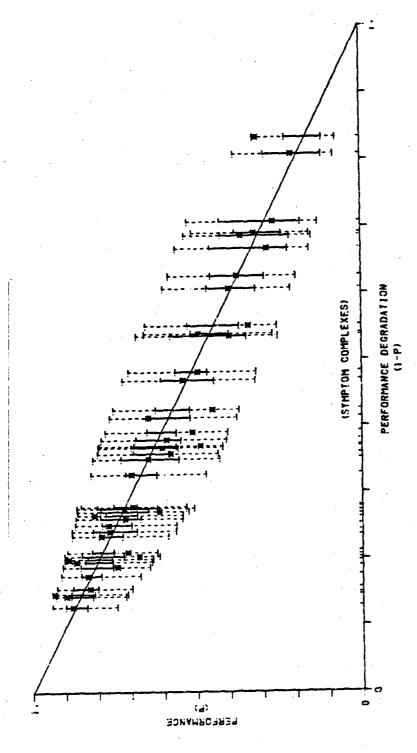


Figure 28. TOW crew individual performance: squad leader.

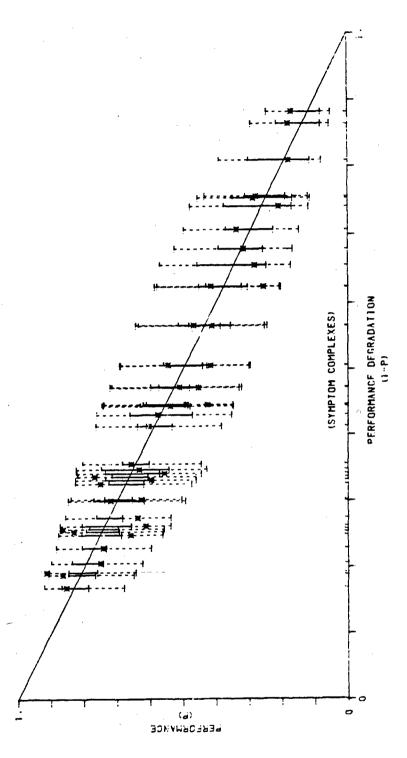


Figure 29. TOW craw individual performance: gunner.

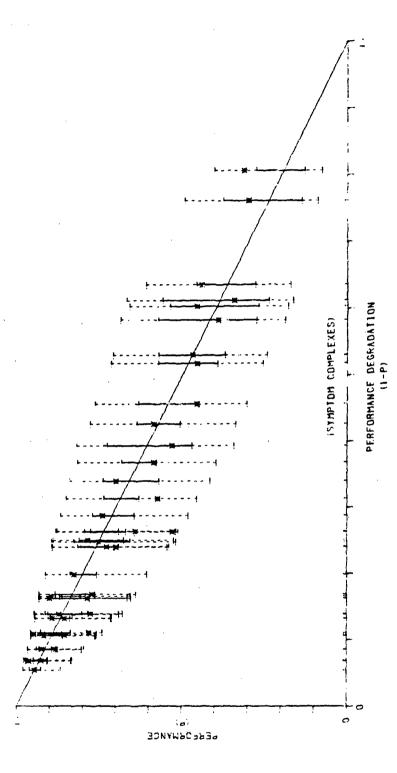


Figure 30. TOW crew individual performance: driver.

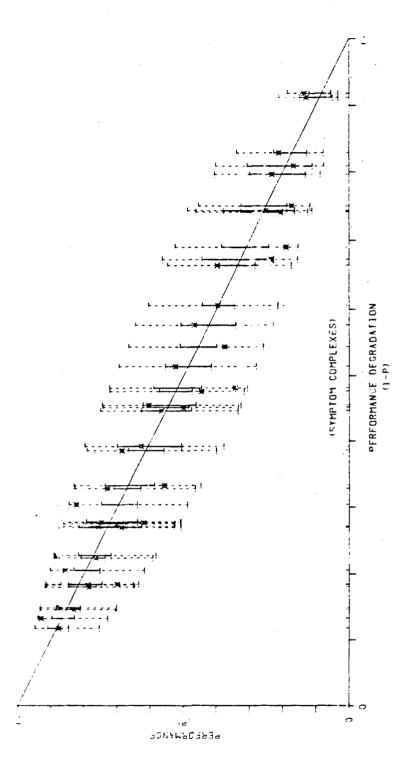


Figure 31. TOW crew individual performance: loader.

The performance plots indicate relative trends for each crew position such as tendencies toward high, low, and middle of clustering responses along the straight line. High and low clustering would indicate skewed distributions, and those tending to cluster toward the middle may indicate a more symmetric distribution. The lowest estimates of performance are provided for the artillery gun crew loader, whose tasks are probably the most physically demanding. On the other hand, the highest estimates of performance are provided for the FDC crew computer position, whose activity is the least physically demanding, consisting wholly of cognitive tasks. Some crewmembers show a near-threshold-like effect even for the most benign symptom complexes where performance drops from 100 to between 70 and 80 percent.

Also noteworthy are the relative widths of the error bar patterns. For example, the gun crew loader plot also shows the narrowest error bar widths, indicating the most consistency in the response data. On the other hand, the fire direction officer plot shows perhaps the widest error bar spread, indicating a relative lack of consistency in the response data.

Differences between input data and regression prediction performance values are seen to occur more frequently for symptom complexes 112111, 113111, 224111, and 515223. Table 28 lists those cases, termed outliers, where the data values lie outside the 95 percent confidence limits of the regression mean value predictions. Data values for complexes 112111 and 113111 are consistently higher than the regression values. Moreover, data values for symptom complex 113111 are consistently, although only slightly higher, than complex 112111. Based on our evaluation of the data (Sec. 2) and this analysis, we are unable to positively explain those differences. However, we point out that the regression analysis served to predict performance for symptom complexes 112111 and 113111 in the order that one would expect, i.e., a lower value of performance for 113111 than for 112111.

In Figs. 17 through 23, symptom complex 224111, for the artillery gun, and FDC crews, is associated with lower values from the data relative to the regression values, whereas symptom complex 515223 is associated with substantially higher values. We are also unable to explain

Significant outliers: percentage variation of performance data prediction relative to regression performance prediction. Table 28.

Commence of the second second

			Sym	Symptom Complex		Performance Data
Crew	Crewmember	112111 113111	113111	224111b	515223 ^b	Difference between 224111 and 515223
Sun	Chief of section Gunner Assistant gunner Loader	11.0 6.6 ^c	14.0 10.0 21.0	-29 (0.36) -13 (0.54) 13 (0.50) -16 (0.33)	92 (0.29) 54 (0.40) 57 (0.36) 33 ^c (0.13)	0.07 0.14 0.14 0.20
FDC	Fire direction officer Horizents! control operator Computer	7.9	14.0 29.0 8.9	-29 (0.48) -44 (0.23) -17 (0.57)	41° (0.42) (0.22) (0.44)	0.06 0.01 0.13
Tank	Commander Gunner Loader Driver	4.3 5.0 5.5°	9.9 5.2 ^c 12.0 11.0	(0.57) (0.66) (0.52) (0.62)	61 (0.33) 47 (0.43) 55 (0.25) 36 (0.36)	0.24 0.23 0.27 0.26
TOW	Squad lender Gunner Driver Loader	5.2° 6.6° 3.5	8.1 11.0 8.9 ^c 14.0	(0.61) (0.54) (0.78) (0.61)	91 (0.32) 44 ^c (0.17) 63 (0.32) 65 ^c (0.14)	0.29 6.34 0.45 0.47

a Negative values indicate data values less than regression values.

bata predictions are in parentheses.

Cludicates near upper 95 percent confidence limit.

these differences based on the treatment of the data. However, we do observe that the spread (given in the last column of Table 28) in data performance values between complexes 224111 and 515223 given for the gun and FDC crews (parenthetical values in Table 28) appears narrow given the differences in the severity levels of the two complexes. A wider spread in values as predicted by the regression relationship seems more reasonable considering the two complexes.

In addition to the crewmember positions, regression analyses were performed for the separate tasks under each crew position, using the task response data given in Appendix E. Results of predicted task performance are graphically compared with predicted position performance in Appendix G. The regression parameters for task performance prediction are also listed in tables given in Appendix G.

The regression analysis described in this section serves to develop performance input data for further extending individual crewmember performance to dose and time based on the numerical procedures described in Sec. 5. After improvements were made to the army questionnaire raw data discussed in Sec. 2, performance data were analyzed and prepared for mapping onto the dose/time framework developed in Sec. 4. Section 5 then describes the process of joining the individual crewmember performance data with the dose and time variables to develop the performance dose/time relationships.

SECTION 4

DOSE/TIME SYMPTOM COMPLEXES

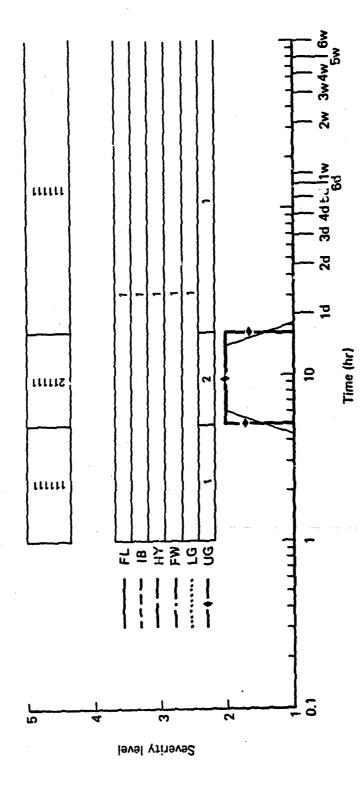
In this section, we build a framework for expressing the performance prediction estimates of Sec. 3 as a function of dose and time. Using time-dependent symptom profiles, a dose/time structure is developed, which consists of discrete regions that represent the various symptom complexes. From the symptomatology descriptions of the acute radiation syndromes in humans (developed from actual case experience of irradiated individuals [Baum et al., 1983]), time-dependent profiles are constructed to typify the symptom severity for each of eight subdivisions of the intermediate dose range [75 to 4500 rads (cGy)*] [Anno and Wilson, 1983]. Time boundaries are assigned to the symptom complexes according to symptom severity level. Finally, the symptom complex areas are joined for each of the eight dose ranges—according to dose—to form a dose/time map of symptom complexes.

Figures 32 through 39 plot symptom severity level against the logarithm of postexposure time for each of eight free-in-air dose ranges [75-150, 150-300, 300-530, 530-830, 830-1100, 1100-1500, 1500-3000, and 3000-4500 rads (cGy)] for the six symptom categories developed in Baum et al. [1983]; those categories are as follows:

- 1. Upper gastrointestinal distress (UG).
- 2. Lower gastrointestinal distress (LG).
- 3. Fatigability and weakness (FW).
- 4. Hypotension (HY).
- 5. Infection, bleeding, and fever (IB).
- 6. Fluid loss and electrolyte imbalance (FL).

The severity profiles developed in Anno and Wilson [1983] for each of the six symptom categories are represented in the figures by the "curves" formed by the connected sloping and parallel straight lines. The curves are also shown as step functions where vertical lines connect

 $^{^{\}star}$ One centigray (cGy) is equal to one rad.



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Figure 32. Symptom severity level: 75 to 150 rads (cGy) free-in-air dose.

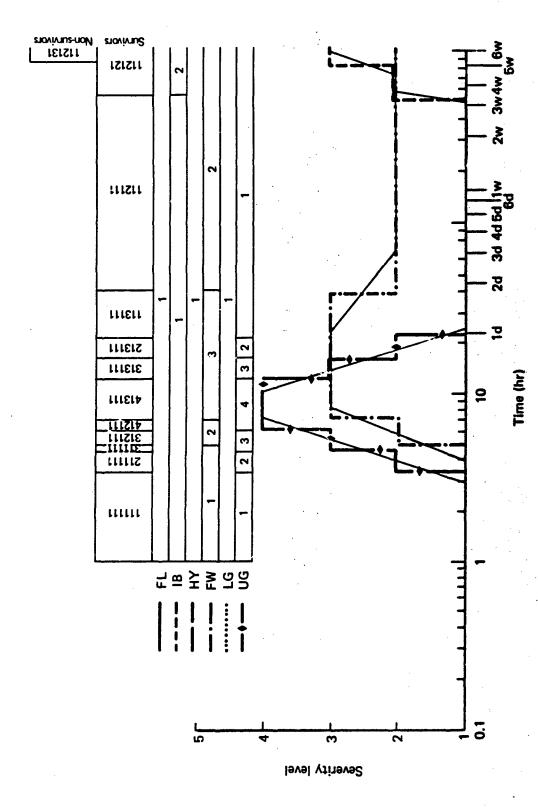
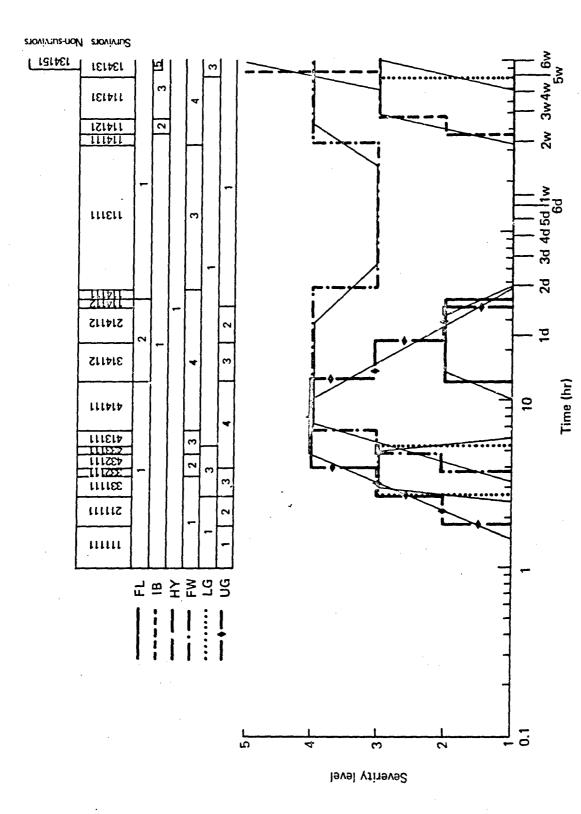
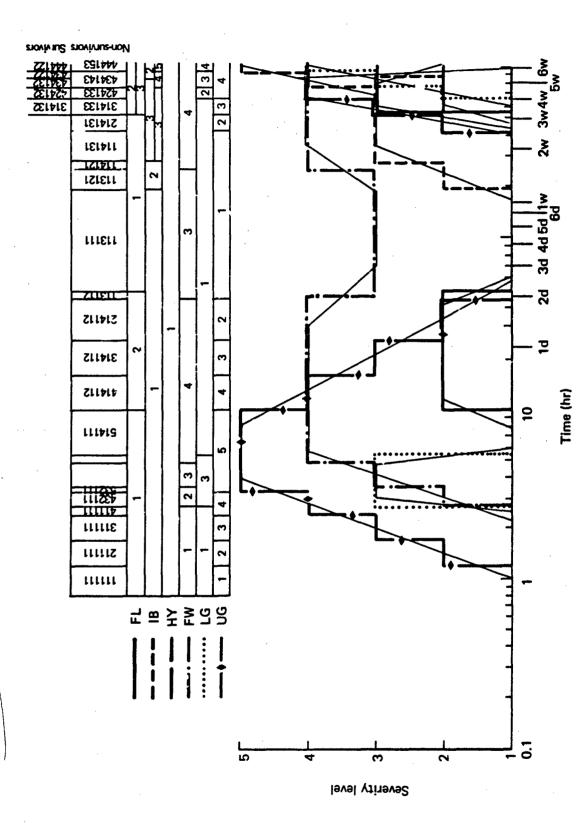


Figure 33. Symptom severity level: 150 to 300 rads (cGy) free-in-air dose.



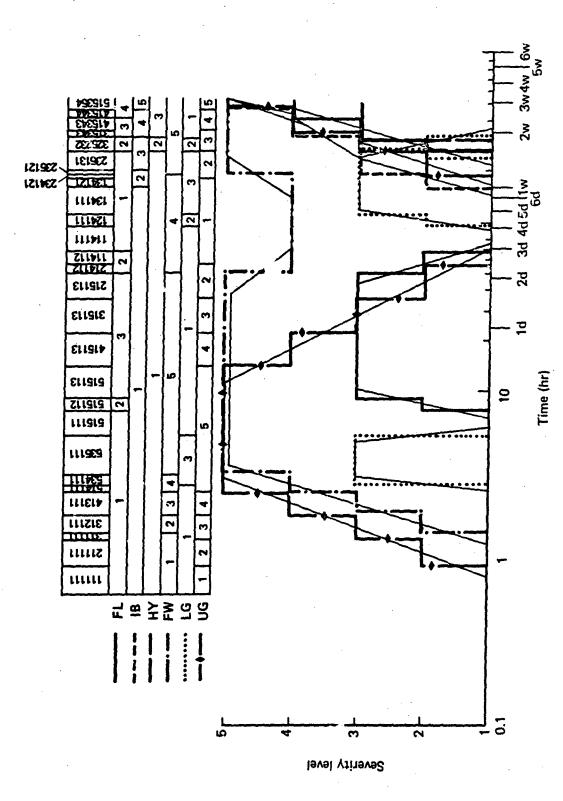
Symptom severity level: 300 to 530 rads (cGy) free-in-air dose. Figure 34.

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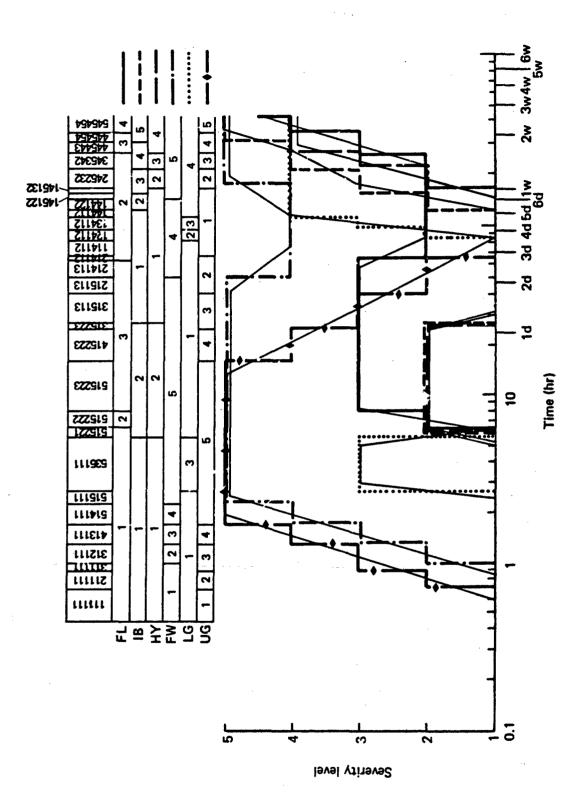


Symptom severity level: 530 to 830 rads (cGy) free-in-air dose. Figure 35.

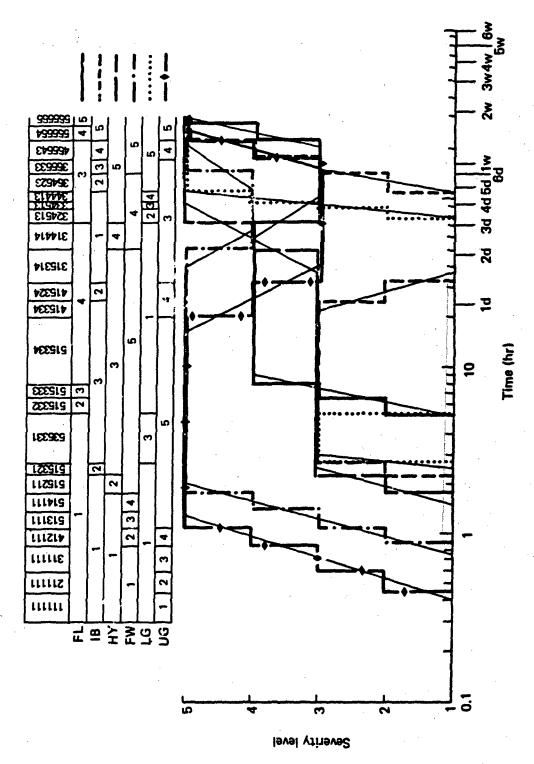
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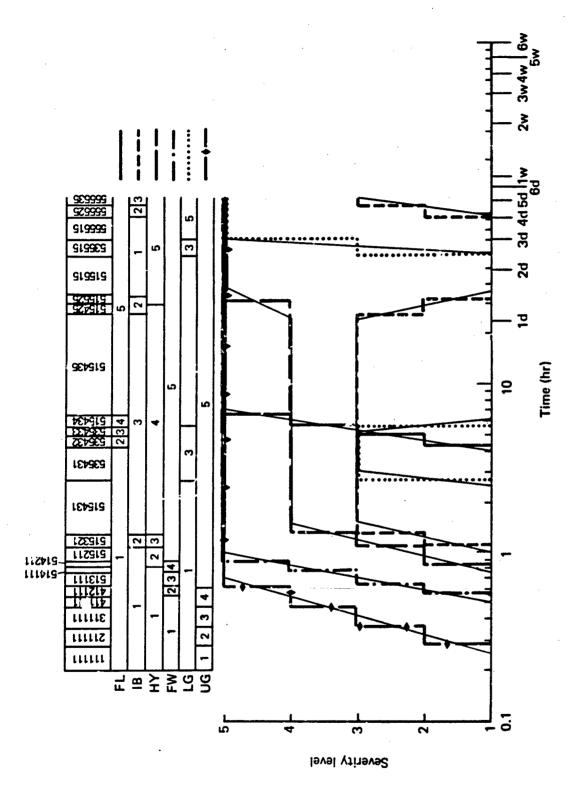
Symptom severity level: 830 to 1100 rads (cGy) free-in-air dose. Figure 36.



Symptom severity level: 1100 to 1500 rads (cGy) free-in-air dose. Figure 37.



Symptom severity level: 1500 to 3000 rads (cGy) free-in-air dose. Figure 38.



Symptom severity level: 3000 to 4500 rads (cGy) free-in-air dose. Figure 39.

the levels. Thus, symptom severity is represented in terms of discrete levels consistent with the formation of the severity level descriptions in Anno and Wilson [1983]. The step function profiles are constructed such that approximately equal areas under the sloping curves are maintained.

Above those curves, each of the symptom categories is shown as a horizontal band spanning time and is divided into a series of rectangles of varying length. The symptom category bands contain integers that designate the severity level and associated time period. Above the group of rectangles is another band that defines the symptom complexes in terms of a six-digit code. Those coded rectangles merely "collapse" the separate bands of each of the six symptom categories depicted below them into the symptom complexes. The position of each digit in the code corresponds to one of the six symptom categories shown earlier, and in the order indicated. However, the *value* of each individual digit indicates the severity level of each symptom category.

For example, in Fig. 34, for the dose range 300 to 530 rads (cGy), symptom complex 314112, existing between 13 and 22 hr following exposure, consists of symptom categories in the following order: upper gastro-intestinal distress (UG), severity level 3; lower gastrointestinal distress (LG), level 1; fatigability and weakness (FW), level 4; hypotension (HY), level 1; infection, bleeding, and fever (IB), level 1; and fluid loss and electrolyte imbalance (FL), level 2. The description for this symptom complex [Anno and Wilson, 1983] used in the army combat crew questionnaire [Glickman et al., 1983] is as follows: "Nauseated, considerable sweating, swallows frequently to avoid vomiting; very tired and weak; thirsty and has dry mouth, weak and faint."

Except for the early LG distress, we estimate that all other symptom categories represented by the symptom severity profiles in Figs. 32 through 39 are applicable to about 50 percent (except for the 75 to 150 rads [cGy] dose range) or more of those irradiated, and are thus typically representative. The profile for LG distress, shown by a dotted line between 2.5 and 5.5 hr in Figs. 34 through 39, is a brief one— or two-time episode of diarrhea that may occur in the early or prodromal phase following radiation exposure in about 10 percent of those irradiated up to a dose of about

1500 rads (c3y). That threshold may increase to a maximum of about 30 percent up to a dose of 4500 rads (cGy). Since our focus in this report is on the effects on performance of the "typical" acute radiation syndrome and symptom sequelae, we have omitted the early LG effect from the main calculations of performance for typical combat crewmombers as a function of dose and time. However, additional calculations have been made that do take the early LG effect into account (see Appendix II).

At the extreme ends of Figs. 33, 34, and 35, two sets of symptom complexes are indicated at corresponding or similar times to reflect the possible sequelae of "survivors" and "nonsurvivors." In Fig. 33, for the 150 to 300 rad (cGy) dose range, a small number of lethalities, less than or equal to about 5 percent, may be expected to occur sometime after the fifth week following exposure [Baum et al., 1983]. Accordingly, we have represented the nonsurvivors by complex 112131 as the offset rectangle. It Fig. 34, for the 300 to 530 rad (cGy) dose range, up to 50 percent lethallities may be expected sometime after the fourth week following exp. sure [Baum et al., 1983]. Similarly, we have represented nonsurvivors be symptom complex 13415) as the offset rectangle. However, in Fig. 35 for the 530 to 830 rad (eGy) dose range, 50 to 99 percent lethalities may be expected starting at the end of the third week following exposure [Baum et al., 1983]. In that case the survivors, rather than the consurvivors, are represented by the offset rectangles containing symptom complex designations.

Figure 40 gives the dose/time locations of all the symptom complexes. The symptom complexes in the upper band of rectangles in Figs. 37 through 39, for each of the eight dose ranges, are combined. The percent (incidence) of individuals expected to have acute radiation symptoms represented by the symptom complexes are indicated by dose range to the left of the ordinate [Baum et al., 1983]. The various complexes typity expected states of acute radiation sickness following a prompt period of exposure. However, since each complex is composed of six different symptomatic components, it is not a straightforward matter to quantify each in terms of an overall state or condition measured on some uniform scale. This is because we cannot stipulate the degree of severity level equivalence or symptom dependence across the symptom categories. It is

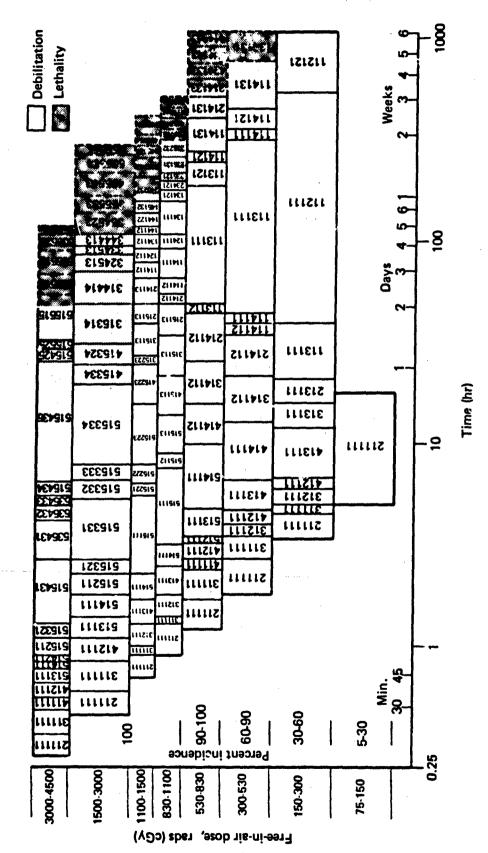


Figure 40. Symptom complexes.

possible, however, to indicate where severe conditions such as debilitation and lethality can be expected. In Fig. 40 the dark shaded areas indicate the occurrence of lethality. Although not shown in the figure, possibly a small number of lethalities may occur after 5 weeks for the 150 to 300 rad (cGy) dose range. The lightly shaded areas indicate severe debilitation ranging from shock, prostration, and fainting at the high dose ranges to infection, fever, weakness, and exhaustion at the low dose ranges.

The severe conditions (debilitation and lethality) indicated in Fig. 40 are where the radiobiological considerations alone suggest extreme functional impairment and are therefore useful to guide the development of performance boundary conditions to combine with the performance estimates from the regression analysis estimates. Figure 40 provides the dose/time framework for the numerical performance mapping process described in Sec. 5, which follows.

SECTION 5

DOSE/TIME PERFORMANCE MAPPING

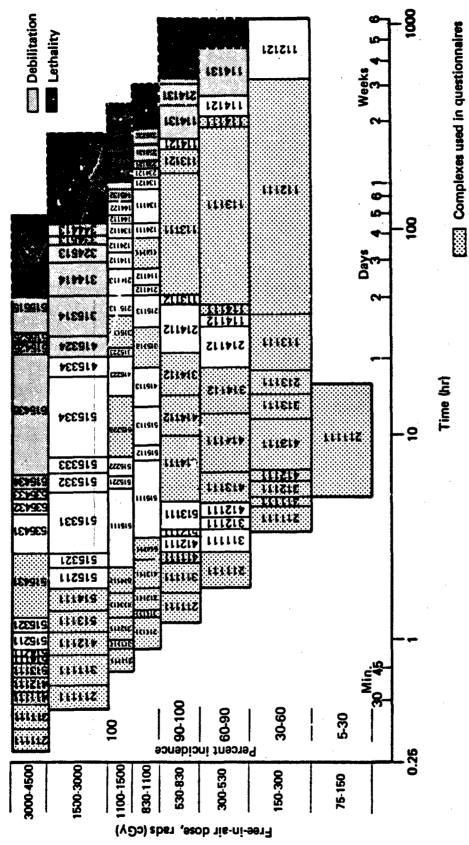
In the last section, a dose/time framework of symptom complexes was constructed; here, the quantitative relationship of crewmember performance with dose and postexposure time is established. The procedure consists of a one-to-one numerical mapping of crewmember performance values obtained from the regression analysis onto the dose/time framework of symptom complexes. Through numerical methods described below, we extend the input performance values from the regression analysis (Sec. 3), ranging from 0 to 100 percent, to produce output performance surfaces and isoperformance contour levels as a function of dose and postexposure time. The discussion that follows details the procedure and lists the numerical values used to obtain the performance dose/time output relationship.

INPUT DATA

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Performance values developed from the regression analysis of the combat crew questionnaire responses, together with the appropriate dose and time values, constitute the basic input data. The crew questionnaire responses on which the regression analysis is based do not correspond to all symptom complexes indicated in Fig. 41, owing to a limitation on the number of symptom complexes allowed in the combat crew questionnaires [Glickman et al., 1983]. However, a substantial portion of the dose/time domain, shown by the lightly shaded areas, corresponds to the symptom complexes where questionnaire response data were obtained.

Table 29 lists the input values used for the dose/time performance mapping. For each dose range, the symptom complexes, time canges, times, and corresponding performance predictions from the regression analysis are given. The performance values are for the chief of section of the gun crew, as a generic case, although the same input format holds for all crew positions (see Appendix I). Graphically, the time range values correspond to the time boundaries of the symptom complex rectangles shown



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Figure 41. Symptom complexes including those from questionnaires.

in Fig. 41. The time value where performance input is specified is the midpoint of the horizontal length of those rectangles. Since the time axis is logarithmic, the midpoint is given by the square root of the product of the time boundaries.

Referring to Fig. 41, input boundary conditions are specified at the outer periphery of the connected collection of symptom complex areas. This is done by specifying the performance with a series of relationships described below that designate where the performance is 100 percent (symptom-free) or assumed to be 0 percent (extreme symptom severity or lethality).

COMPUTATIONAL PROCEDURE

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In order to create a three-dimensional representation of performance as a function of dose and time, we take the symptom map (Fig. 41) plus imposed boundary conditions to build a smooth surface that both covers the regions of interest and passes through each performance input data point. To do this, a "french curve" algorithm (FCA) is used to translate the input data into an evenly spaced (logarithmic) grid of performance predictions for 18 values of dose and 39 values of time.

We chose the particular dose/time grid structure to allow full resolution of the underlying symptom map without adding an excessive amount of easily interpolated information. Within the areas defined by boundary conditions there are 143 irregularly spaced input points and about 400 output values. Since the only regularities in the structure of the input data are the 8 dose bands, the dose grid lines are chosen to correspond to the middle of the bands to the extent possible. No such regularity is present in the time structure of the input data, so the grid lines are chosen for calculational convenience.

Figure 42 shows the output grid structure, along with the locations assigned to the input data and the imposed boundaries. The dose grid lines are indexed i, where i = 1, 2, ..., 18, which correspond to dose values listed in Table 30, given by

$$D_{i} = 10^{(0.11i+1.67609)}$$
 rads (cGy) . (21)

Table 29. Input data for dose/time analysis of gun crew, chief of section.

Dose Range [rads (cGy)] Complex	Time Range (hr)		Time (hr)	Performance Value for Input Data	
75-150	211111	5.00	18.00	9.49	0.7226	
150-300	211111	3.40	4.50	3.91	0.7226	
,	311111	4.50	5.00	4.74	0.6751	
	312111	5.00	6.00	5.48	0.6341	
	412111	6.00	6.80	6.39	0.5804	
	413111	6.80	12.00	9.03	0.5357	
	313111	12.00	16.00	13.86	0.5912	
	213111	16.00	21.00	18.33	0.6444	
	113111	21.00	40.00	28.98	0.6943	
	112111	40.00	540.00	146.97	0.7314	
	112121	540,00	1060.00	756.57	0.6568	
300-530	211111	1.80	2.70	2.20	0.7226	
	311111	2.70	3.50	3.07	0.6751	
	312111	3.50	3.90	3.69	0.6341	
	412111	3.90	4.60	4.24	0.5804	
	413111	4.60	6.60	5.51	0.5357	
	414111	6.60	13.00	9.26	0.4904	
	314112	13.00	22.00	16.91	0.4386	
	214112	22.00	35.00	27.75	0.4947	
	114112	35.00	40.00	37.42	0.5510	
	114111	40.00	45.00	42.43	0.6545	
	113111	45.00	320.00	120.00	0.6943	
	114111	320.00	360.00	339.41	0.6545	
	114121	360.00	450.00	402.49	0.5712	
	114131	450.00	780 00	592.45	0.4836	
	134131	780.00	1080.00	917.82	0.3108	
530-830	211111	1.20	1.70	1.43	0.7226	
	311111	1.70	2.40	2.02	0.6751	
	411111	2.40	2.70	2.55	0.6238	
	412111	2.70	3.25	2.96	0.5804	
	512111	3.25	3.50	3.37	0.5246	
	513111	3.50	4.80	4.10	0.4793	
	514111	4.80	10.00	6.93	0.4343	
	414112	10.00	16.00	12.65	0.3840	
	314112	16.00	26.00	20.40	0.4386	
	214112	26.00	45.00	34.21	0.4947	
	113112	45.00	50.00	47.43	0.5953	
	113111	50.00	190.00	97.47	0.6943	
	113121	190.00	250.00	217.95	0.6149	
•	114121	250.00	280.00	264.58	0.5712	
	114131	280.00	410.00	338.82	0.4836	
	214131	410.00	520.00	461.74	0.4276	

Table 29. Input data for dose/time analysis of gun crew, chief of section (Continued).

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Dose Range		Time Range (hr)		Time	Performance Value for Input Data	
[rads (cGy)]	Complex			(hr)		
530-830	314133	520.00	630.00	572.36	0.2000	
(cont.)	424133	630.00	760.00	691.95	0.1216	
•	434143	760.00	910.00	831.62	0.0633	
	444153	910.00	1080.00	991.36	0.0319	
830-1100	211111	0.90	1.30	1.08	0.7226	
	311111	1.30	1.40	1.35	0.6751	
	312111	1.40	1.80	1.59	0.6341	
	4.3111	1.80	2.50	2.12	0.5357	
•	514111	2.50	3.20	2.83	0.4343	
	515111	3.20	7.60	4.93	0.3904	
•	515112	7.60	9.00	8.27	0.2932	
	515113	9.00	14.00	11.22	0.2118	
	415113	14.00	22.00	17.55	0.2519	
	315113	22.00	35.00	27.75	0.2968	
	215113	35.00	50.00	41.83	0.3460	
	214112	50.00	56.00	52.91	0.4947	
	114112	56.00	67.00	61.25	0.5510	
	114111	67.00	92.00	78.51	0.6545	
	124111	92.00	110.00	100.60	0.5680	
	134111	110.00	160.00	132.66	0.4771	
	134121	160.00	180.00	169.71	0.3908	
	234121	180.00	190.00	184.93	0.3386	
	235121	190.00	200.00	194.94	0.2992	
	235131	200.00	260.00	228.04	0.2309	
	325232	260.00	320.00	288.44	0.1730	
	315343	320.00 360.00	360.00	339.41	0.1138	
	415343 414344	410.00	410.00 460.00	384.19 434.28	0.0930 0.0622	
	515354	460.00	520.00	489.08	0.0359	
1100-1500	211111	0.70	0.90	0.79	0.7226	
1100-1500	311111	0.90	1.00	0.75	0.6751	
	312111	1.00	1.30	1.14	0.6341	
	413111	1.30	1.70	1.49	0.5357	
	514111	1.70	2.30	1.98	0.4343	
	515111	2.30	5.30	3.49	0.3904	
	515221	5.30	5.70	5.50	0.2965	
	515222	5.70	8.00	6.75	0.2144	
	515223	8.00	16.00	11.31	0.1502	
	415223	16.00	25.00	20.00	0.1814	
	315223	25.00	27.00	25.98	0.2174	
	315113	27.00	40.00	32.86	0.2968	
	215113	40.00	50.00	44.72	0.3460	
	214113	50.00	66.00	57.45	0.3881	

Table 29. Input data for dose/lime analysis of gun crew, chief of section (Continued).

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Dose Range [rads (cGy)]	Complex	Time Range (hr)		Time (hr)	Performance Value for Input Data	
1100-1500	11/112	66.00	80.00	72.66	0.5510	
	114112	80.00	92.00	85.79	0.4600	
(cont.)	124112			100.60	0.3715	
i	134112	92.00	110.00 120.00	114.89	0.3713	
	144112	110.00				
	144122	120.00	140.00	129.61	0.2238	
	145132	140.00	160.00	149.67	0.1446	
*	245232	160.00	210.00	183.30	0.1121	
	345342	210.00	260.00	233.67	0.0622	
	445443	260.00	300.00	279.29	0.0311	
	454454	300.00	340.00	319.37	0.0120	
	545454	340.00	420.00	377.89	0.0115	
1500-3000	211111	0.45	0.60	0.52	0.7726	
•	311111	0.60	0.84	0.71	0.6751	
	412111	0.84	1.10	0.96	0.5804	
	513111	1.10	1.40	1.24	0.4793	
•	514111	1.40	1.80	1.59	0.4343	
	515211	1.80	2.30	2.03	0.3748	
	515321	2.30	2.70	2.49	0.2829	
	515331	2.70	5.40	3.82	0.2171	
	515332	5.40	6.60	5.97	0.1523	
	515333	6.60	8.00	7.27	0.1042	
	515334	8.00	20.00	12.65	0.0701	
	415334	20.00	24.00	21.91	0.0863	
	415324	24.00	32.00	27.71	0.1184	
	315314	32.00	50.00	40.00	0.1932	
	314414	50.00	72.00	60.00	0.2118	
	324513	72.00	86.00	78.69	0.2123	
	334513	86.00	96.00	90.86	0.1576	
	344413	96.00	110.00	102.76	0.1218	
	354523	110.00	140.00	124.10	0.0596	
	355533	140.00	170.00	154.27	0.0358	
	455543	170.00	220.00	193.39	0.0204	
	555554	220.00	270.00	243.72	0.0000	
·	555555	270.00	300.00	284.61	0.0000	
2000 / 500				\		
3000-4500	211111	0.28	0.36	0.32	0.7226	
	311111	0.36	0.48	0 42	0.6751	
	411111	0.48	0.56	0\52	0.6238	
	412111	0.56	0.66	0.61	0.5804	
	513111	0.66	0.77	0.71	0.4793	
	514111	0.77	0.84	0.80	0.4343	
	514211	0.84	0.90	0.87	0.4181	
	515211	0.90	1.10	0.99	0.3748	

Table 29. Input data for dose/time analysis of gun crew, chief of section (Concluded).

Dose Range [rads (cGy)]	Complex	Time Range (hr)		Time (hr)	Performance Value for Input Data	
3000-4500	515321	1.10	1.30	1.20	0.2829	
(cont.)	515431	1.30	2.70	1.87	0.2061	
	535431	2.70	4.20	3.37	0.1111	
	535432	4.20	5.00	4.58	0.0749	
	535433	5.00	5.60	5.29	0.0498	
	515434	5.60	6.60	6.08	0.0659	
	515435	6.60	26.00	13.10	0.0437	
	515425	26.00	30.00	27.93	0.0610	
	515525	30.00	33.00	31.46	0.0573	
	515515	33.00	55.00	42.60	0.0796	
	535515	55.00	70.00	62.05	0.0400	
	555515	70.00	91.00	79.81	0.0197	
	555525	91.00	110.00	100.05	0.0139	
	555535	110.00	120.00	114.89	0.0000	

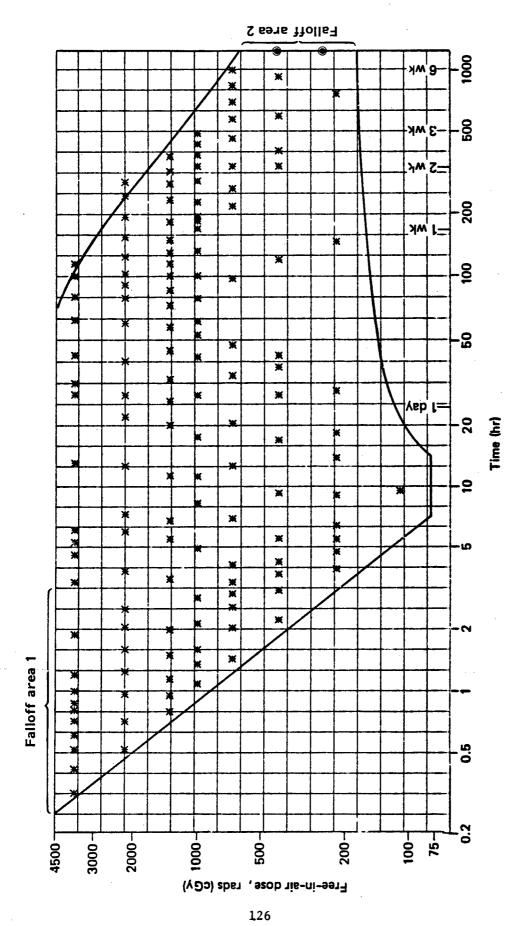


Figure 42. Data points and boundaries.

Table 30. Dose/time grid lines.

	Dose (free-in-air)		Time				
Range [rads (cGy)]	Index (i)	Grid Line [rads (cGy)]	Index (j)	Grid Line (hr)	Index (j)	Grid Line (hr)	
75-150	1	61.11	1	0.20	21	19.95	
	2	78.72	2	0.25	22	25.12	
	3	104.42	3	0.32	23	31.62	
	4	130.65	4	0.40	24	39.81	
150-300	5	168.30	5	0.50	25	50.12	
	6	216.81	6	0.63	26	10. د ع	
	7	279.32	7	0.79	27	79.43	
300-530	8	359.82	8	1.00	28	1600	
	9	463.55	9	1.26	29	125.89	
530-830	10	597.17	10	1.58	30	158.49	
	11	769.29	11	2.00	31	199.53	
830-1100	12	991.04	12	2.51	32	251.19	
1100-1500	13	1276.71	13	3.16	33	316.23	
1500-3000	14	1644.72	14	3.98	34	398.11	
	15	2118.81	15	5.01	35	501.19	
	16	2729.55	16	6.31	36	630.96	
3000~4500	17	3516.35	17	7.94	37	794.33	
	18	4529.94	18	10.00	38	1000.00	
		est ap.	19	12.59	39	1258.93	
			20	15.85			

Similarly, the time grid lines, indexed by j, j = 1, 2, ..., 39, represent time values listed in Table 30, and are given by

$$t_j = 10^{(0.10j-0.8)}$$
 hr. (22)

Note that the outermost grid lines in both cases fall just outside the area covered by the symptom map.

The boundary conditions were chosen by making a priori assumptions regarding the extremes where performance is 100 percent (nondegraded) or

O percent (totally degraded). Those particular boundary conditions were derived to ensure a smooth transition of the performance surface between the boundaries and the interior regions. The functional forms of the following boundary value formulas are not based on any specific theoretical model, but yield curves that are not inconsistent with the data and represent the perceived effects of radiation exposure on humans at the boundary extremes. Those boundary conditions, specified in terms of performance fraction p, will be described in terms of four areas of the grid in the same manner in which they were implemented in the analysis. Dose values are in rads (cGy), time in hours.

1. Upper edge (D = 4529.928) (23)
$$0.1995 \le t \le 0.2606$$
: $p = 1.0$
$$0.2606 \le t \le 3.1623$$
: $p = (1 + \varepsilon) \exp [-(a + b \log_{10} t)] - \varepsilon$
$$a = 1.32819$$
$$b = 2.27430$$
$$\varepsilon = 0.0928716$$
$$3.1623 \le t \le 1258.925$$
: $p = 0$.

The shape and effect of this boundary condition are particularly evident on the three-dimensional plots and correspond to falloff area 1 indicated in Fig. 42.

2. Right edge (t = 1258.925) $61.107 \le D \le 168.303; \quad p = 1.0$ $597.161 \le D \le 4529.928; \quad p = 0$ $168.303 \le D \le 597.161; \quad \text{This falloff area, indicated in Fig. 42,}$ is the least well known on the grid. A smooth transition from the data area was achieved most often by setting

$$p = a - b \log_{10} D$$

 $a = 4.31952$
 $b = 1.58364$ (24)

for two points at D = 141.421 and D = 264.575. The french curve algorithm (discussed below) was then used to generate a

curve through these points (see Fig. 42). The actual shape is evident on the three-dimensional plots and corresponds to fall-off area 2 in Fig. 42.

$$\log_{10} D = \frac{1.43}{1 + \exp(a \log_{10} t - b)} + 2.44609$$

$$a = 2.32698$$

$$b = 6.00965.$$
(25)

This curve is easily seen on the contour plots.

4. p = 1.0 limit (left and lower boundary) $0.1995 \le t \le 0.2606$: All doses; same as upper edge limit $0.2606 \le t \le 6.9314$: $log_{10} D = 2.92609 - 1.25 log_{10} t$ $6.9314 \le t \le 13.8523$: D = 75.0 $13.8523 \le t \le 1258.9254$: $log_{10} D = a + b ln (log_{10} t - c)$ a = 2.16549 b = 0.0877468c = 1.105.

Again, this curve is clearly evident on the contour plots and in Fig. 42.

The actual procedure for generating time output data uses the FCA mentioned previously. That algorithm fits as smooth a curve as possible to irregularly spaced values for a single independent variable. Figure 43 shows the basic technique, which is to estimate the slope at two adjacent points and then find the intersection (if any) of their tangents. A new point on the curve is generated by dropping a perpendicular from that intersection to the line connecting the original points and choosing the new point halfway between. This procedure is done for each adjacent

Total
$$2N-1$$

$$s(p_2) = \frac{s_{12}(1/d_{12}) + s_{23}(1/d_{23})}{(1/d_{12}) + (1/d_{23})}$$

d45 \

$$s(p_3) = \frac{s_{23}(1/d_{23}) + s_{34}(1/d_{34})}{(1/d_{23}) + (1/d_{34})}$$

Figure 43. "French curve" algorithm.

, \$23,^d23

% perpendicular

pair of points, so if N points are originally given, N - 1 new points are generated. The entire procedure is then repeated on all those 2N - 1 points, etc., until a desired density of points is achieved.

The algorithm has many desirable properties. It is capable of finding a peak (or valley) higher (or lower) than either of the original points that straddle it. Also, the density of points will be greatest where the curve is changing most rapidly, which is where the most resolution is needed. Most important, the FCA yields a curve that always passes through each and every original data point.

For purposes of fitting to the performance data, a three-step procedure is used. The first step is to generate an essentially continuous curve for each of the eight original dose bands. Input data to the FCA consists of the performance and time values for each of the locations (asterisks) on a given row in Fig. 42. Also included are additional data points corresponding to the boundary condition, the edge of the grid, and halfway between. This is done at both ends of the dose band, and yields six extra data points. Thus, even for the lowest dose band, which has only a single performance input point, a total of seven points, ranging over the entire time range of the grid, is input to the FCA. The result is eight curves of performance versus time.

The second step is to generate 39 different "continuous" curves of performance versus dose, each corresponding to one of the time grid lines. Input data to the FCA are eight performance and dose values (from the eight curves generated in step one) plus additional points for the edge. of the grid and boundary conditions. This is done 39 times to yield the desired curves.

Finally, the third step is to generate 18 curves of performance versus time, corresponding to the dose grid lines instead of to the original dose bands. Each of these curves is found by using the FCA with input consisting of 39 data points (from the curves generated in step two) plus boundary conditions.

Three-dimensional plots (given in Sec. 6) result from plotting those 39 constant time curves and 18 constant dose curves as seen from the

appropriate perspective. Note that the tables of output values, given in Appendix J, contain only the performance values at the intersections of the grid lines, and thus do *not* reflect the full resolution shown in the plots.

CONTOUR PLOTS

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A similar procedure was used to generate contour plots. The first step, generating the eight performance-versus-time curves, is the same as above. Step two, however, is different. Instead of only 39 time-constant curves, a total of 875 such curves are generated. That procedure yields the performance surface to a very high resolution. (On the scale of Fig. 42, if those 875 vertical lines are drawn, the spacing between them would be less than the width of the lines, i.e., the figure would appear as a solid black block.) Each of these "continuous" curves is in fact not continuous, but consists of 885 points. Thus, the surface is represented by a massive array of 875 × 885 = 774,375 points.

Next, each and every one of those points is compared with each of its neighboring points. If one of them is greater than a specified contour level, and the adjacent point is less than that level, then a dot is drawn on the plot for the original point, which then becomes one of the points that forms the contour. The resulting plot is simply a pattern of small dots that appears to the eye as continuous contour lines.

This approach, though tedious, eliminates the need for fitting local analytic approximations to describe the surface, which is the procedure used by most traditional contour plot algorithms. As a result the very detailed resolution of the FCA is preserved in the final contour plots.

Using the numerical procedures detailed above, we describe three-dimensional crewmember performance surfaces and isoperformance contours as a function of dose and postexposure time. In the following section, the overall picture of crewmember performance provided by three-dimensional plots, as well as the isoperformance contours that enable numerical performance estimates to be made graphically is described.

SECTION 6

RESULTS AND DISCUSSION

This section details the relationships of individual crewmember performance with acute radiation dose and time after exposure. The relationships are expressed graphically, based on the calculational methods described in Sec. 5 for the 15 artillery, tank, and TOW combat crewmember positions. Comparisons of the performance of five different types of crewmembers according to task similarities are detailed as a function of dose and time following exposure. Also presented and discussed are the confidence bounds associated with our individual performance predictions in order to illustrate the conditional uncertainty associated with the regression predictions of Sec. 3.

PERFORMANCE SURFACES

Three-dimensional surface representations of the relationship of individual performance to dose and time following a single prompt exposure are shown in Figs. 44 through 58 for each of the 15 crewmembers. The figures provide an overall picture of individual performance as a function of dose and time. Individual performance in percent is expressed as the vertical axis, with dose and time along the horizontal axis. Dose and time are both expressed logarithmically in order to include the entire intermediate dose range of 75 to 4500 rads (cGy) and time (minutes to 6 weeks) on each graph. Accordingly, a visual distortion is introduced where the slope of the surface for small doses and/or early times appears much more pronounced than that of large doses and/or times.

The particular orientation of the axes with the large values of dose and time at the bottom of the graphs enables a more revealing view of the performance surface than if the axes were oriented in the conventional manner with the smaller values at the bottom. The orthogonal lines along the surface are the 18-dose by 39-dose grid lines specified in Sec. 5. The end segments of the grid lines extending to the axes are dashed to indicate the span between input data and specified boundary conditions (discussed in Sec. 5), also shown as dashed lines. Insofar

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Figure 44. Performance surface: gun crew, chief of section.

Percent performance

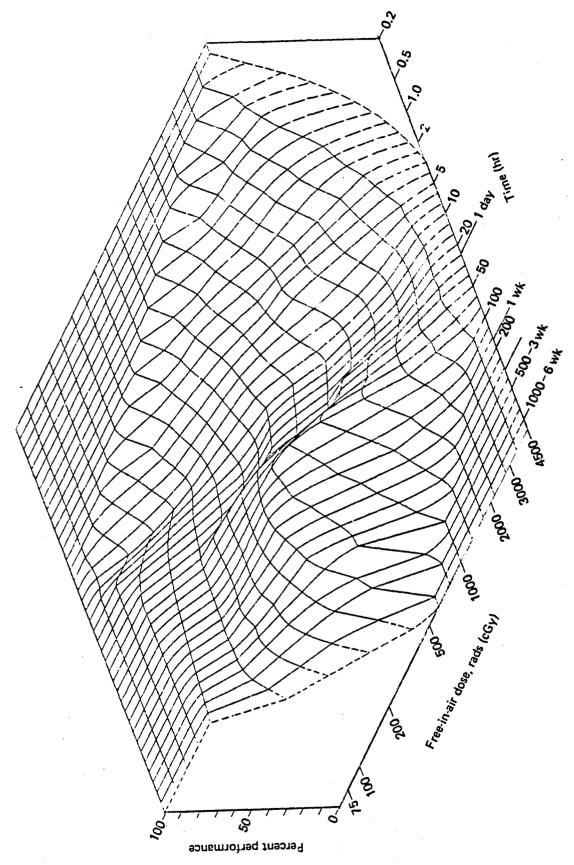


Figure 45. Performance surface: gun crew, gunner.

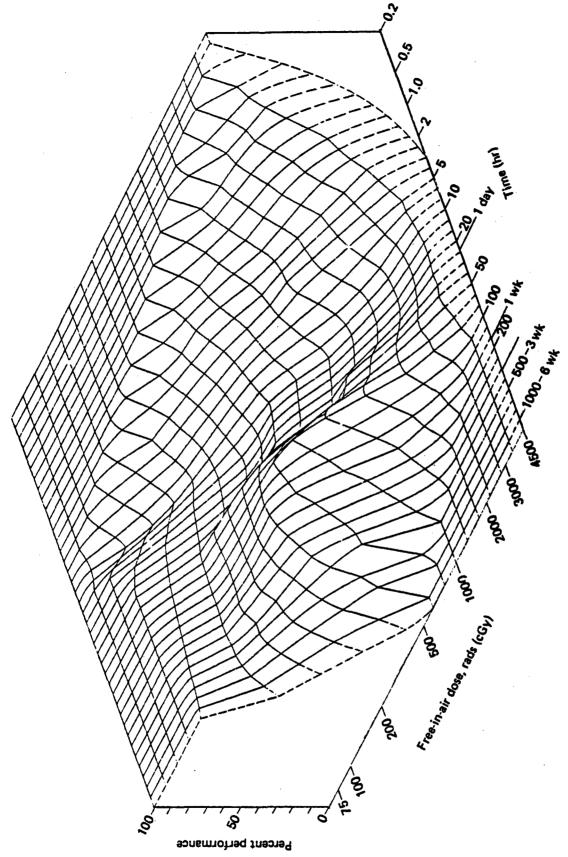


Figure 46. Performance surface: gun crew, assistant gunner.

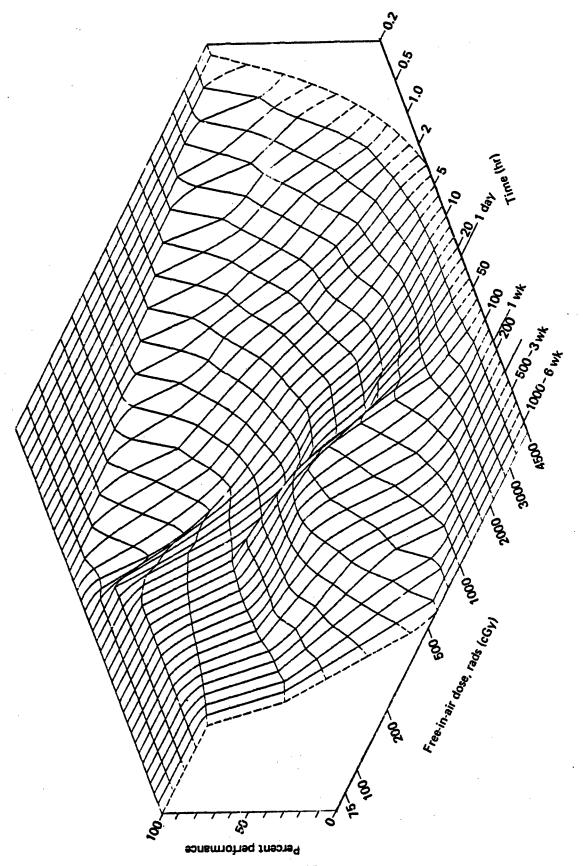


Figure 47. Performance surface: gun crew, loader.

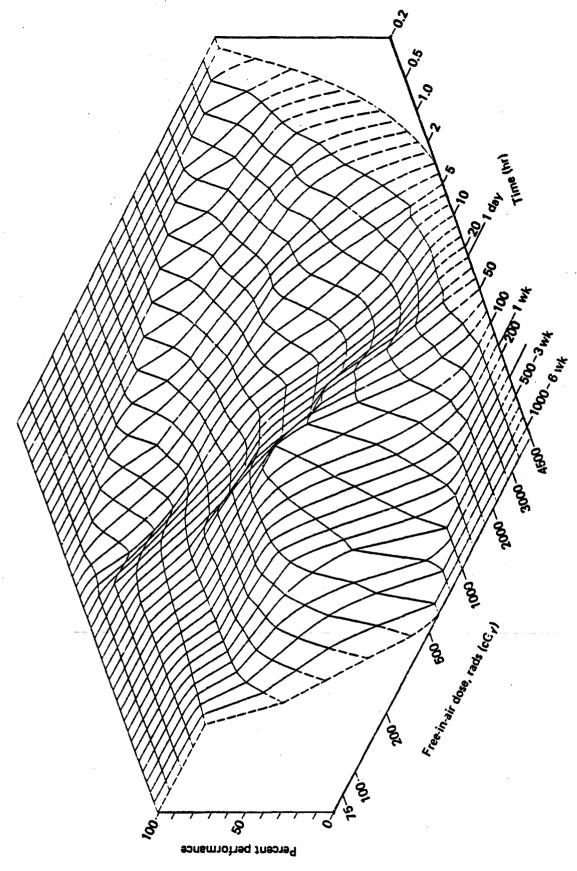
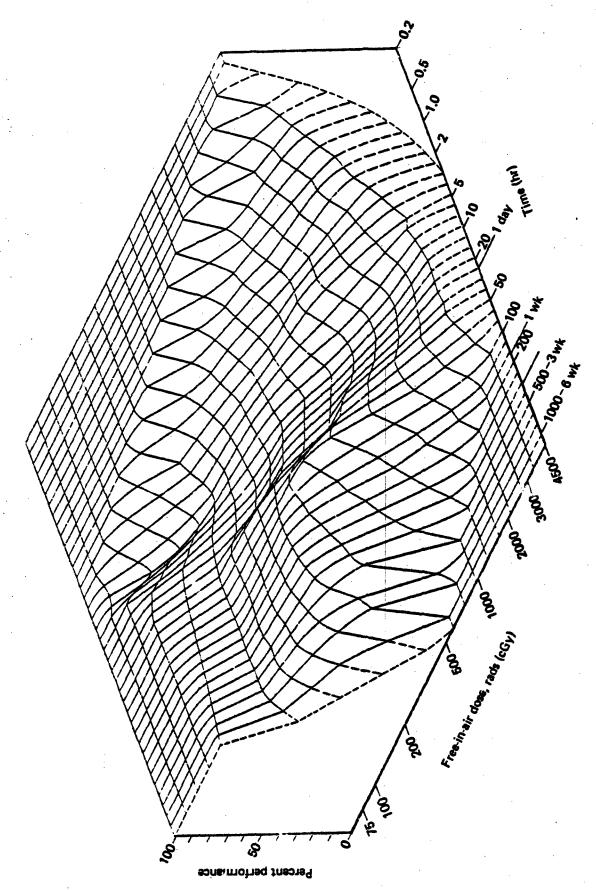


Figure 48. Performance surface: FDC crew, fire direction officer.



Performance surface: FDC crew, horizontal control operator. Figure 49.

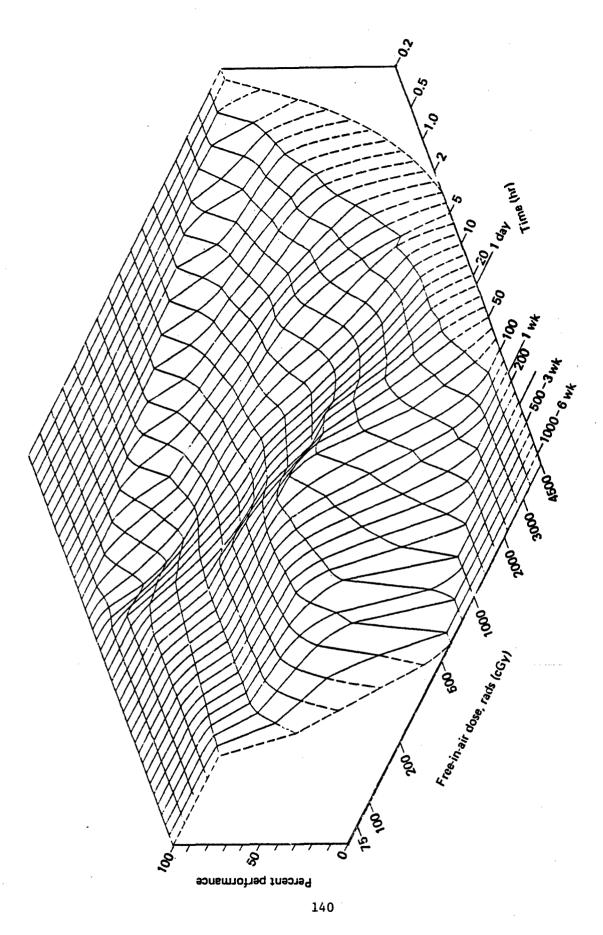


Figure 50. Performance surface: FDC crew, computer.

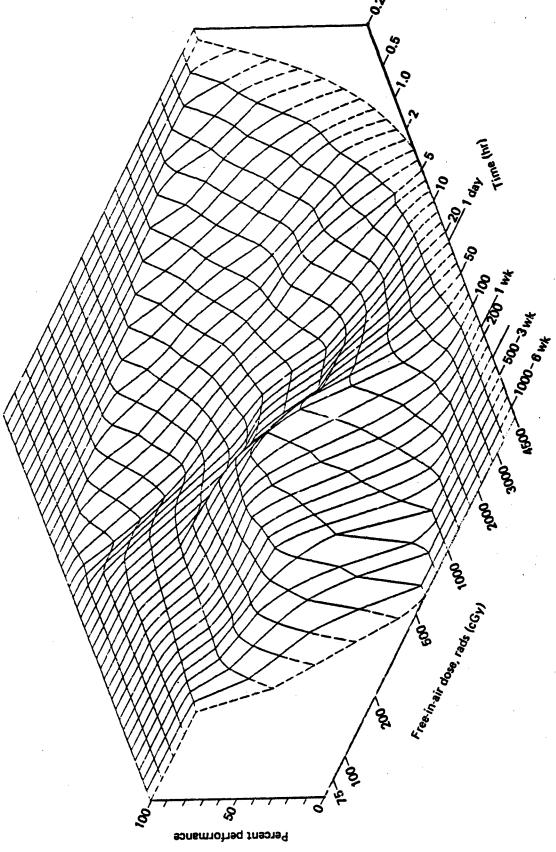


Figure 51. Performance surface: tank crew, tank commander.

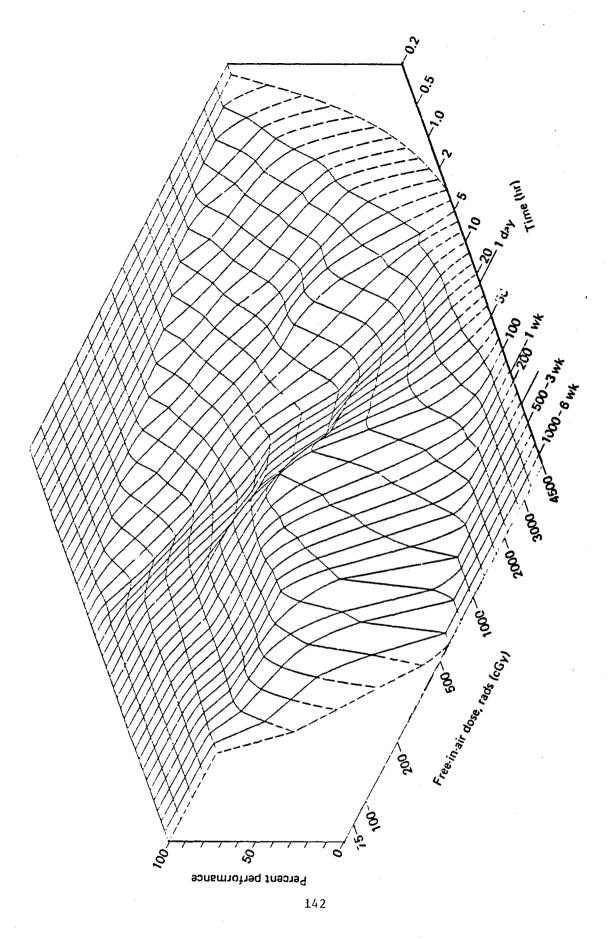


Figure 52. Performance surface: tank crew, gunner.

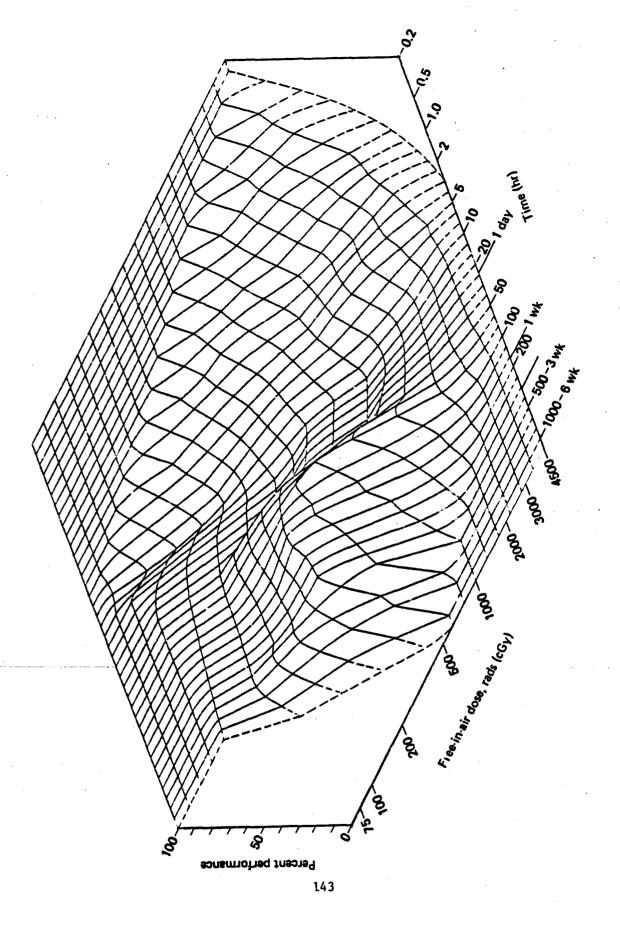


Figure 53. Performance surface: tank crew, loader.

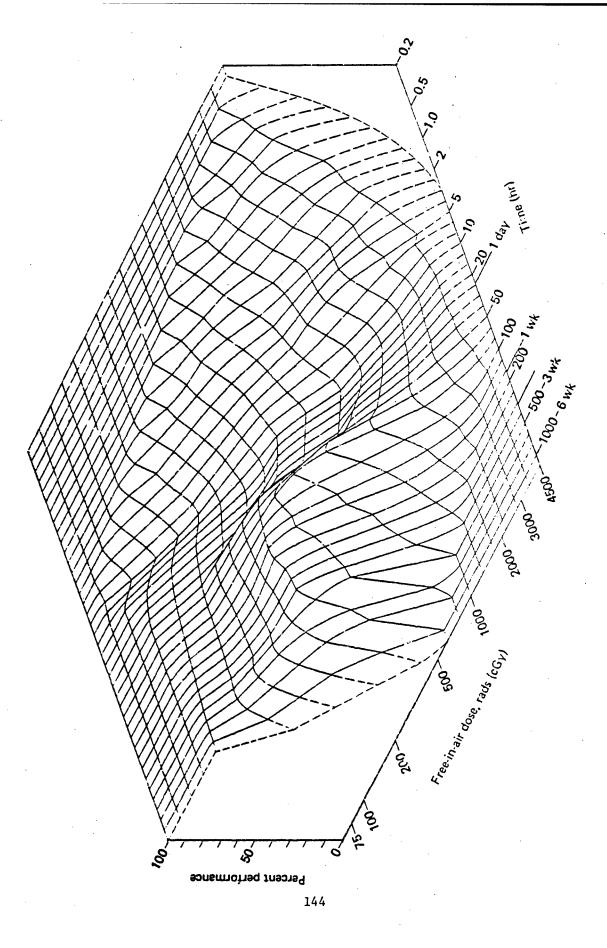


Figure 54. Performance surface: tank Crew, driver.

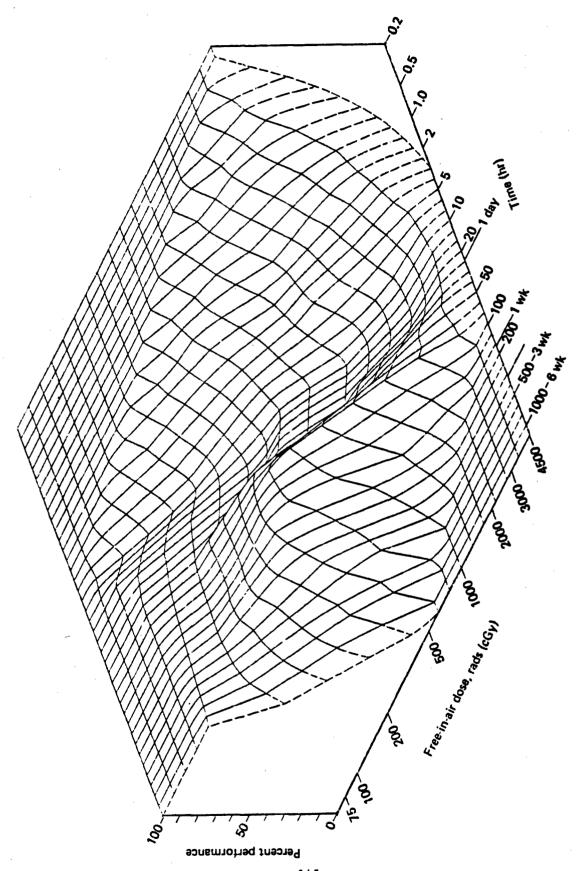


Figure 55. Performance surface: TOW crew, squad leader.

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Figure 56. Performance surface: TOW crew, gunner.

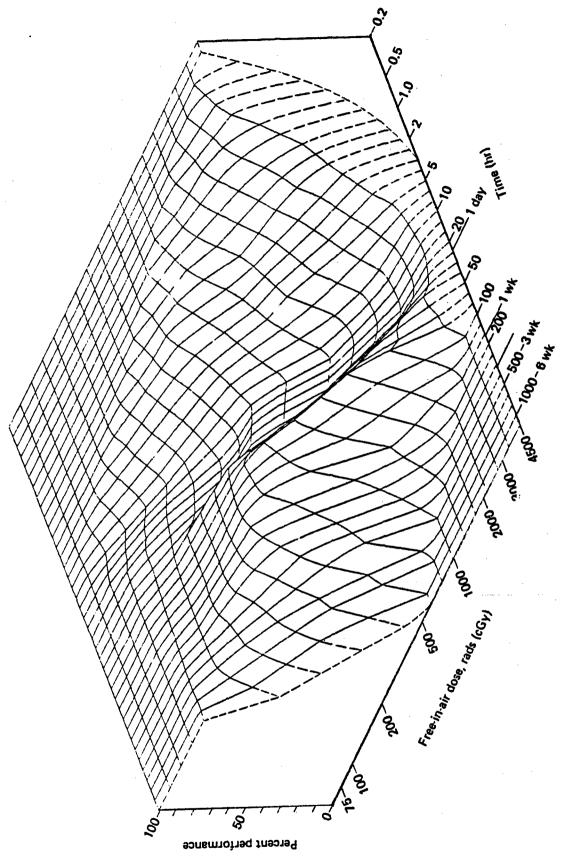


Figure 57. Performance surface: TOW crew, driver.

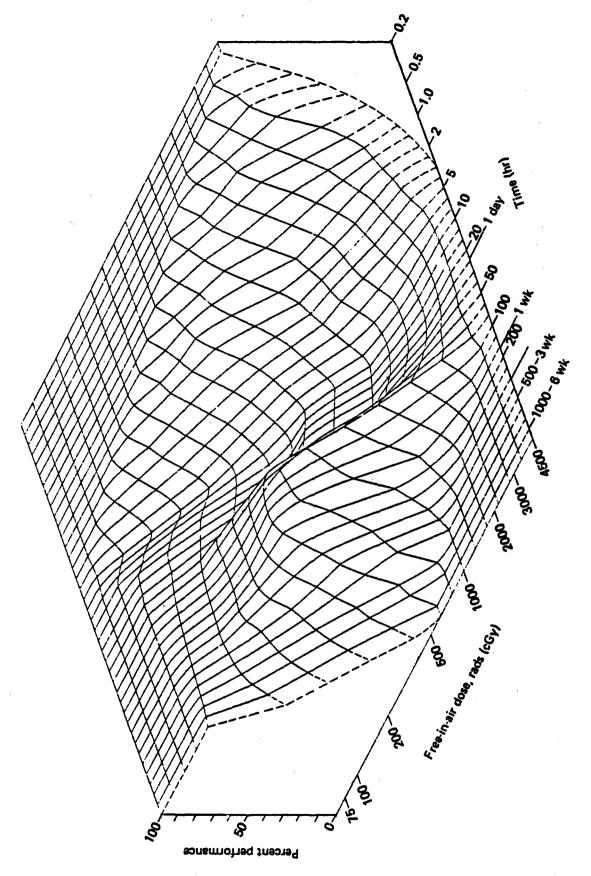


Figure 58. Performance surface: TOW crew, loader.

as the boundary conditions are not based explicitly on input data, the dashed portions reflect a greater degree of uncertainty as compared with the solid grid lines.

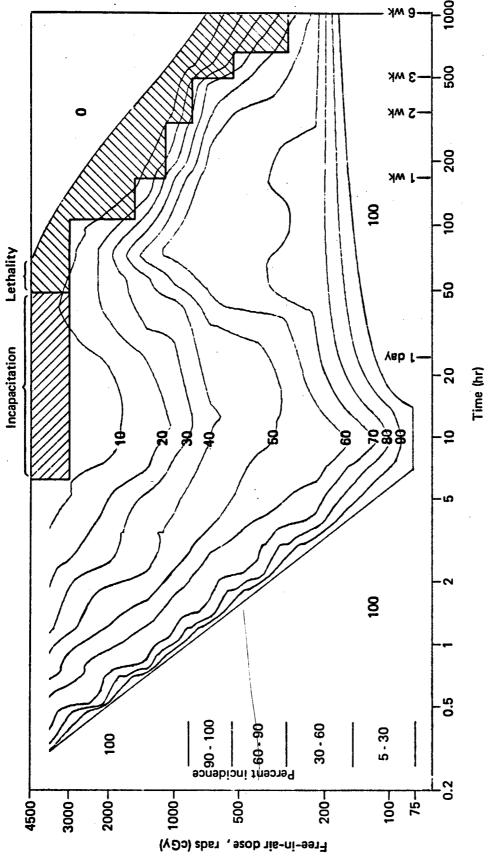
Surface depressions indicate where performance becomes degraded. The initial overall depression is related to the prodromal symptomatology, which includes nausea, vomiting, fatigue, weakness, and initial fluid loss [also hypotension and fever at the higher doses beginning at around 1100 to 1500 rads (cGy)]; gastrointestinal effects, because of their relatively lower expected incidence—10 to 30 percent [Baum et al., 1983]—are not included in Figs. 44 through 58. The broad rise in the performance surfaces toward the left side of the graphs is related to some remission of the prodromal symptoms, prior to the onset of delayed ones (manifest illness period) such as infection, bleeding, fever, lower gastrointestinal distress, fluid loss, and reoccurrence of symptoms such as nausea, vomiting, fatigability, and weakness. For doses exceeding around 600 rads (cGy), the height and width of the rise progressively disappear, reflecting reduced recovery consistent with the increasingly severe symptomatology [Baum et al., 1983].

At the high-dose edge of the plots, the downward slope of the surface near the boundary is more apparent the higher the performance estimates, e.g., as in Fig. 50 for the FDC computer crewmember. That effect is due to matching the boundary condition using the logit model for the regression predictions. For example, in excess of about 3 hr, the boundary condition is assumed to be zero, whereas the logit form predicts values that approach but do not equal zero.

ISOPERFORMANCE CONTOURS

Isoperformance levels for the 15 crewmembers as a function of dose and time after exposure are given in Figs. 59 through 73. The contour level plots, shown in increments of 10 percent, can be used to extract performance estimates. The plots also contain estimates of the percent incidence of those expected to surfer from the effects of radiation

Performance surfaces that include early lower gastrointestinal effects are provided in Appendix H.



gun crew, chief of section. Figure 59. Performance contours, 10 percent performance intervals:

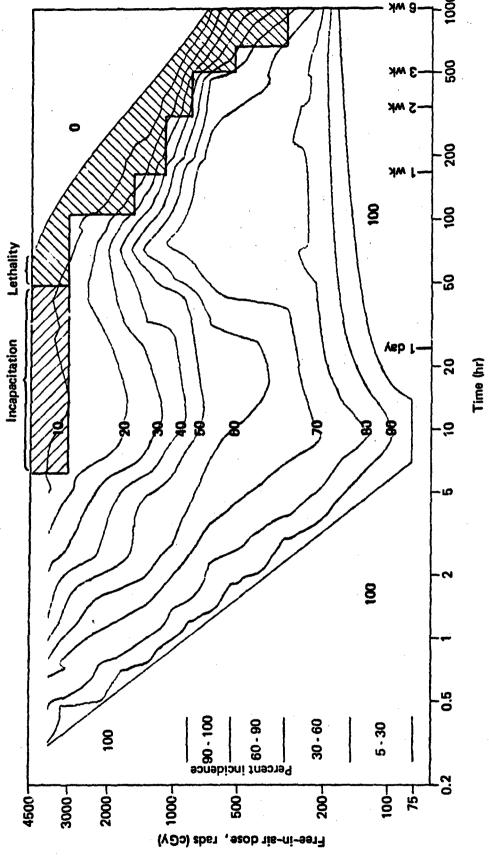
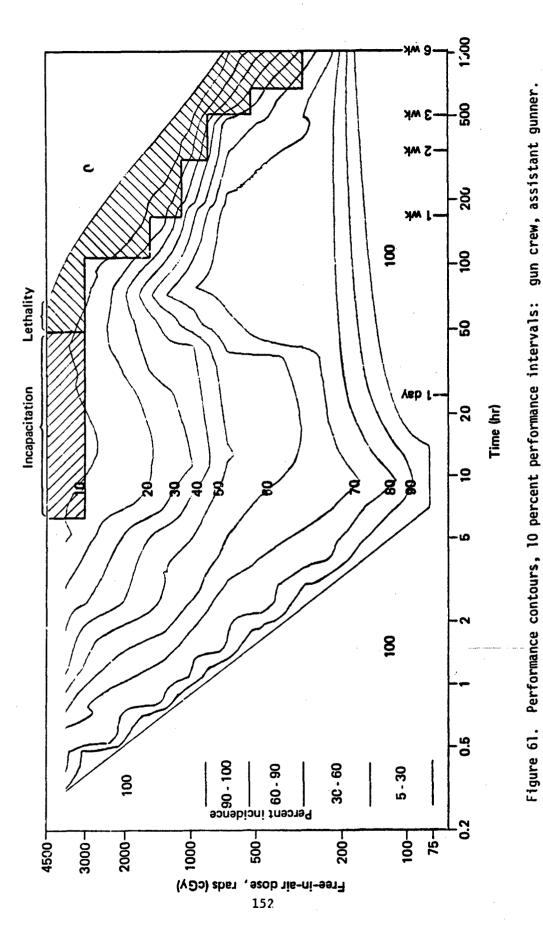
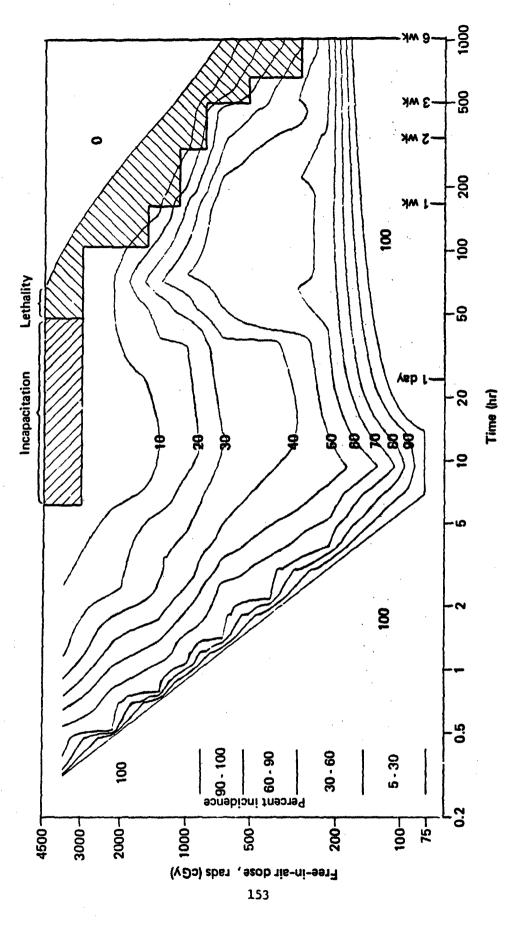


Figure 60. Performance contours, 10 percent performance intervals: gun crew, gunner.

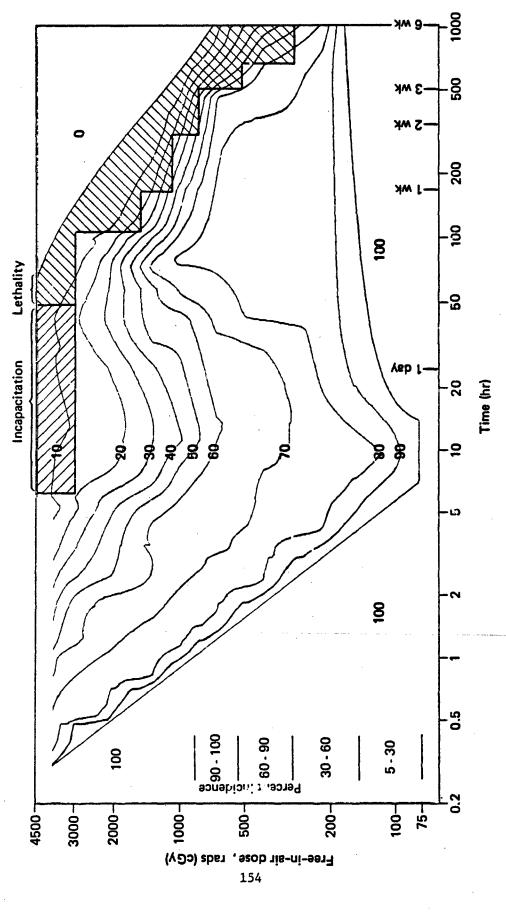




Performance contours, 10 percent performance intervals: gun crew, loader. Figure 62.

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Performance contours, 10 percent performance intervals: FDC crew, fire direction officer. Figure 63.

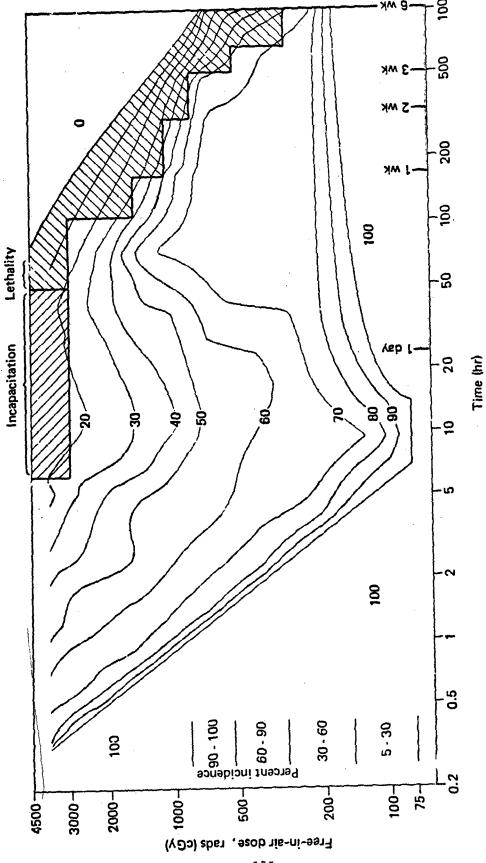
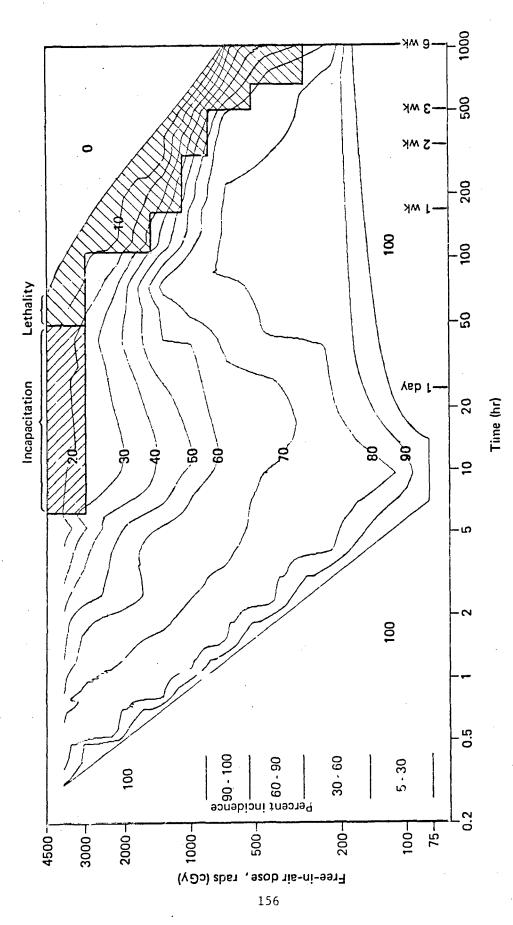
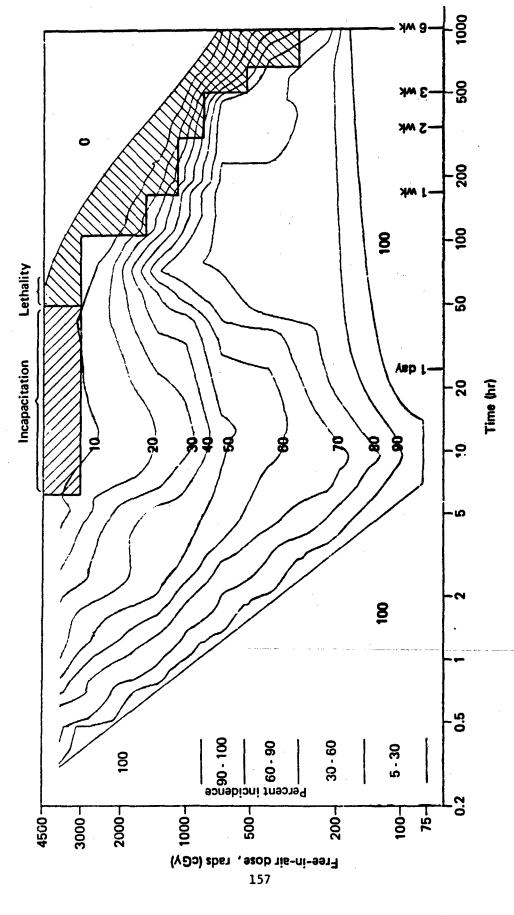


Figure 64. Performance contours, 10 percent performance intervals: FDC crew, horizontal control operator.



Performance contours, 10 percent performance intervals: FDC crew, computer. Figure 65.

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Performance contours, 10 percent performance intervals: tank crew, tank commander. Figure 66.

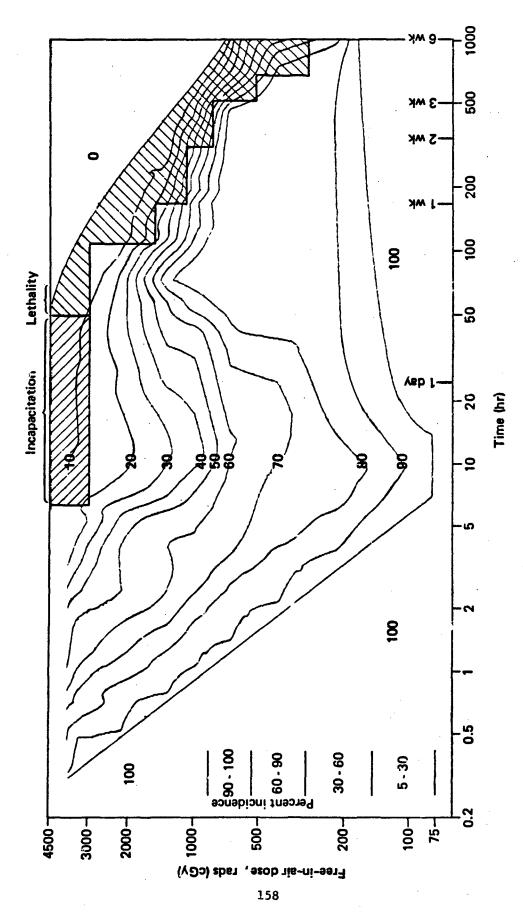


Figure 67. Performance contours, 10 percent performance intervals: tank crew, gunner.

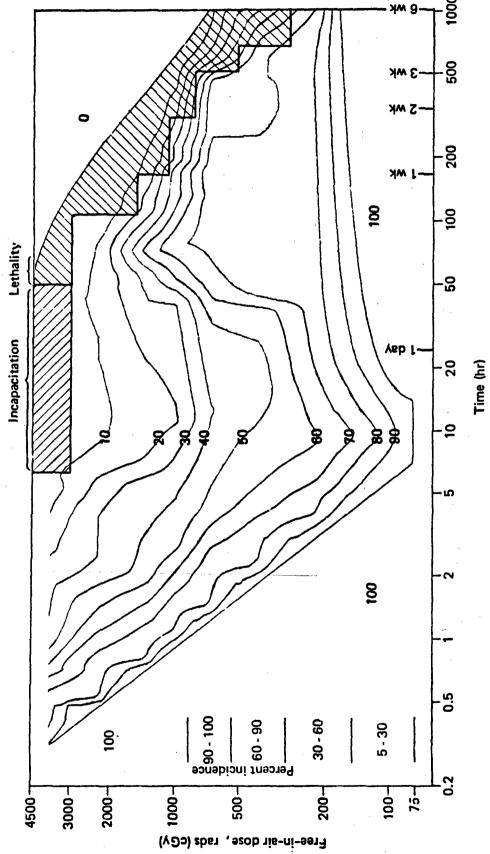


Figure 68. Performance contours, 10 percent performance intervals: tank crew, loader.

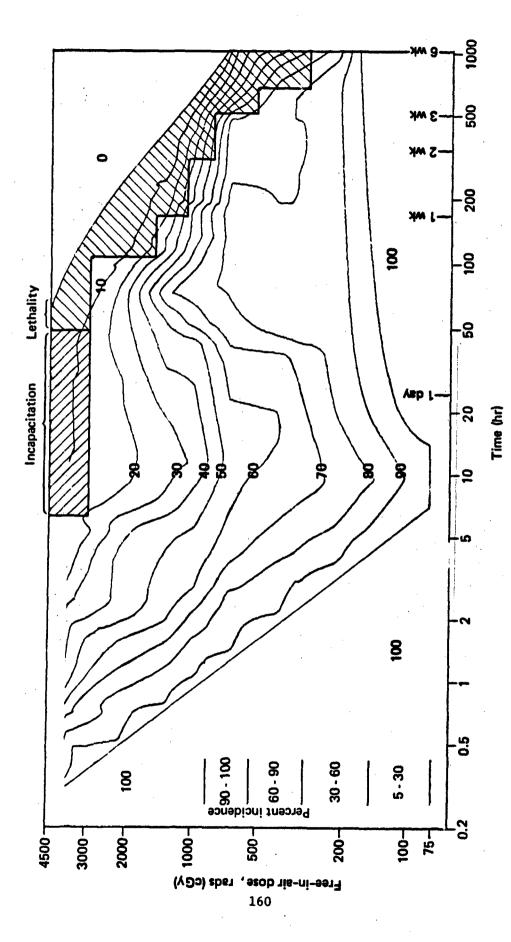


Figure 69. Performance contours, 10 percent performance intervals: tank crew, driver.

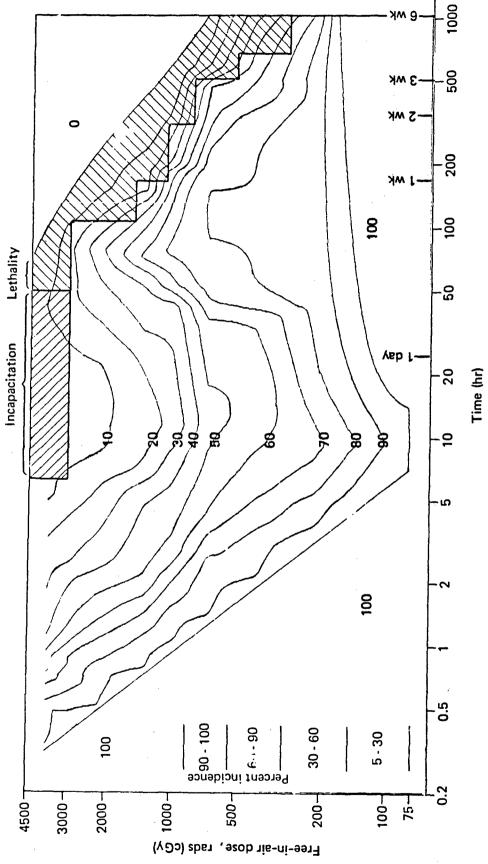
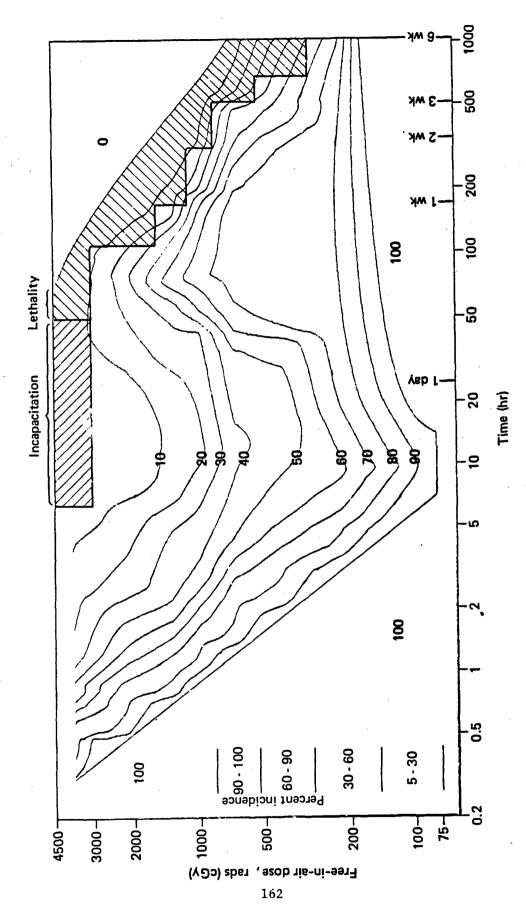
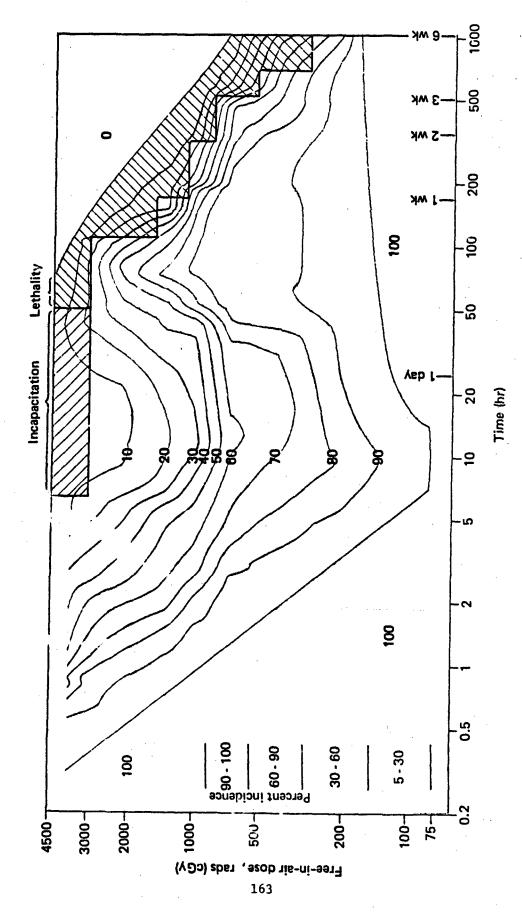


Figure 70. Performance contours, 10 percent performance intervals: TOW crew, squad leader.

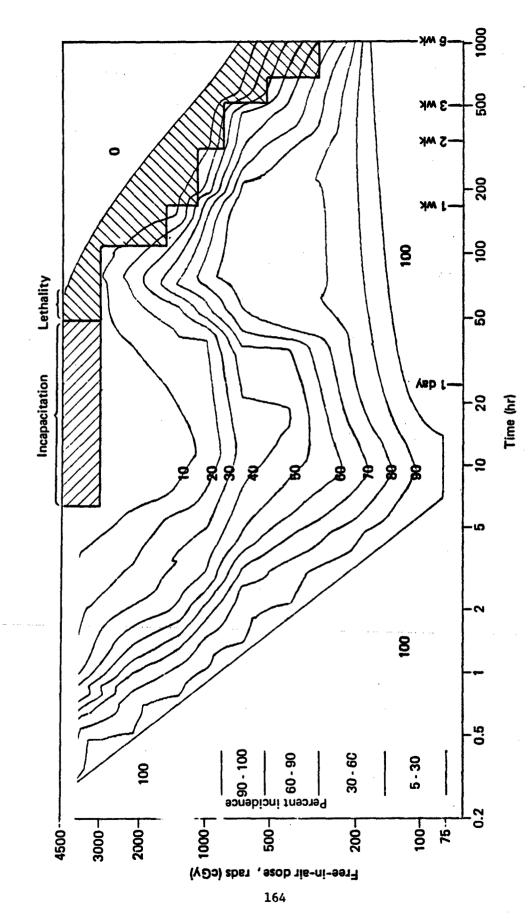


Performance contours, 10 percent performance intervals: TOW crew, gunner. Figure 71.



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Performance contours, 10 percent performance intervals: TOW crew, driver. Figure 72.



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Figure 73. Performance contours, 10 percent performance intervals: TOW crew, loads..

exposure based on Baum et al. [1983] which affect performance as indicated on the plots. The percent incidence is given along the left side of the plots for the designated dose rarges, commencing from 5 to 30 percent for the lowest dose range [75 to 150 rads (cGy)] and reaching 100 percent at and above 830 rads (cGy).

Any point along the isoperformance contour curves defines a dose level and postexposure time that correspond to the performance level of the contour. The performance profile over time, following exposure to a given dose, can be readily constructed from the performance contour plots by ascertaining the times where a given dose level intersects with the performance contour curves. For example, in Fig. 60 the estimated performance for the gun crew gunner exposed to 500 rads (cGy) would be 100 percent up to 1.5 hr following exposure; about 90 percent close to 1.8 hr; 80 percent at 3 hr; 70 percent at 4.5 hr; 60 percent at 10 hr; between 50 and 60 percent from 10 to 30 hr; 70 percent at 40 hr; between 70 and 80 percent from 40 hr to 2 weeks; etc.

The performance contour levels for all crewmember positions are constrained within a common dose/time boundary, since a uniform set of boundary conditions were specified [O percent for the upper-right-hand corner and top of the 4500 rads (cGy) dose level, and 100 percent on the left-hand and bottom portions].

However, we point out here that the stairstep boundary beginning at 48 hr for the highest dose range [3000 to 4500 rads (cGy)] indicates where lethality commences [Baum et al., 1983] (see also Figs. 40 and 41). The time increment between the stairstep boundary and the outermost curve in the upper-right-hand corner, which we designate as the zero performance boundary for the performance level computations, represents the period over which the vast majority of lethalities would be expected to take place. Accordingly, we believe that although our computations indicate some level of performance in the period shown by the contour curves, they should be regarded with extreme caution. The authors also point out that the period extending from about 7 to 48 hr for the highest dose range [3000 to 4500 rads (cGy)] is spanned by symptom complexes (Figs. 40 and 41) that correspond to symptom descriptions including "exhausted with almost no strength," "faints upon standing quickly,"

"in shock," and "prostrate" [Anno and Wilson, 1983]. Again, the performance contours in that region, which we term as "incapacitation" in the contour plots, should be similarly regarded with caution. Also, along the upper portion of the plots between 0.4 and 5 hr, we have not connected the contour lines to the upper boundary at the 4500 rad (cGy) level. That region represents an area of relative uncertainty, because of the effect of the imposed boundary condition where there are no explicit data (discussed on p. 149).

Along the left-hand edge of the contour plots near the boundary, the wave-like appearance of the 80 to 90 percent performance contour lines, as well as the 70 percent line for some cases, are a consequence of the selected discrete dose range structure (see Sec. 4) and the numerical mapping procedure described in Sec. 5. For convenience, those portions of the contour lines could be consider as straight lines, running diagonally between the "peaks and valleys," and be well within the uncertainty of the calculated values.

Differences in performance among the various crewmembers are more noticeable in the contour plots than in the three-dimensional surface plots. For example, let us examine the contour differences between the gun crew loader in Fig. 62 and the FDC crew computer in Fig. 65, which represent two extreme cases. The gun crew loader performs the most physically demanding set of tasks, which includes loading the heavy (about 100 lb) artillery projectile, whereas the computer in the FDC crew performs the least physically demanding tasks, which include selecting tabulated numerical data, performing computations with a hand-held calculator, and verbally communicating data.

CREWMEMBER ROLE GROUPS

Graphical comparisons of the performance contours have been made by dividing the 15 combat crewmembers into five different groups based on the similarity of combat tasks they perform in each crew; the five groups and crewmembers included in each are shown in Table 31. The numbers in the column labeled "Identification" help in labeling the plots discussed below. The last group listed, FDC, consists of the horizontal control

Table 31. Crewmember groups.

Group	Crewmember	Identification
Leader	Artillery-chief of section	1
	FDCfire direction officer	5
	Tanktank commander	8
	TOWsquad leader	12
Gunner	Artillerygunner	2
	Artilleryassistant gunner	3
	Tankgunner	9
	TOWgunner	13
Loader	Artilleryloader	4
	Tankloader	10
	TOWloader	15
Driver	Tankdriver	11
	TOWdriver	14
FDC	FDChorizontal control operator	6
	FDCcomputer	7

operator and the computer. Those crewmembers primarily perform cognitive, or the least physically demanding tasks. Graphical comparisons are made by plotting the contours for each of the five groups separately for three different performance levels: 30, 50, and 70 percent.

Thirty Percent Performance

Figures 74 through 78 are plots of the five groups at the 30 percent performance level. Figure 74 shows a fairly close grouping over dose and time with the fire direction officer generally at somewhat higher dose levels. Figure 75 shows a close grouping between the gunner and assistant gunner of the artillery crew, which makes sense, since they both perform essentially similar tasks. The tank and TOW gunners are at the high and low dose extremes, respectively. The loaders in Fig. 76 show a fairly consistent pattern—at least over the first two days following exposure—where the 50 percent performance level for the artillery, TOW, and tank loaders, respectively, are each at decreasing dose values. Since much of the loaders' tasks consist of handling

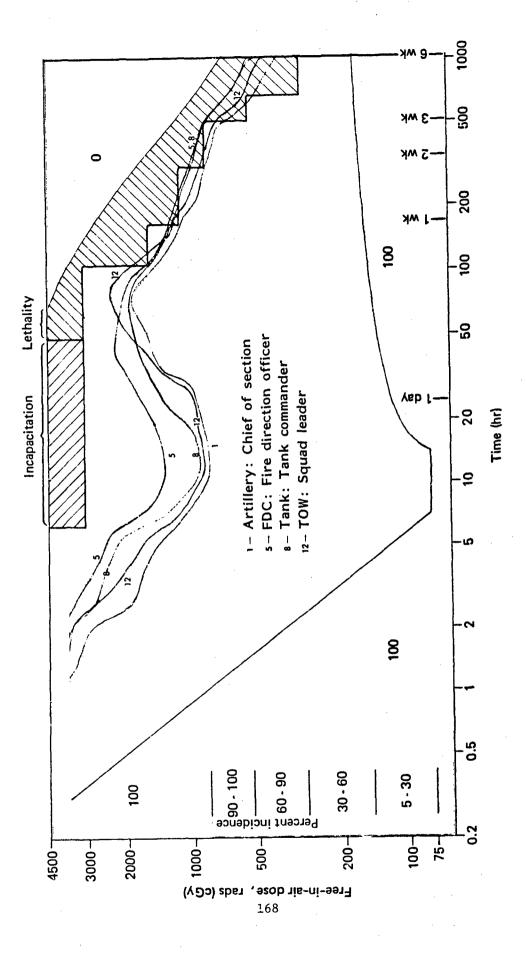


Figure 74. Crew leaders, 30 percent performance.

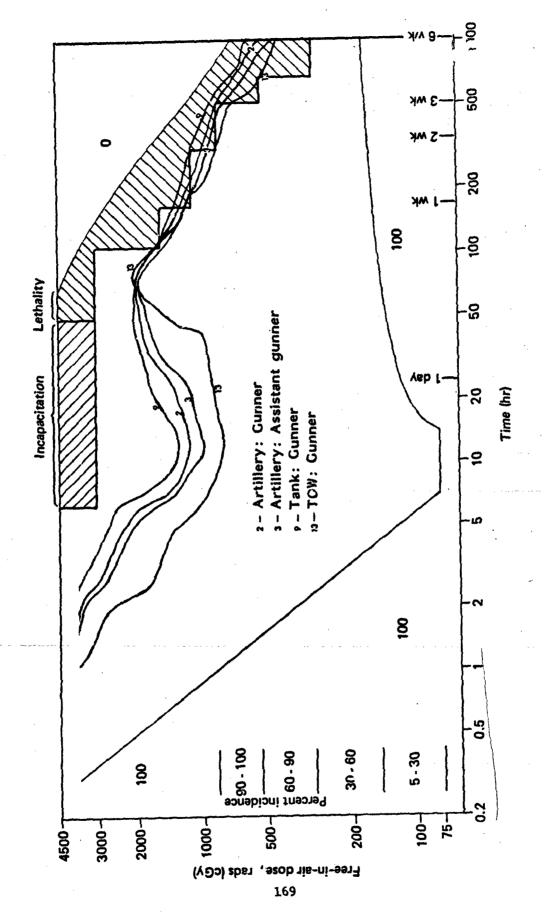


Figure 75. Crew gunners, 30 percent performance.

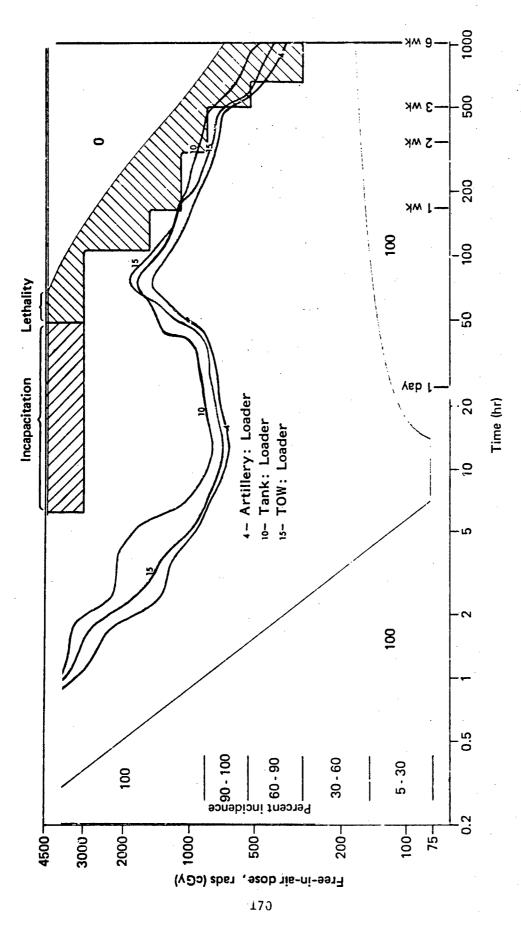


Figure 76. Crew loaders, 30 percent performance.

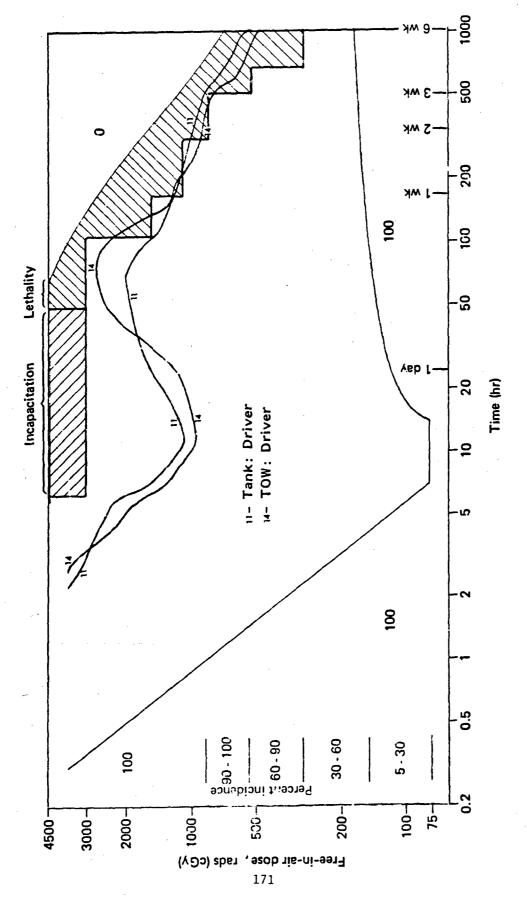


Figure 77. Crew drivers, 30 percent performance.

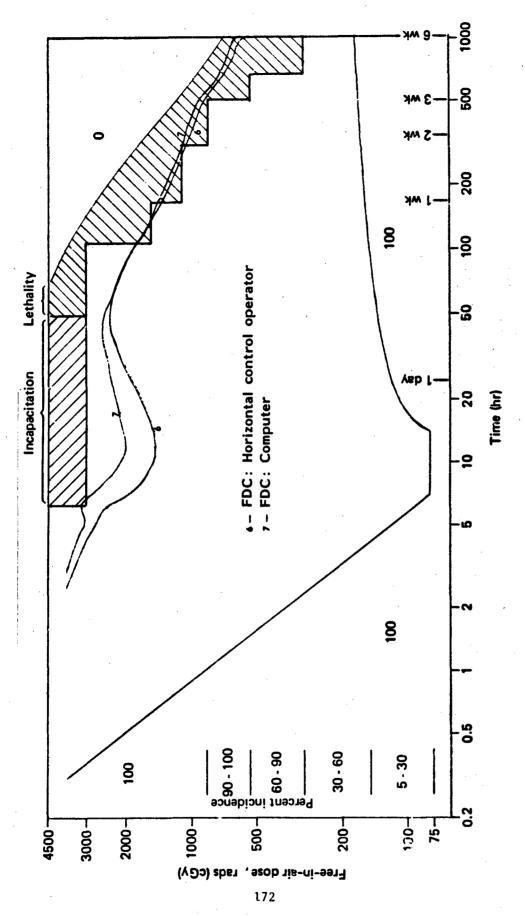


Figure 78. FDC crew, 30 percent performance.

munitions, the order of difficulty and the decreasing order of affecting dose are consistent with the weight of the munition, i.e., the artillery loader handles a 100 lb projectile, the TOW loader a 54 lb missile, and the tank loader a 30 lb projectile.

Figure 77 indicates a fairly close contour resemblance for the tank and TOW drivers except between about one and one-half to several days, where the TOW driver appears to require a somewhat higher dose to reduce performance to 30 percent. Figure 78 shows the two crewmembers that require the highest dose to reduce performance to 30 percent; as previously mentioned above, they have the least physically demanding tasks. In particular the computer is shown to be the least affected dosewise.

Fifty Percent Performance

The 50 percent performance contours for the five groups of crewmembers are given in Figs. 79 through 83. At this level, there is a relative widening of all the performance contours compared to the 30 percent level with the exception of the drivers in Fig. 82, which even become comparatively narrower. The widening is most apparent in the deviation toward lower doses of the artillery chief of section, TOW gunner, and artillery loader relative to the others in their respective groups. That is, lower doses that produce 50 percent performance, as compared with higher doses that produce 30 percent performance, have a relatively greater effect on performance for those positions as compared with the others in their respective groups. Such a widening effect is also seen for the horizontal control operator/computer group. However, since there are only the two members in the group, it is not readily apparent from the plots which position accounts for the widening. The driver group does not show the widening effect when comparing the 30 percent and 50 percent performance contours.

In Fig. 79, performance contours for the leaders of the tank and TOW crews are essentially the same, whereas the fire direction officer requires the highest dose and the artillery chief of section requires the lowest dose to be affected at the 50 percent performance level. The relative position of the contour for the chief of section is somewhat

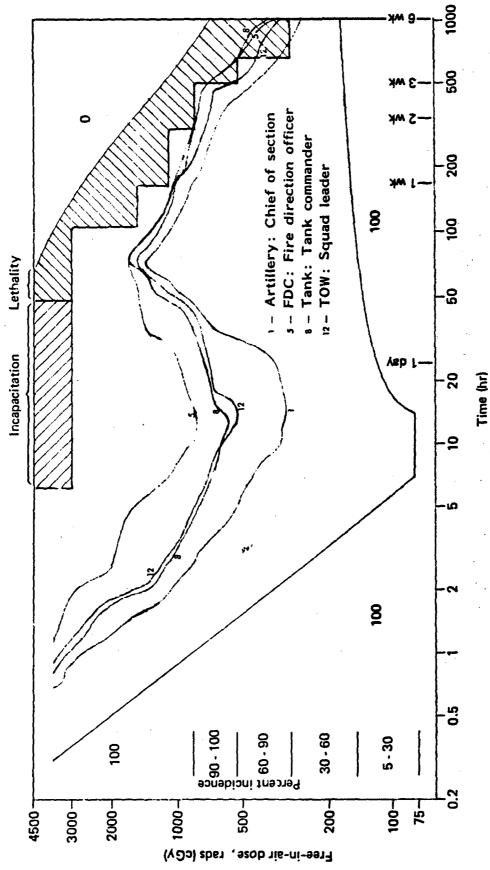


Figure 79. Crew leaders, 50 percent performance.

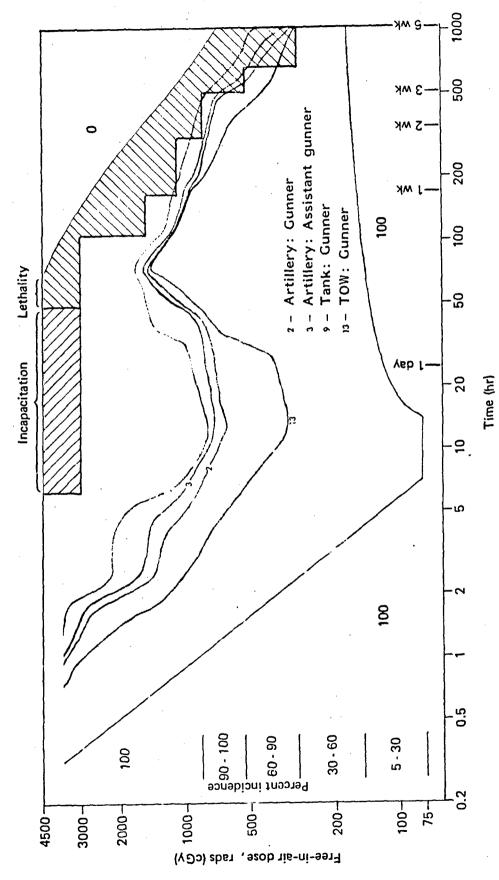
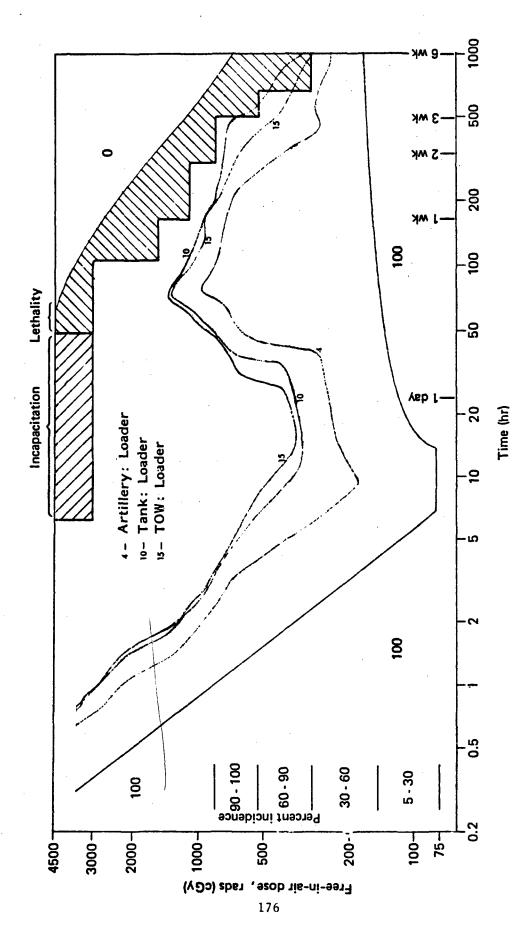
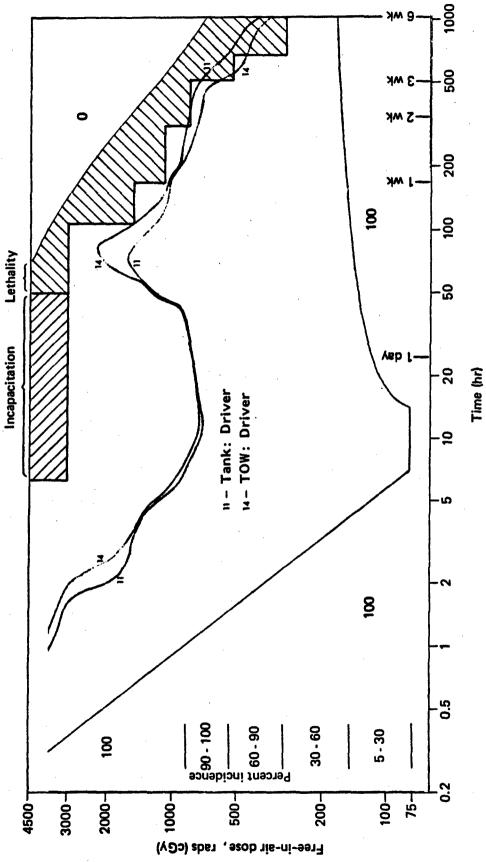


Figure 80. Crew gunners, 50 percent performance.



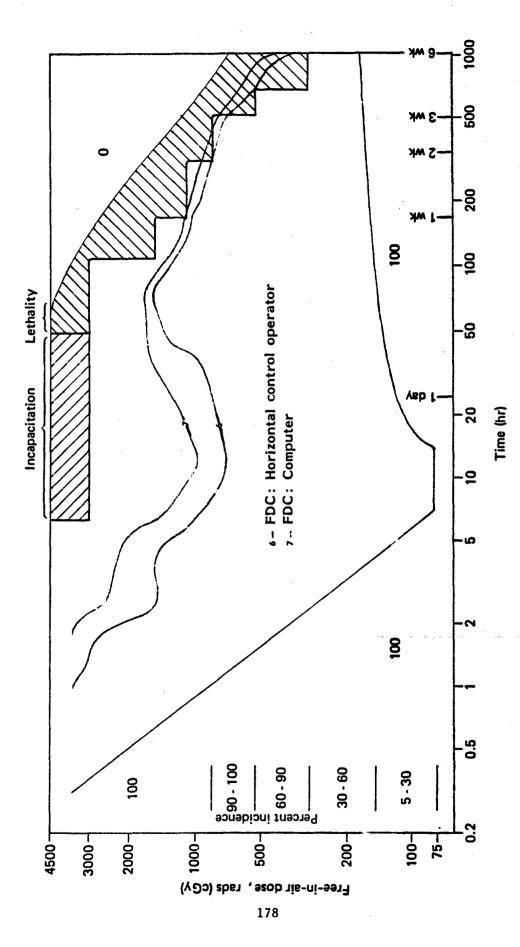
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Figure 81. Crew loaders, 50 percent performance.



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Figure 82. Crew drivers, 50 percent performance.



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Figure 83. FDC crew, 50 percent performance.

contrary to expectations when, realizing that compared with others, his tasks are no more demanding. Moreover, like the fire direction officer, his tasks are performed while stationary as compared with the tank commander and TOW squad leader who are mobile—a situation that can aggravate the symptoms associated with acute radiation sickness.

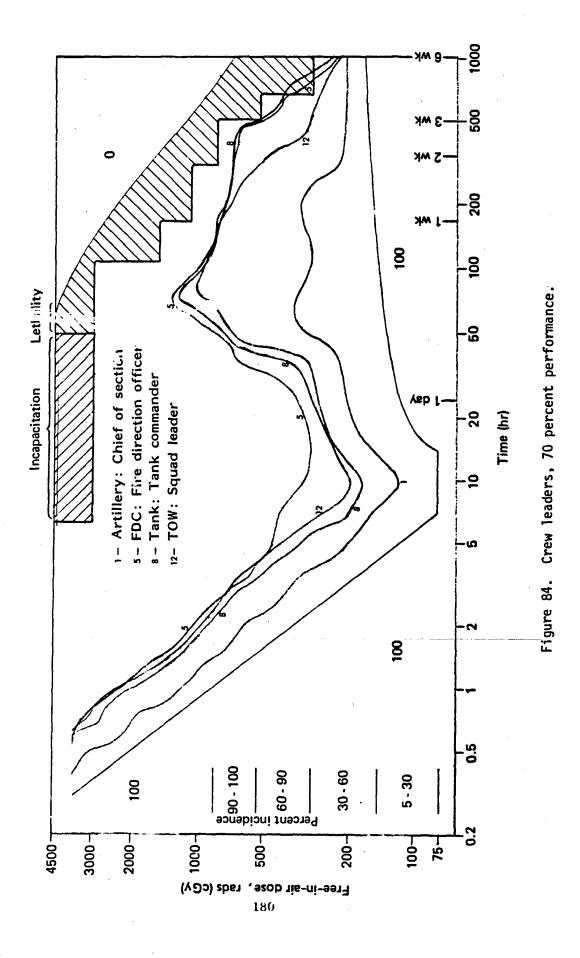
Relatively smaller doses reduce the level of performance of the TOW gunner to 50 percent as compared with the other gunners (Fig. 80); the tank gunner requires the highest dose to be at the 50 percent performance level. As would be expected to a compared of the artillery loader is reduced to 50 percent. I lower doses compared to the tank and TOW loaders, as shown in Fig. 81. Again, as shown in Fig. 83, the FDC group appears to be among the least affected dosewise, with the computer requiring the highest dose to reduce performance to the 50 percent level.

Seventy Percent Performance

The 70 percent performance contours are given in Figs. 84 inrough 88. Again, the relative contour positions are similar to the 50 percent performance levels although at lower doses. As shown in Fig. 84, the significant relative deviation to lower doses of the chief of section from the others in the leader group is again somewhat puzzling; this becomes particularly more apparent for times between a couple of days to a couple of weeks. At the 70 percent level, the tank gunner shown in Fig. 85 appears not to be affected until relatively higher doses compared with the other gunners. At the 70 percent performance level, again, the artillery loader is affected at relatively lower doses as shown in Fig. 86. Noteworthy are the low dose levels that reduce performance to 70 percent commencing within a few hours following exposure. Figures 87 and 88 show a relative widening of the performance contour compared to the 50 percent performance level for the driver and FDC groups, respectively.

Contour Plot Summaries--30, 50, and 70 Percent Performance

Graphical summaries for 30, 50, and 70 percent performance contour levels for all five groups are shown in Figs. 89 through 91. In those



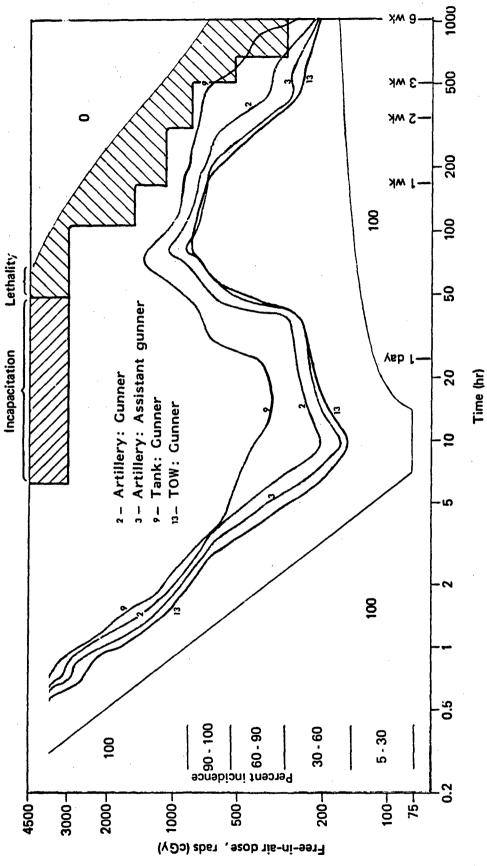


Figure 85. Crew gunners, 70 percent performance.

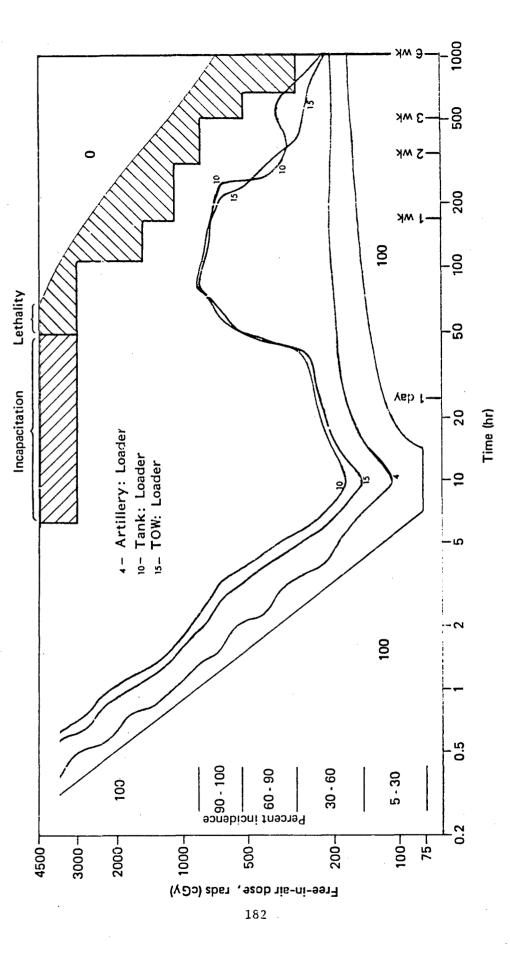


Figure 86. Crew loaders, 70 percent performance.

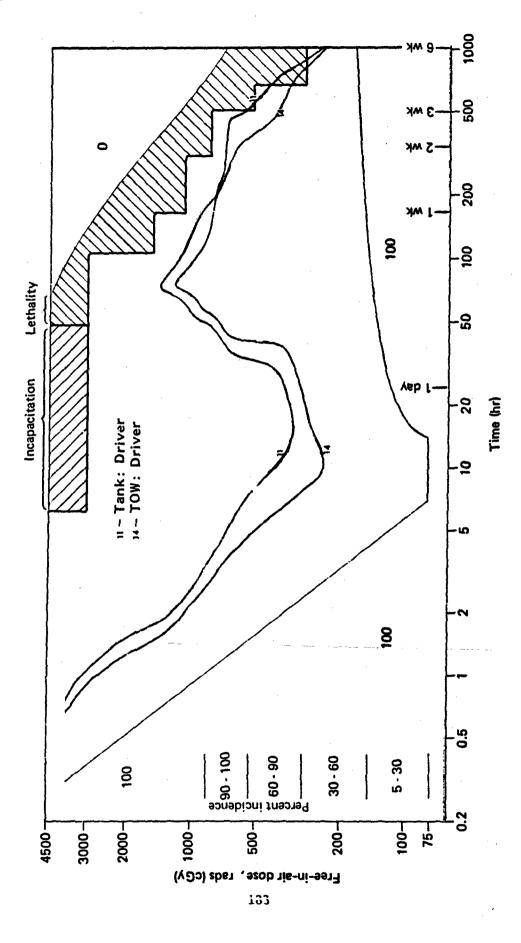


Figure 87. Crew drivers, 70 percent performance.

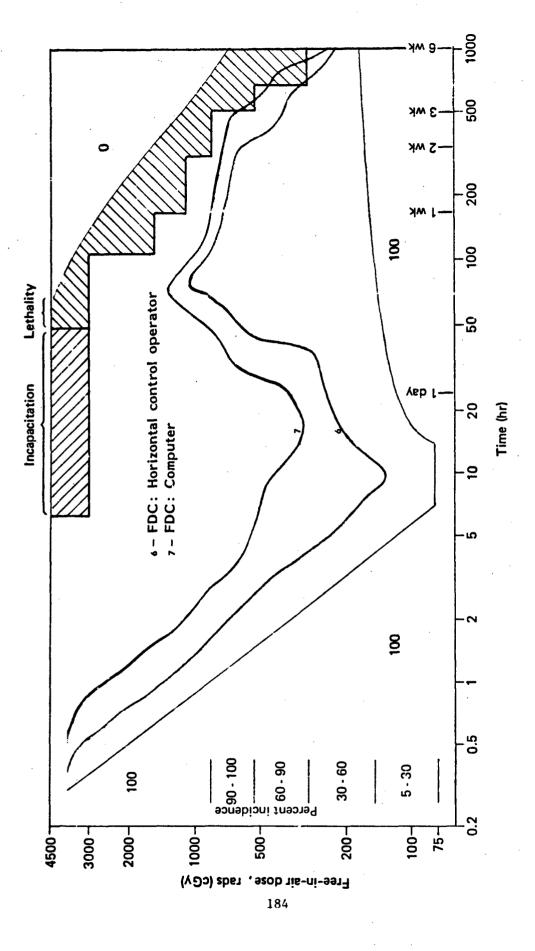


Figure 88. FDC crew, 70 percent performance.

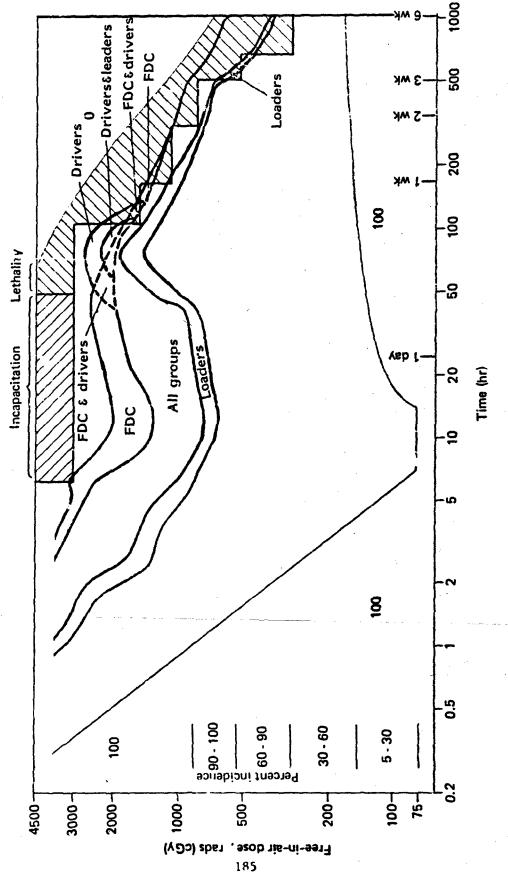


Figure 89. Summary of 30 percent performance.

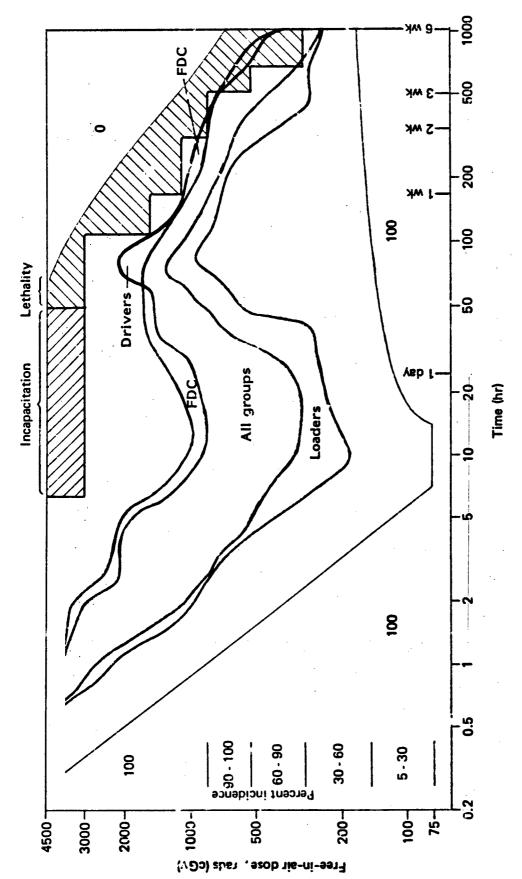


Figure 90. Summary of 50 percent performance.

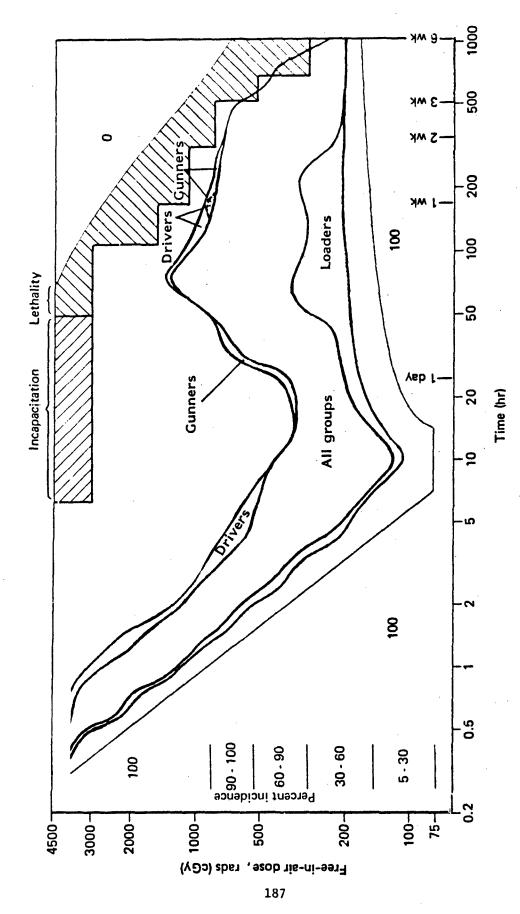


Figure 91. Summary of 70 percent performance.

figures, we show isoperformance bands represented by any groups formed by the two outer level contours. For example in Fig. 90 the lowermost band labeled "Loaders," includes only loaders; the uppermost band labeled "FDC" includes only FDC crew positions. In one region, the uppermost band labeled "Drivers" includes only drivers. The middle band labeled "All Groups" is composed of all other groups, although some loaders, FDC crewmembers, or drivers could also be included because the outermost isoperformance contours represent their respective group extremes. In the interest of clarity, we have not presented a more extensive collection of performance profiles.

The contour summaries all show the meandering band pattern, reflecting the period of remission between initial prodromal symptoms and manifest illness [Baum et al., 1983], which becomes less apparent with decreasing performance level, i.e., with increasing dose. At the 30 and 50 percent performance levels, the middle band, which includes all groups, is bordered primarily by the loaders on the low dose and the FDC group on the high dose end, except for the few "outcroppings" of other groups between about 50 and 100 hr following exposure. There the drivers compete with the FDC group for the high dose values. At the 70 percent level, the loaders border the low dose side of the middle band that includes all groups, whereas the drivers and gunners alternatively form the border at the high dose end rather than the FDC group. Any particular reason for outcropping is not apparent.

Some generalizations regarding performance can be made from Figs. 89 through 91. A dose of at least 500 rads (cGy) is required to reduce performance levels of all groups to 30 percent 2 weeks following exposure. Doses of from only about 150 to 350 rads (cGy) reduce the performance of the loader group to 50 percent between a few hours to a couple of days following exposure; the performance of other groups are reduced to 50 percent during the same period after high exposures—from about 350 rads (cGy) to about 1100 rads (cGy). Doses from about 130 rads (cGy) reduce performance of all groups to 70 percent from a few hours to a couple of days following exposure. Doses as low as 100 rads (cGy) reduce performance for the artillery gun crew loader and chief of section to 70 percent between several to about 15 hr following exposure.

CONFIDENCE BOUNDS--CONDITIONAL MEAN PERFORMANCE

The approximate 95 percent confidence bound (L_{95}) of the performance predictions given by the regression relationships are indicated in Fig. 92. The values presented are based on the variance of the conditional mean $(\hat{\sigma}_{m}^{2})$ as predicted by the regression relationships given in Sec. 3. The L_{95} values represent the average percent deviation from the predicted (mean) value for the 95 percent confidence bound (Student's t-distribution) given as follows:

$$L_{95} = \frac{\frac{1}{2} (UL_{95,m} + LL_{95,m})}{\hat{P}_{k}} \times 100$$
,

where $\text{UL}_{95,m}$ and $\text{LL}_{95,m}$ are upper and lower 95 percent confidence bounds, respectively, and \hat{P}_k is the performance prediction (given in Sec. 3). The L_{95} map given in Fig. 92 is a composite representation applicable to the 15 different crewmember positions and, hence, is approximate. The L_{95} ranges are given for the regions bounded within the curved lines.

The scale of Fig. 74 matches those of Figs. 59 through 73; accordingly, approximate L₉₅ values can be related to the performance contours. Although the regression prediction L₉₅ values do vary somewhat among the different crewmembers (see Table 28), the variations are not large enough to merit individual attention. Some exceptions, however, can be specifically pointed out. For symptom complex 113111, the performance data estimates exceeded the upper 95 percent conditional mean confidence bounds of the regression prediction, being higher than the mean value predicted by the regression relationship as follows (see Table 28): gun crew, chief of section—14 percent; gun crew, loader—21 percent; FDC crew, fire direction officer—14 percent; FDC crew, horizontal control operator—29 percent; and TOW crew, loader—14 percent.

The rectangular enclosures bordered by the dotted lines in Fig. 92 correspond to the regions where symptom complex 113111 is stipulated (see Fig. 44). The FDC crew horizontal control operator and gun crew loader crewmembers represent the most extreme cases and may merit special consideration when making performance estimates, depending on

Figure 92. Individual performance prediction confidence bounds.

Time (hr)

whether or not conservative estimates are desired. It should be noted here that the performance data for symptom complex 113111, although exceeding the conditional mean bounds, do not lie outside the 95 percent confidence bounds for a further data observation based on the variance $\hat{\sigma}_0^2$, discussed in Sec. 3.

The L_{95} contours represented in Fig. 92 are only applicable to the performance values at a particular dose and time. We have not attempted to relate them to lateral variations in dose and/or time although, in principle, estimates of that type can be made. The $L_{\alpha \beta}$ contour pattern shows the correlation with input data points associated with symptom complexes used in the questionnaires (given by the asterisks). In general, Los values increase in regions devoid of the asterisks, where regression predictions were made for symptom complexes not included in the questionnaires. Large increases are situated in regions of high dose and/or long times, where caution should be exercised. Consider the upperright-hand region where the L_{qs} value is indicated as \geq 75 percent. If a performance value of 10 percent were estimated from one of the contour plots, and an error of 100 percent chosen from Fig. 92, the estimated upper and lower 95 percent limits based on the regression analysis would be 0 to 20 percent. Depending upon the dose, 20 percent may be unreasonably excessive or 0 percent may be too severe; that is a judgment that must be made by each individual user of the information presented here.

SUMMARY AND CONCLUSIONS

In this report, the performance levels of individual combat crewmembers have been estimated following prompt ionizing radiation exposure. The estimates have been developed to serve as the basis for
planning military field operations and training for combat in a nuclear
weapon radiation environment. We have expressed performance as a function of two critical variables, dose (free-in-air) and time.

Performance levels have been expressed both graphically and in tabular form. The overall picture is given by the three-dimensional plots prepared for each of the 15 differer remembers selected to represent typical short-term (from 30 to 30 ec) battlefield engagement

scenarios for small combat crews--3 to 4 members. Isoperformance plots and the numerical data given in Appendix J provide working data for selecting or developing further numerical estimates of performance.

Unfortunately, we cannot in any succinct manner assign numerical degrees of uncertainty to the dose/time performance estimates provided (other than the conditional confidence bounds discussed above). That problem is caused by a lack of quantitative data associated with the source of information we combined to formulate the estimates of performance. The performance results we developed rely on two basic bodies of information. The first comes from the comprehensive symptomatology review of human irradiation experience [Baum et al., 1983], and the second comes from the army questionnaires. Based on those two sources some guidance can be provided for utilizing the performance estimates presented.

From the review of acute radiation sickness and symptomatology, we are confident that the dose/time framework (Sec. 4) of symptom complexes describes the typical acute sequelae for humans even though considerable variation in response has been observed in symptom severity and time of expression.

The symptom complexes used to construct the dose/time framework represent well over 50 percent of those exposed to doses of from 300 rads (cGy) and above, from 30 to 60 percent of those exposed to doses of 150 to 300 rads (cGy), and from 5 to 10 percent of those exposed to doses of from 75 to 150 rads (cGy) [Baum et al., 1983]. Therefore, since the performance response data obtained from the army questionnaires were based on the symptom descriptions appearing in the dose/time framework, our performance estimates as a function of dose and time correspond to those percentages.

The performance data correlated with dose and time were derived from army personnel who were asked to judge how they might be able to perform if they had acute radiation symptoms described to them. Accordingly, we have no clear direct way to quantify in a comprehensive manner just how reliable their judgments might be, although the respondents selected for the questionnaires were combat crewmembers trained in

performing the tasks and operating the equipment we focused upon. We can point out, however, that after making some improvements in the response data, our analysis indicates reasonable consistency in the performance trends with symptom severity (and dose level) and the type of crewman (i.e., type of tasks performed). In view of the fact that we cannot prescribe a sound quantitative measure of uncertainty, other than the conditional variation in the response data, we encourage a measure of understanding with regard to purpose in its application.

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Appendix A

RESPONSES TO QUESTIONNAIRES

This appendix contains all of the responses from each questionnaire administered to acceptable respondents (116 total). The data are entered in the form of time in seconds. Table 1 in Sec. 2 itemizes the disposition of all the questionnaires (161 total). The responses to the 24 questionnaires were not recorded from the excluded respondents because they did not lie within the population we wished co-poll. Appendix D contains the responses to the 21 questionnaires from respondents who were rejected because their answers were unresponsive.

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HUY FONG		
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T HAVE TO SUPLOYTSE HT PEUPLE TO THE BOAMING, MICH IS 7 PEUPLE, TO CLEAMING UP TOFIE ROOM AND GFITING MEANT FOR THE JOB. I HAVE A MILOAZ DOATITE'S TOCH. TOAL TO MAKE SUPLINE PPUPLE PREVENTIVE MAINIFMANCE + CHECKS AND SERVICES ARE DONE. I HAVE TO BE ACCOUNIADE FOR MY TOOLS AGO SERVICABILITY

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T ALL A CHIFF OF SECTION OF 155 SP., HIBOAX AND THAT IS WHAL I HAVE BONT AND SUGER! TRAINA SODIFH, A C 3/18FA

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155 S.P. GUN CHEL

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CUMBER, SECTION CHILE . 2 HOPTHS

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		155 S.P. GUN CHEN	

MILH HUW LUMB

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FIRE DINECTION CFNTER CREM

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FIRE DIMECTION CENTER CHEM

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GRADE MUS IN ARHY IN ARITLLERY :

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MAVE BEEN A SUPEPJISFK FOR A FOL SECTION FOR THE PAST YEAR

MUSE MED FUND DROVERLY FURNICLEPH PRIOR IN TAKING UVER FUE SECTION

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UF ... OUPAPHIL DATA

FAC HED FAC COMPUTER

D=NU INCREASE ABOVE HSHAL TIME -1=CANNOT UN IT AT ALL 9990=NU KEPLY 9=NU MEPLY (FOR CUNFIDENCE)

FIRE DIRECTION CENTER CREW

CALC SAY COMPUTER MFAD RANGE HCO. CREW IASKS PL01 SAY UPUEH CALC SAY RFVIEW NSIN UPEN LIFI BOXFS HUSTIPHLATED MALK URDINARY TASKS #SHPERVISED : LIFT CLING RUYLS STAIRS LIWINAMAIII NWAIAUS LICENCRR TITRORIS CO CRFW SYMP COM C! 14B GRADF :E-5 MOS :13E IM ARNY :10YH IM ARTTL!ERY : 1YM COMBAT :N ARTIL. COHRAT:N IISHAL TIME, SFC CUMBAT

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MUM LUNG

ENEM PO VK

FAC HOU :

GRADF :F-A MUS :13F-0 IN ARNY : 27d IN APITLLPY : 24d

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CHEM TASKS

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HUW LUME

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DESINGPAPHIC DATA

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DR STUP

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これでは1月日日でも今日の日の大学の日本のできませんできました。

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MLO TANK CREW

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MGO TANK CREW

#SHPFRVISED : 50

CUMBAT TY 49 70 ANTIL. COMMAT:Y 49 70

UFINDSPAPHTC DATA

GRADE :F-7 MUS :19F4A IN ARHY :14YK AHO IN ARITLLEPY :14YK A

GRADE MUS

CREW TASKS

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TA'IN SFLTION L'ANER TA A CAV IRONP. SUPERVISF TANK SECTION AND 20 PEOPILE, LEAD TANK SECTION IN MANNVEHS AND GUNNERY EXENCISES.

0=NU INCREASE ABOVE USUAL TIME -1=CANNOI DO IT AT ALL 9990=NU RCPLY 9=NO REPLY (FUR CONFIDENCE)

CPEW TASKS

MGO TANK CREW TAUK CUMMANDER 2 78
GINNNER : 71
LOADER : 71 #SUPFRVISED :>50 14 H GRADF :F-K MUS :19F50 IIA ARHY : AYK IHARTILLEPY : AYK COMBAT COURATIN

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MEN TANK CREW

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#SHPFRVISLD :>50 TAUK CUMAAARE GUJUER LAADER GRADE :F-4 HUS :19F3 TA APNY : 9YK AMN TA APTELERY : 9YK A

COMBAT : THE ARTIFFE COMBATIN

CREW TASKS

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0=NU INCREASE ABOVE (ISHA), TIME -1=CANNOL DO II AT ALL 9990=NU KEPLY 9=NO KFPLY (FUR CONFIDENCE)

MEG TANK CREW

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UFINGRAPHIC DATA

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IMPROVED TOW VEHICLE CREW

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UF HOURAPHIC DATA

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COMBAT SHATEN

GUNNER TARGET THACKING ACCURACT TO UPERATE, UR LUADER START HELMAD WEADT UPLIVE RACK STOP 9 SET ACCUIR DESIG CO SULLAN LEADER SFLF-STIPHLATFU VALHES 1 1F 3 BOXES URUTHARY LIFT CLIMB RUYES STATES PREM SYMP COM CLIMB HSHAL TIME, SFC

William Pitte DAIA

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#SHPFRVISEN :>50 CUTUAL COMBATIN

THPROVED ICA VENTUEL CREM

CHEM TASKS

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DEFINITION APPLIE DATA

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IN ARNY IN ARITLIERY

GKAUF MUS

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CHEM TASKS

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PSHIPFAVISED SYSU

THPHOVED ION VEHICLE CREW

CHEM TASKS

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UFFIREPAPHIC DATA

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IMPROVED IN VENICLE CREW

CHEM IASKS

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CO-1841 ANTIL LOHOATER

UFHINGPAPHIC DATA

INPHOVEU TOW VEHICLE CREM

CAE A TASKS

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OCHU INCREASE ABUVE USHAL ISHL -15CANOL JO 11 × T ALL 9990=NU MEPLY 9=NU MEPLY (FUR CUNFIDENCE)

IMPROVED TON VEHICLE CREW

#SHPERVISED 1550

COMBAÍ :V 71 AKTÍL, COMBAT:N

SOLAD LEADER LOADER URIVER

:1144x :124k

GRADE MUS TW ARHY TN ARTILI LPY

UFLIGHTAPHIC HASA

GUNNER TARGET THACKING ACCURACT LUADER -SWILAN LEADER UPER I.1F1 BOXFS BALK URDIMARY TASKS Ş SYNP LON LI 146 COMP STAIRS USUAL TIME, SFC CKFW

#OHPFKVISED :>50

COWBAI : COMMITTE

DENOGRAPHTE DATA

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PLANCE WHILE DAILY

INPROVED ION VEHICLE CREW

GUNNER TERGET THACKING ALCURACY 00220 0053 3 750 ~27277 LUADER CHEM IASKS 0 STARI URIVE STOP 20 SET ACUITE **LUNNER** ~ SUITAN LEADER DESTE CO . CO UPEN. SFLF-SITPHLATFU VALUES 1 1F1 BOXFS MALK UPDIGARY TASKS #SHPFRVISLD :>5w JADAD LFADER LIMBER BRIVER LIFT CLIMB ş HHEP CUMBAT 3Y FB A AMTH, COMBATSM CKFW SYMP CON LLIMB : 111139 : 107k : 77k 7 HSHAL TIME, SFC GRADF
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DELINGRAPHTC DATA

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#SHPFRVISER :>50

COMBAT TY 68 708 AKTIL, COUNTY 40 708

INPARVED THA VEHICLE CREW

IF ALD NOISLAND BIND BOALDION OF BI TARGE! TAACKING ACCURACY GUINNER LUADER CHFN TASKS SEL ACULLA DESTO CO SUUAN LLAVER CPLN LPCK SFLF-SITPILLIFU VALILS LIFI LIFT CLIND RUYES STAIRS CREA STAP LOW CLIMB HOUAL TIME, SFL

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U=NU INLKEASE ADUVE HOHM! IIML 4940=NU MEPLT FUR CUNFIDENCE)

DESIGNBAPHIC DATA

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Appendix B

DEMOGRAPHIC DATA-

This appendix contains the complete returns from the demographic data sheets at the front of each questionnaire, and is divided into two parts. The first lists the fill-in-the-blank answers to explicit questions. The second contains the essay responses to the question:
"Briefly describe your military duties during the past year," plus any remarks written anywhere in the questionnaire.

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 ALSO INTHALLY THEN INTERPRETED HAVE DOING HAVE

 IN A CHIFF OF SECTION A SPECIAL WEAPONS TEAM THAIL IS WHAT I HAVE

 CHIEF OF SECTION A SPECIAL WEAPONS TEAM CHIEF, SUPFRVISING A 10 MAN GON CHEW 4 A 4 MAN SPECIAL WPNS. TEAM.

 T'VE BYEN A 13R ALL OF MY ARMY CAREEP. I'H ALSO IN SPECALL WEAPONS AND HAVE REFW FOK THE PAST 3 YEARS.

 TOURING THE PAST YEAR I NAVE REFW. THE CHIFF OF A MIGSASS.P. AND HAVE HAD ANYWERE FROM 3 TO B MEN WORKING FOR ME.
- SUPERVISING THE PEOPLE IN MY SECTION, KEPTING A SAFE GUN HAS BEEN SECTION CHIFF STWE 1082
 - STAFE 1082
- I HAVE BEING A MUCLEAR ASSEMILER AND MEANEN ON THE SPECIAL MEAPONS SECTION (A. HOMT.) ALSO I BEEN BIRY NAC MOD, AND ALTERNATE
- PETACHMENT SGT. OPFRATIONS HED, GUMPERY SGT. CHIEF OF SECTION, RE-EMISSIMENT HED.
 MY DUITES WEPE HAC NEW IN GERMANY AND SECURITY STIF MED ALONG WIGEPMAN SOLDIENS GUSTODIAL GUARDS FOR 155 NUKE RD. TRANSFER HI
 TO FT. STLL RECAME CHIEF FIRING REPY FOR Z/121H. A VIETNAM
 SUPERVISE THE MATHIENGMEE AND ACCUMINIANTILITY OF SEC. EQUIP AND IRAINING OF PERSUNNEL BOTH INDIVIDUAL AND CALECTIVE TRAINING.
 SUPPONT AND FACCHRAGE CAREER DEVELOPMENT OF SHRUPDINATE SOLUTERS. 97
 - - DUPING THE PAST YEAR I HAVE REFH AMMO SECTION CHIEF AND HOWITZER SECTION CHIFF I MAS AN ASSCHALFK ON THE 155 SYSTEM IN MURTHERN GREFCE.T WAS AT THE IATH HSAFAD.I PCS'ED TO FT. SILL WHERE I AM OM A SECTION OPF AUD OU 121 315
 - 123
- REFN ASS. GUMNER AMD BI MAN THEN WENT TO CHLEF DF SECTION OF AMMN. I Havey't Really had any, pust of the 1,mes this past year I have blen moved around a Lot. My Military Duties dihthe the rast year was An Ammo agent responsible what to pick up and diverly ammo to all
- SECTION CHILE 1558M SP, GUNIFRY SGT , ABMU PZI, FI, SILL & AT THE AGE OF 18 &* VIFINAM I WAS A GUNIFR I'I A A THCH UPIT IN GERMA?! AND THEN IN FEBUARY 1982 I PCS TO FI, SILL AND I WAS A GUNNER UNIIL 2 JUNE 1982 THEN RECAME SECTION CHIFF ON A 1551M HOWITZFR 12k 127
 - RUNINFR, SECTION CHIEF . 2 NOHTHS
- 'S ASSIGNED AS 15G OF A 155 NM HUW RATIFRY C-AIRY 2/37 FT. SILL OK. 17503 F OF FIRTIG ATRY, SUPERVISE AND TRAIN CHIEF OF SFCTION TO RE LFADER, TO DEVELUPED THE YUUNG SULDIER OF TOMMURROM, HOM TO
- HAVE BFEN A RPFRAION OF AU 155 SP HUMITZFR AS MELL AS A GUNNFR AND CHIFF OF SECTION I ALSO SERVED IN MEST REPLIN GERHANY FOR YEAR ARU I WAS STATINGFO IN TUPKFY. ALL OF MY NUTIFS THERE MERE SPECIAL WEAPONS RELATED. I WAS ASSIGNED HERE DUCASIONALLT
- SECTION CHIEF, INC NOIC FOR 3/18 FA A BINY, I HAVE BEER WITH 3/18 FOR 2 1/2 185 AND HAVE WURKED WITH NBC, AND OTHER MAJOR
- THAS IN AN ARMU SECTION DEVING A S-TON TOUCK AND LAKRYING OUT NORMAL DINTES, SINCE I MADE E-5 4 MONTHS AGO I AM AN AMMO AGENT.
 MAKING SHKF THE FIRING DATTENIES GEI AMMO, FT, STLI IS THE OMLY PLACE I'VE BFLN SINCF IN THE ARMY AND HAVE NEVER BELN ON A GUM,
 FOR, AND SPECIAL MEADUNS, ATTENDED BNCOC/CA
 RN. AIMU SGI, HERE AT FT, SILL
 KUPEA AD-81,"ARCH/ ARMY TAMIS AU, I MAS PROHOTE IN FPL. FPUM PFC ON JINE AT, PNCOC AUG AL, BNCOC OCT, ALGUNER FT, RILEY KA.
- BI, CHIEF OF SECTION SEPT. AZ, OCT. AZ SOT. TASIRUCION
 - * NOT 155 RUT "FILED B-17CH SECTION FILEF ON 155 SP, ANGOC-LA SHUDENT, S W LHIFF, SECTION CHIEF ON 155

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DUTY DESCRIPTION

RECLASSIFIED INTO ARTILLERY; MY DUTIFS AS FUC MOUTO OF A BRIGADE TACFIRE, SUPPORT OF 3N ARTER'S
FINISHED ATT IN JULY REEN WITH MY PRESENT HATT APPROX, 4 NOWTHS WORKED AS BIO IN-UKILL NOW.
POLICE CALL, FORMATION, PULLING GUARD-SATU NATO GUARD MOTOR POOL GHARD, VEHICLE MAINT, DATH, AND CEREMUNY, SOT IEST, P.T.
TEST- MUS WORK, A LAST 7 NOWINS
WORKED IN BATTALION FUL AS A BATTERY COMPUTER, PRESENTLY JUST COMPULETED A STANCE OF ACTING SECTION CHIEF AND PRESENTLY A 3-, TERY 204

COMPUTER IN A RATTERY FOR. DIPECTION: UF TIRE FOR BATTALION, MAINTANANCF: SECTION, FUITPHENT-VEHICLFS : PHYSICAL FNVJRUNNENT; CUITIG GRASS,SWEEPING ASPHALT 205

STAYTING OUT OF LEGAL/FTJANCIAL TRUIBLES TOVE NORKED ON CHAPIS, DAIVE THE 577 VEHICLE THAT WE TAKE OUT ON FIELD MISSIONS , AND T PAVE BEEN THE RIO OR MOUTO IPANSMITTER

TACFTHE CUMPHIER SPECIALIST, ASST SECTION CHIEF, OVERSEES MAINT ON ALL VEHICLES PELATED TO TACFIRE UNIT, AND TRAINING ON ALL SECTION PERSONNEL 207

FDC RELATED DUTÍFS AS HGO VGO GOMPHIFR, MBC ASSISTANT. MY DITTES AS A FDC MEN HAVE PANGED ANYWHERE FKON 577A1 (TRACK) MAINTANCE TO CHMPHIFR; RTO; FDC HGD, FDC VCG, 30 CHENTSAL SHRVEY

TEAM. * DEF AND DIA.
IN THE PAST YEAR I HAVE SUPERVISED THE OPERATION OF THE BIRY FOC AND BOC, WHILE ALSO OPERATING AS THE CHIEF COMPUTER.
I) BE AT APPOINTED PLACE OF DUTY ON THE 21 TO WORK IN THE 13E10 MOS. 3) PULL C.O. 4) WORK ON PETATLS 5) * 3 DAYS
I'M PRIOR SERVICE AND FAME IN A DIFFERENT MOS, LAST WAS 15DIO. I'VF BEFN WORKING MY PHESENT MOS A LITTLE OVER A YEAR AND

TO OF COMPHER 213 214 215

216

217 317

510

I HAVE BEEM A SUPERVISER FOR A FOC SECTION FOR THE PAST YEAR 220

WURKTWO TN 5-5 FRATMING SECTION AS PAPER-PUSHER, FTELD DAILY AS TACFIRE VEMED UPERATOR, ALSO MS77 COMMAND POST DRIVER, I HAVE UFEN SECTION CHTEF TH FOC FOR 4 HONTING AND TEFURE HAT I WAS THE CHIEF COMPUTER WORKING MSTONERA AND THE USAS USING BOTH THE 198 AND 109A7 HOWITZEMS. I HAVE LATELY BEEN WORKING AS COMPUTER FOR DURING FIX'S AND ALSO MAS COMPUTER DINITING YMARS SMOKE TEST FOR THE U.S. AMMY FTELD ARTILLERY BOARD. I AM WORKING AS I WURKED IN AN FOLL STOLLERY BOARD. 223 223 224

TYPICI IN THE S-2 SECTION. 225

221 MUS NEO FUN ORDERLY RUDH CLERK PRIJK ID TAKING OVER FDE SECTION 227 FDE CHIEF/SIP MENZA & P MEN ALD GEE NEO, HY TIME IS SPENT IN ONE OF THESE AKFA'S ALMOST ALL OF THE TIME! 226 MOV AL-FFB W2 MHR 15G FEM A2-NOV W2 OPH SGT

729

OPERATUS SPECTALIST AT FUPT STEL, IN GEPHANY I MAS A CHART OPERATOR, COMPUTER, AND TRACK DRIVER I MAS SECTION CHIEF. I FOLLOMED OR LOUKED OVER AND TAUGHT MY HEN THE CORRECT HAYS TO COMPUTE DATA AND I FIGURED DATA FOR 230

TYPE OF PUBLIS KITH A 109AP FIRING BATTERY. CLEKK (ABM AMD FAZINTYG AIN USP ASST) TRAINING SCHEDHLFS AND AMAR FORECASITAG AND RECURDS FOR THE GDE. (ACTIVLY FNVOLVED IN TAPPEAR METT PATATING) ...

PESPONSIALE FUT THE SUPERVISION, IPAINING AND THE FUNCTION OF THE FUC CHART OPFRAION TRUOP UVER SEFER WHEN CHIFF IS NOT AROUND FACEIRE PELL FOR THE LAST 7 MUNIUS I HAVE REFU LEARHING AND STUDYING FACEIRE CLERK- SO-FUR

HAVE BEEN TRAINING IN DESERT WAREARE AND TACFIRE, AND HAVE BEEN SUPPORTING THE UPFICER'S ADVANCED TRAINING COURSE, WELL HERF AT FORT SILL, I HAVE HAD VERY LITTLE TRAINING TN MY MUS 13FID, LUCKLY I WENT IN GERNANY AFTER BASIC, BUI DOING PRIMARY CHART OFFRAINR ANYTIME WFORE IN THE FIFLD HERE AND METS.

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CREW 3; DUTY DESCRIPTION

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TAME SECTION LEADER THE A CAV TROOP. SUPERVISE TANK SECTION AND 20 PEDPLE, LEAD TANK SECTION IN MANUVERS AND GUNNERY EXEKCISES. PLATOOM SERVEAUT OF A 30 MAIL TAIN WITH 7 TAINS SUPPURITING THE INJURE OF HE ID.S. ARMY ARMUR SCHOOL FT. KNOX, KY.
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   BRILFED ALL MATU FORCES ON UPFOR VEH. AND PERFORMED MAINTANCF ON 182,1-62-4, 154, 1548, P176, MIRISZ, BIR60PR, BAZ-69 AND BMP.
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  PLISOUN SGT. OF A TANK PLATOON IN FURDPE.
PLI SGT/PLI LUR. HESPONSIBLE FOH THE FRAINTNG OF 19 S.M., AND TOFWIFING TRAINTNG DEFFICIENCIES, AND TAKING STEPS TO CORRECT
THESF DEFFICIENCIES, A DEC 66 - JUL A?
I HAVE BFEN THAIPING ATT/OSUT THOUPS AND I AM DUM THAINING ARMFW DFFICIER RASIC.
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     PLT SGT, MASIER GUNNER OF H-; TAWK PLI.
Tank Chrmanjer with a prew of 4. Also, being the manking e-6, I was fulfilling the 300 as assistance platuon sfrreant also.
Lugistics chief, iank plt sgt, ginnert and lactics instructor. 25 MM Chaingu. Instructor, cumpan; tank lor, usmc
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             KVED AS PLATONI SET, FUP THE LAST YEAR, CONTROLLING AND SUPENVISING 20-24 MFN BOTH IN BARRISON AND THE FIELD IN
I also teach them un set task,
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           I HAVE BEEN AN ARHOW WALL SGT. I MAVE BFEN TEACHING BASTC SKILLS AND AKWOR SURJECTS.
Platoon commander Tam: Platoon Stationed Ukinama, japan and Republic of Korea and Republic of Philippines. USMC
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                LAINUN SERGFANI IN A CAV PLAINUN, PFNFUPNING NUTPNST AND PATHOL DIITY ALONG THF IRON CHRTAIN, . ALSO 1971
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  SCT AKMURED CAV PLT. SHPFHVISED MAINT OF 5 MITTAL 4 MEDAL TRAINING OF BUTH 19D AND 19E E-6 AND BELOW
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 AND MISSIONS
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 TH CHAPLE OF A TANK PLAINON, KESPUNSTBLE FOR HAINI OF VEHICLES, THAINING AND WELFARE OF PERSONNEL
                                                                                                                  PLATOON SGT OVER IN PERSONEL ALSO COMPANY MASIER GINNER
I AM THE BAITALION MASTER CONIER, I COORDINATE ALL TANK CONNERY AND OBSERVE TURKET MAINTANCE.
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          LT. SGT./TANK SFCTION LOR, USNC
VF REFU A TANK CUMMANDER, PI 1 SG1. WEMI 14UR 3 CUNNFHYS, ARTEP AND NUMERIOUS DIHER DUTIES,
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               WAS IN GERMANY IN 28M 41 APHOR. FNLUNGEU FRG MAS A PLATUON SERGENT FON IN ENTIRE IFAR.
                                                                                                                                                                                              DRILL SGT. -SHPERVISE AND IRATH YOUNG CIVILIANS IN RECUME ARMON CREMMAN, . OFF AND ON
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        PLT SGT, SFLTIDU SGI TAHK FUMHANDER
Instructor at an ucu acadeuv, instruct bastc non commisioned officers cuinse 19Echf
P/T seakcent & rouths, bu master guinner & muinths
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        THSTRUCTOR MAUAS HETT TEAM TEACHING FIRE CONTROL, LASTING ABILITY OF A-3 SYSTEM
                                                                                                                                                                                                                                                                             TANK CYUR, SUPFKVISUR NF 3-20 PENPLE AND INUK NVFK AS PLT SERGFANI
PLT SGT.- MAINTAIN 5 M60AI TANKS WITH A PLT NF APPRUX 20 LREW MEMBFKS.
INSTRUCTOR (PRILL SERGEANT SCHOOL) TAC NOT (PRIMARY NEW COURSE)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         DURNING THE PAST YFAR TECH INTEL ANILYST SOVIET AKNUR
                                                                                                                                                                                                                                                                                                                                                                                                                                     TANK PLI SGT/ MASIFH GUMMER FOR AN ABHON TANK UNIT
TANK PLI SGT AND MASTER GUNGER FOR NY COMPANY
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DUTY DESCRIPTION **..**

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TOO WORNING AS AN ANTI APANCH PIT, 10YHS, I HAVE WURK WITH THE LEFP TOW, THE M220 SYSTEM AND AT THE PRESENT THE ON THE M901.
TOO WORKING AS AN ANTI-TAKE PLT GGT. TARTHE CARE OF THE WELL FAIR OF MA WEN, ALL TO TO AND ONE APC. ALSO MAKING SHIFF MT PLT. IS
THAINED AND ARFPARE FUR COMBAT. ALSO TRAINING LE'S WHIN WORK AS PLT. LFADERS.

THAINED AND THE TOWN TO TO THE TOWN TO THE WAINTING TEACH APPROX, A STRUFNTS EVERT 3 WERKS ON HOW TO UPERATE, MAINTAIN, SHOUT

ADT DUPING THE PAST YEAR 4 HAVE REHA ASSIGNED AS A URLIL SGT.

407 DUPING EXFERICUE TH ALL TOM VEHTULES FXCEPT THE MILES. I'M A PLI, SGT. WORKING TOM JEEPS AT THE PRESENT TIME.

409 AS AN THSTRUCTOR FOR PALCOCKA IN THE 116 SFRAIFS. ALT ARFA'S TIV'S PLI. SGT. 2YR. FURUPE.

410 PEAVY ANTI-APHON CREWMAN SHPFRVISOP. CHIFF SHPFRVISOR SPFCIALIZING IN NIGHT OPTIC.

411 THAVE DEEN A SEFTON SGT FUP THE LAST IN MUMIH AND OUT OF THAT TIME MY TIV'S HAVE BEEN IN SOPORT ABOUT 5 TO 9 TIME FOR DIFFRENT THIMCS AND MY TIV OUR!T HAVE THAT MANY HOUPS ON THE GON.

T MAS AT 11H IN 1973+74 AND MAS THEN RECLASSIFIED AS AN 11A BY DA. IN 1979 WHEN DA RE-ESTRALISHED THE 11H MUS, I WAS AUTOMATICALLY SAITENED BACK. STICE THEN THAVE HEEN IN A MANGER BM OR ON STATUS AS A UPILL SET, SO I'M NOT YOUR REST SHURE T ATT THE HTSSLF FUCISITES MED FUR THE TUM PHOJECT, HEBSTOVE ARS I WAS AN ITV JUSTHILETUR AND LATER PLATOUN SERGENT IN EUROPF INFURNATION

SUPERVISED APPOUX 30 PERSONIEL. I HAVE ALSO ALEN AN ANTI-ARNOR INSTRUCTOR AL ET BENNING, GA. FRUM 1978-79

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SECTION SOT PESPONSIALE FOR A F-M AND 2 TOW VEHICLE, PRESENT DHIY IS PLT SOT OF THE ITV AND STERM.
I AM CHREENILL AN TIV SECTION LEADER IN A COMORT UNIT, I MAVE TRAINED SOLDTERS IN ALL DIFFERENT MODE OF TOWING, I HAVE BEEN A TOM SELITON SOT FUR THE 4TH DIV, ANTI ARMON SCHOOL.
I HAVE UFEN A PLATOUM SERGANT MEDIN-JFEPS WITH THE TOUST FUR THE PAST & MIS APLATOON SFROENT MOOT WITH 3RD ARMON DIVISION THAT I HAD IN PETUFUREE WITH HY THAINLES.

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I'VE ANTWELD WITH JEEP MUNICATED THA AND WIRE TOW TON CAP VEHICLE, MY PRESENT JON TS PHONG INSTRUCTOR
JAN AL WHILL AND SECTION SET IN GERMAN.
IN 1977, IN GENERAL SECTION SET IN GERMAN.
I STAKE MURATURE THE TOW IN 1977, I DEPARTED FOR BERMANY IN 1979. THERE I WORK WITH WITH THE ITY, I RETURNED TO FI. CAMPRELL 126 427

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AST OKTEL SEPGEAMT NO EXPERTENCE WITTV. A 1 WEEK. ASZ I WORK OM LEF PAMUE AS AM INSTRUCTOF FOR ITV. A 1 WEEK. ASX I HAVE BFEN PLI SGI OF AM AT PLI APPX IMICE IN THE PAST VK, RIGHT NOW I AM PRESENILY A SFCTION SGI OF AN ITV CREW IN MAINTAPL, "LIFAKE, AS "ELL SUPFRVISION OF MY SECTION & US NAVY I HAVE OFEN A PRILL THSIRUCION AT F1 DIX, N.J. WHICH IS VERY LONG HUING AND MENIALLY VERY DIFFICILLI, TOW SECTION LOSS, CEPMANY, BN NCOIC IN CHARGE OF ALL TOW PRAINTNG, INA INSTUCTOR IT POLK MOUNTFU, JI

434 I) ITV SECTION LEADER- KESPUNSTBIE FOR STIPFRVISION OF 7 PEOPIE AND 2 ITVS 2) WEAPONS PLI SGT-RESPONSIBLE FUR SUPERVISION OF F. THACK AND GUAL. PH HORTAP SECTION AND 1 TEV SECTION.
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459 SECTION SGT, FOR A TOW WEAPONS SYSTEM MOUNTED ON AM MISTAZ

440 ACTED BRITELY AS PLI SGT FOR AN AT FLET, SECTION TOR FUR APPROX 9 MONTHS AS TOO AND

ACTED BRITELY AS PLI SGT FOR AN AT FLET, SECTION TOR FUR APPROX 2 1/2 YEARS) WORKED WITH MARD TOW FUR 2 YEARS

ACTED BRITELY DUALIFYING ON THE TIV (WORKED WITH THE LIVE FOR APPROX 2 1/2 YEARS) WORKED WITH MARD TOW THO THE TOW TY, AND MOW I HAVE BFEM A SECT, LUR AMOUNTS.

447 SEMION INSTRUCTOR TOW THOUGHT RAINING FOUNTS, THERMOYED TOW VEHICLE AND DRAGON.

448 INSTRUCTOR ON THE TRAINING FOUR THE MAR FOR FLAY THE THITAL ENTRY STUDENT DURING BASIC AND ADVANCED THAINING.

446 IN HAVE INSTRUCTED TO THE FORT THE PAST FRA ATE STUDENT WERE THITAL HAVE HENDED SERVICE ON ALL POSITIONS ON THE TIV AND THE ASSETCHE.

Appendix C

SINGLE SYMPTOM EFFECT ON PERFORMANCE

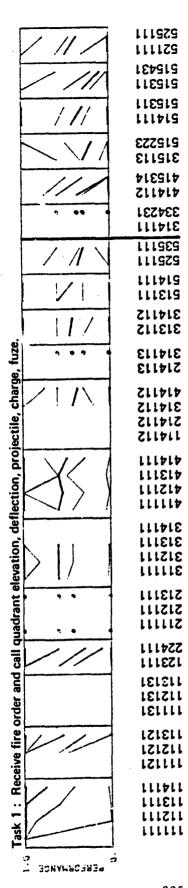
Each figure of this appendix is devoted to one position within a crew. Figure C.2, for example, shows one strip of plots for e ch of the two tasks performed by crew 1 (gun crew) position 2 (gunner). Performance is plotted on the vertical axis ranging from 0 to 1.0. The horizontal axis is composed of symptom complexes that differ from one another in only one symptom (usually). The first plot shows symptom complex 11X 111 where X (fatigability and weakness) ranges from severity level 1 to severity level 4.

The heavy line connects the median values of the soldiers' performance estimates for each of the symptom complexes. The upper and lower lines connect the extreme estimates. The other two lines connect the upper and lower quartile points. In the first plot on this page, the upper extreme, the upper quartile, and the median all lie on 1.0 for all the symptom complexes.

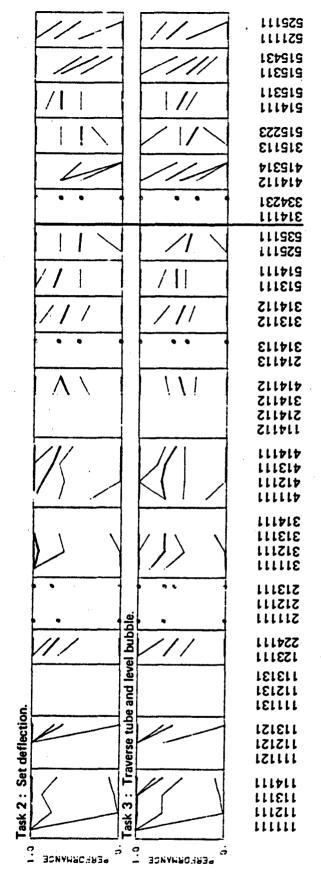
If we have described the increasingly severe aspects of symptom complexes clearly, and the soldier estimates of performance are consistent with that description, the lines connecting the points on the plots should trend downward or should remain level. If one of the lines were to reverse (slope upward), it would indicate that performance improves as sickness becomes more severe.

There are several instances of reversals; not all are cause for concern. A reversal in one of the extremes can result from the estimates of a single respondent. A shallow reversal may be due to the scatter of the estimates about two values that are essentially the same. But if the reversal is steep, involves the median, and is repeated for several crews, it indicates a difficulty in symptom interpretation. There does seem to be a difficulty with the symptom complex pairs 112 111/113 111, 411 111/412 111, 214, 112/314 112/414 112, 314 113/315 113, and 525 111/535 111.

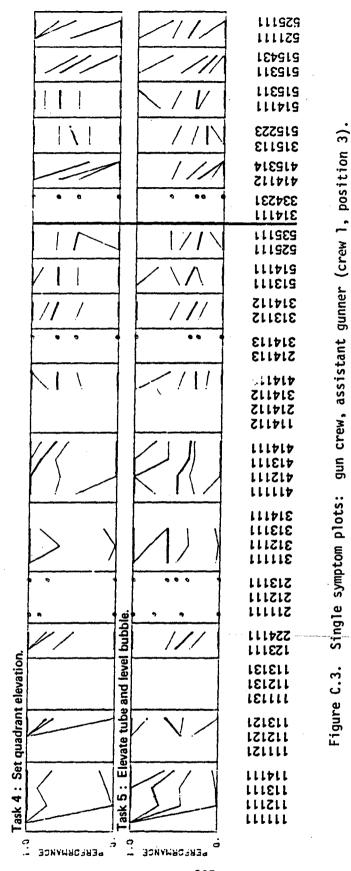
However, there is a more important aspect shown by the single-symptom plots; that is, there is a pronounced difference between tasks for some positions. For example in Fig. C.4, crew l (gun crew) position 4 (loader) tasks 6 and 7 have very different patterns, as do tasks 9 and 10--implying that those tasks will suffer different degradation patterns than other tasks performed by the same crewmember, and therefore should be analyzed separately.



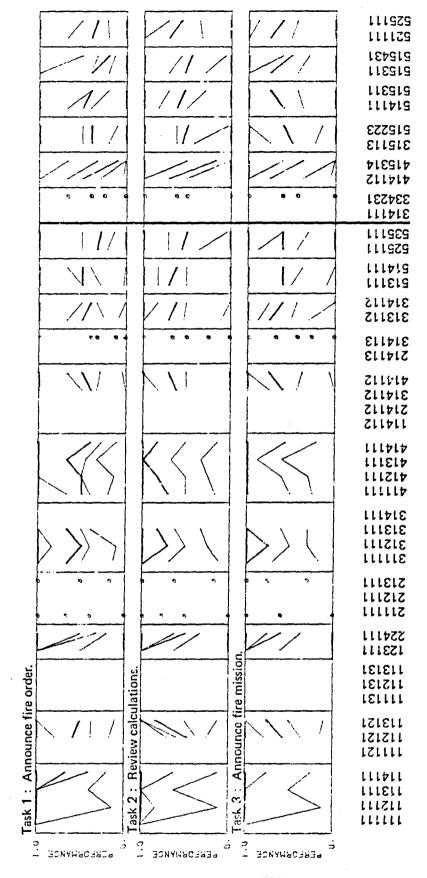
gun crew, chief of section (crew 1, position 1). Single symptom plcts: Figure C.1.



gun crew, gunner (crew 1, position 2) Single symptom plots: Figure C.2.

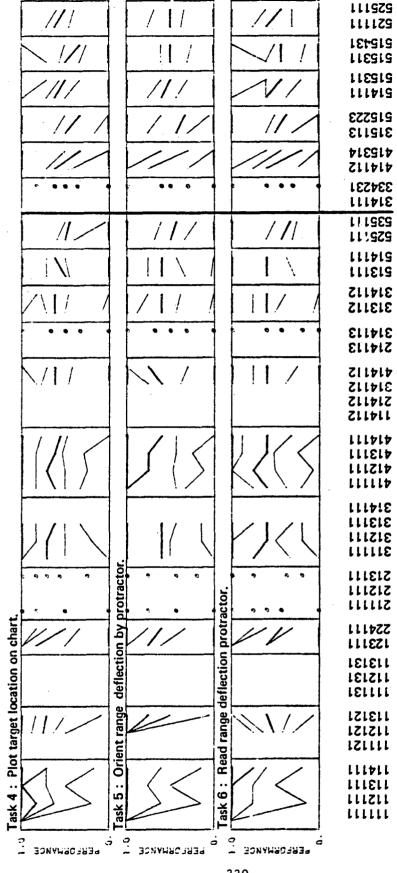


gun crew, loader (crew 1, position 4). Figure C.4. Single symptom plots:



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FDC crew, fire direction officer (crew 2, posttion 1), Single symptom plots: Figure C.5.

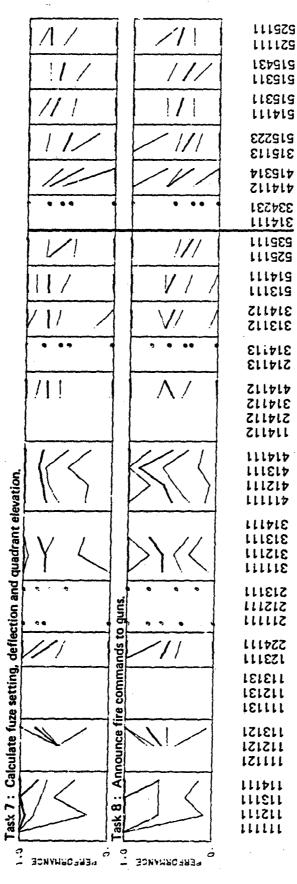


2, position 2).

FDC crew, horizontal control operator (crew

Single symptom plots:

Figure C.6.

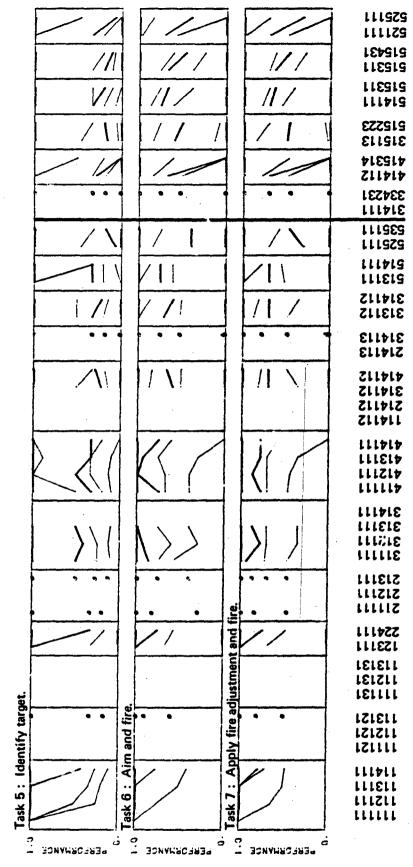


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crew, computer (crew 2, position 3) FDC Single symptom plots: Figure C.7.

tank crew, tank commander (crew 3, position 1). Single symptom plots: Figure C.8.

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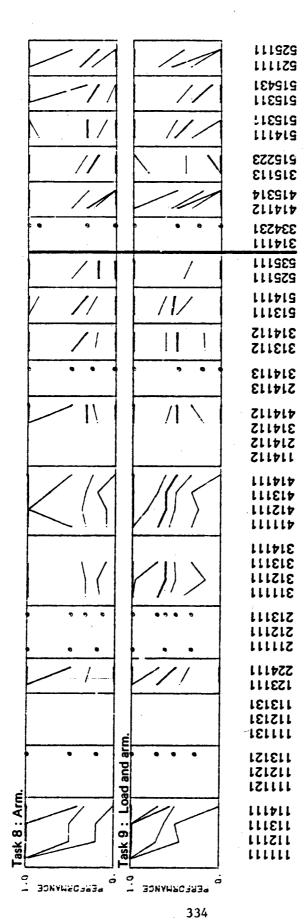
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tank crew, gunner (crew 3, position

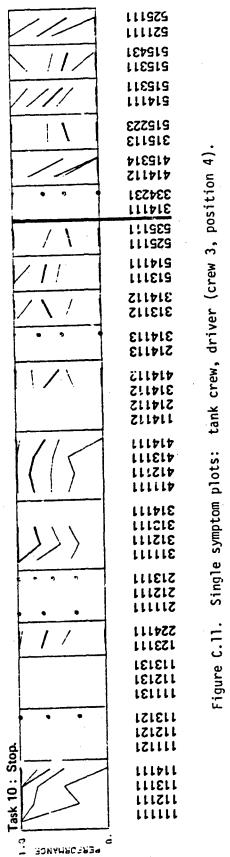
Single symptom plots:

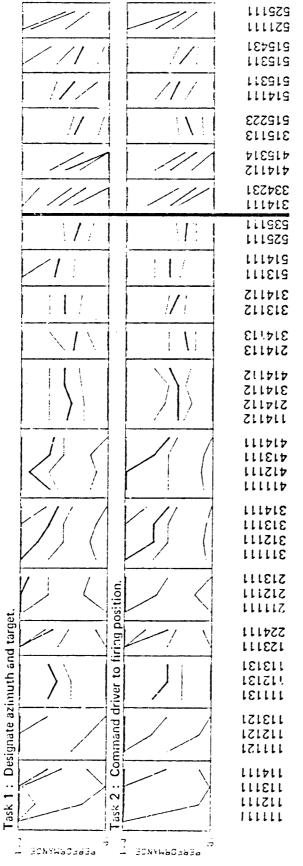
Figure C.9.



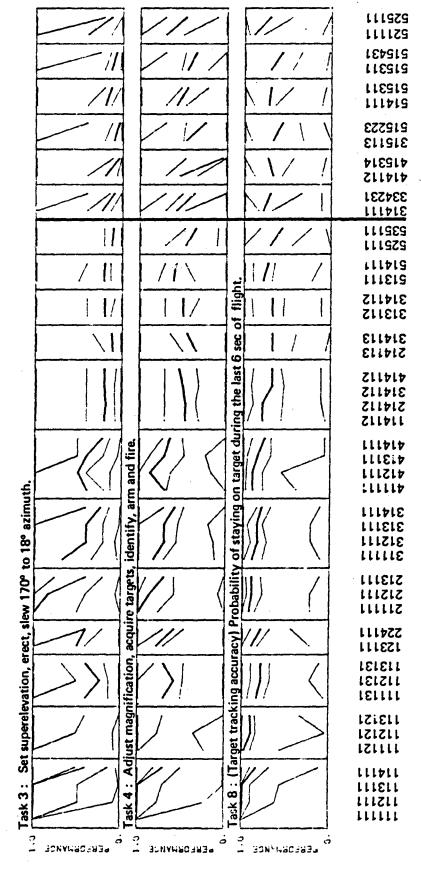
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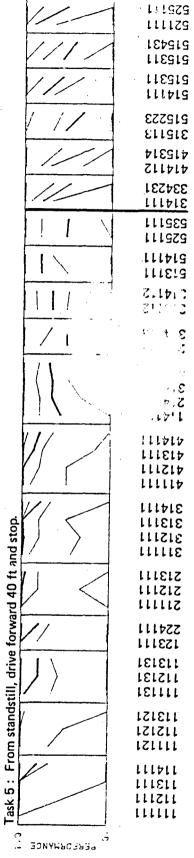




TOW crew, squad leader (craw 4, position 1). Single symptom plots: Figure C.12.



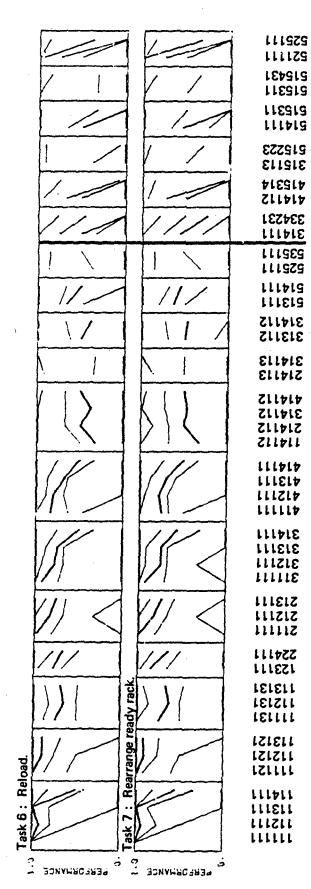
5 sosition 4, (crew crew, TOW plots: Single symptom C.13. Figure (



Single symptom plots: TOW crew, driver (crew 4, position 3).

Figure C.14.

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gure C.15. Single symptom plots: TOW crew, loader (crew 4, position 4).

RETURNS FROM REJECTED RESPONDENTS' QUESTIONNAIRES

The format for the sheets in this appendix is the same as the format used in Appendix \mathbf{A} .

Each sheet of this appendix contains the returns from the questionnaire of one of the 21 respondents who were rejected because their answers were not responsive. The nature of those unresponsive answers was described in Sec. 2, and is summarized in the table below.

Table D.1. Unresponsive answers.

Respondent Number	Percent Noncompliant	Percent Extremes	Percent Excessive Consistency	Percent Combined	Percent Reversals
106		45		1.	40 ^b
108		19,	54	73 ^b	
113	5	19 81 ^b		86 94 ^b 81 ^b	
115		47	47	94 ^D	
121	10,	55	16	81 ^D	
124	10 _b 97 ^b	ř			L
138		26	•	1	40 ^b
218		30	48	78 ^b	L
232					43 ^b
237					47b 43b
238		L			43 ^b
301		99 ^b	L		
303			95 ^b		
304		91 ^b		L	
307		53	31	84 ^b	
309		43	39	82 ^b	L
312				L	38 ^b
316		29	62	91 b	
338		22	67	89 ^b 58 ^c	_
403		38	20	58 ^C	28 <mark>c</mark>
438					49 ^b

^aFifty percent = random.

bGrounds for rejection.

c Rejected for combined causes plus reversals.

CREW TASKS

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T HAVE BFEN A ASFIRER TH SPEATH MEAPON FOR LAST YEAR

O=NO INCREASE ABOVE USUAL TIME 1=CANNOT DO IT AT ALL	9990=NU #FPLY	9=NO KEPLY (FOR CONFIDENCE)				
			155 S.P. GUN CHEM		-	
HUW LUNG		•				
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DUBING THE PAST YEAR I HAVE REFN THE CHIFF OF A MID3A35.P. AND HAV E HAD ANYWERE FROM 4 TO 8 HFW WORKING FOR ME.

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NUPING THE FAST YEAR I HAVE REFU AMAN RECITOR CHIEF AUN NUVILER SFLITOL CHIEF

0=NO INCPEASE ABOVE USUAL TIME -1=CANNOT OO IT AT ALL 9990=NO WFFLY 9=NO WFFLY (FUR CONFIDENCE)

HUM LUMG

WHEN HD YR

UFHINGPAPHIC DAFA

CH, CF SFCTIONS GHANER AS, GUNNER LUADER

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I HAVENIT DEALLY HAD AMY, MUST OF THE TIMES THIS PAST YEAR I HAVE BEEN MOVED APOINN A LUT.

DEHINGRAPHIC DATA		WHEN HOW LONG		
		ON HA HA US		OWNU INCREASE AFOVE USUA
.E-5 CH.N	IF SECTION: 10 AZ			-1*CM4001 DU II AT ALL 9990*NO REFIV
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9. 6 YR 4110 A'S.	AS. GUNNER	-	155 S.P. GUN CRF4	898=UNSFECIFIED TIME, BUT
: 67 LOAD	ER :	1		THAN USUAL TIME
W.H.				
2.				
FILE ASILPE	MSHPFRVISED : 5			

GRADF MUS IN ARE	GRADF :E=5 MUS :15#20 IN ARHY : 67% 4110 IN APITLI LPY : 67%	: 15820 : 678 4:	CH CH FOR	SAN YR CH.ANF SFCTION:10 AZ GHANER AS.GUNNER LOADER	NC T		4K 140		155 £	155 S.P. GUN CREW	SK EK			1 = 0 9990 = N 9 = N 9 9 E = U	OSNO INCRESE REDVE USUAL I INCRINGT DO IT AT ALL FORD FERLY 9=NO PEFLY (FOR CONFIDENCE) BREUNSFECFFIED TIME, BUT LON THAN USUAL TIME	IT AT AL FOR CONF D TIME,	OND TACKESE AFORE USUAL THE -IRCANNOT DO IT AT ALL 9990-NO REPLY 9=NO FEPLY (FOR CONFIDENCE) 898-UNSFECTFIED TIME, BUT LONGER THAN USUAL TIME	u or
CUMBAT ARTIL.	COMPAT			MSHPFRVISED : 5	•• ••								,	*				
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Appendix E

PERFORMANCE DATA INPUT VALUES FOR REGRESSION MODELING:
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n 4			0		3 ×	. 39	•53	. 46	. 59	• 32	• 22	• 40	.24	.37	46	.49
.	141	חו	1 1.	2.	25	\$ 25	• 45	.38	70.	• 26	.13	.31	18	.22	.25	25.
٠,	7101	בי	2.0	5.5	1	٠ د	. 43	.37	. 48	- 22	.07	.29	14	-21	30	.31
0 P		7.	50	٠. د	21.	25.	25	34	.01	.21	.09	.24	61.	2.	.27	24
	1111	020	0.731		56	S.	20.	64	.87	. 55	.31	• 16	.57	54	.80	.64
c a		ר, ש ה ע	U 0) L	200	20,1	57.	0	.77	.59	.33	9.	649	• 56	.64	.60
٠ ح		֓֞֜֜֜֝֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֓֓֡֓֓֓֓֡֓		ָ פּ		٠. د	֓֞֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֓֓֓֓֡֓֡		8 / ·	. 46	ク N	10.	47	5.5	.63	• 56
: -	-	•	• v	90		7 T	35.	٠ د د د	99•	5	٠ د د	5.	• 35	• 36	24.	64.
٠,	5 41		.:	•		7	5,0		3 (. 51		. 4 C	٠ ک	40	.51	4 4 5
: N	1 4 9 1	֓֞֜֜֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֓֡֓֓֓֓֡֓֡֓֓֡֓	4		- 0	7	, r	7	2	7	0	60	1.	.13	. 18	11
٦.		•	2 0	ָ מַ פּ	2	7.	•	0	9:	442	12.	.5	. 33	. 41	• 52	.51
ט ז	֓֞֜֜֜֜֜֝֓֓֓֓֓֜֜֜֜֜֓֓֓֓֓֜֜֜֜֓֓֓֡֓֜֜֜֜֓֓֡֓֜֜֡֓֡֓֡֓֡֓֡֓֡֓֡֓֡֡֡֡֓֡֡֓	7 (3	5	ر د	2	.31	.18	. 50	. 55 55	• 36	. 47	47
٠ ٦	7 6 6	֓֞֞֞֜֞֜֞֜֝֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֡֓֡֓֓֓֓֡֓֡֓֡֓֡֓֡֓֡	7	٠. د	7	200	5	35	8	22.	• 03	. 25	• 15	.22	.31	.31
0 6	. ה	7	7	֡֡֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֡֓֓֓֓֓֓֡֓֓֡֓֡	50	N.	19.	- 6	\$65	34	. 10	.37	. 23	.32	940	.40
~ @	7 - 0	(61.0		ני מי	_	21.	. 33	-) i		. 15	.03	.23	.13	.16	.25	.22
9		•	- =		ה ה ה ה	טינ	V ?	0	֭֭֓֞֞֞֜֜֞֜֜֜֝֓֓֓֓֜֜֜֜֟֜֜֓֓֓֓֓֓֓֜֜֜֟֓֓֓֓֓֓֓֜֜֜֝	7	.37	19.	52.	.57	.63	.56
٠ ح) ·	•	•	0,750	, 0 4	7 .	200	٠ د د	7.0	٠, د	2.5	5	32	30	939
.				-	0.101	00.	•	00.		n V	0	V		ν. Υ	. 55	,2,

a 1, Chief of section; 2, gunner; 3, assistant gunner; 4, driver.

b See Table 2 for task description.

Table E.2. FDC crewmember performance.

		0 906 0 704 0 779 0 709 0 709 0 808 0 707 0 708 0 708 0 708	2	•				_				
		90 90 17 17 10 10 10 10 10 10 10 10 10 10 10 10 10		5	-	2	M	4	Z.	9	7	8
		40770846	. 19	.86	8	98.	M	.79	7.8	8.	8.	.82
		077789797	0.861	0.882	-	0.945	٥.	0.851	0.864	0.874	0.890	0.847
→ → ○ ○ ○ ○ ○ ○ ○ ○ ○ ○ ○ ○ ○ ○ ○ ○ ○ ○		7. 7. 7. 8. 7. 9. 7. 9. 7. 9. 7. 9. 7. 9. 7. 9. 9. 7. 9. 9. 9. 9. 9. 9. 9. 9. 9. 9. 9. 9. 9.	• 65	.78	0	.73	.73	.65	.68	.61	.80	.70
- O O O O O O O O O O		7 0 8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	14	•76	.68	•76	. A B	7.4	.76	.72	.78	69
~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~		20 30 48 77 69 87	64.	.73	• 76	.76	A Z	€68	72	.67	.75	.64
~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~		30 77 69 78	.69	.74	• 59	.70	19	.75	. 7 .	.60	.77	•
() (1) (1) (1) (1) (1) (1) (1) (1) (1) (1)		48 77 69 78	• 49	.77	73	.80	. 88	.70	.72	464	79	7.1
W W W W W W W		77. 69. 78	• 46	• 56	. A 0	.47	.57	. 46	.53	.40	58	.57
W 50 100 100 100 100 100 100 100 100 100		. 69 78	· s.	.76	÷6	٥,	. A 0	.68	69.	.64	.79	.64
14 14 14 14 14 14 14 14 14 14 14 14 14 1		78	68	.74	.57	.72	.74	.68	.66	69.	.77	.62
M W W M	3111		• 64	• 76	.70	.80	. A 2	.66	99.	.59	79	.64
W K1 *1 F	3112	. 65	795	.72	.50	.72	.67	.61	63	.62	.76	56
W1 W1 W	14112	,54	. 55	•66	. 45	.57	•59	• 56	.57	.53	.70	.51
~ 1 ⊦	4113	, 42	• 45	5.5	.32	46	. 48	. 45	₩ 4 B	. 41	9.	349
•	2	. 47	. 43	\$2,	• 38	.50	.50	. 41	4 4 B	. 43	.51	. 40
	54231	.37	.43	.50	• 54	• 4≥	.42	.43	643	.37	. 55	. 35
	1111	69.	.67	.72	• 58	7.	.76	.67	.76	.59	.75	.59
ec i	2:11	.76	69.	.75	• 46	. 78	81	.61	.71	.70	.78	5.7
19 41	3111	°.8℃	.67	32.	\sim	8.		• 66	• 70	• 65	. B 3	.76
c	4	69.	,59	69•	.55	.73	.76	• 57 B	• 64	.57	.72	9
_	4112	. h 2	. 56	• 64	.50	• 65	88.	.57	61	55.	•60	.50
۸		.27	٠ در	4 W •	.18	.27	.36	82.	. 38	.22	3 į	.24
~	31:1	.60	.53	99.	.48	.63	99.	• 54	59	10.	69.	.53
7		.62	555	. f. 4	٠ س	,65	• 65	. 55	5.	.52	.68	. 48
r	5223	, ü 2	5	77.	333	41	. 54	.34	39	.32	. 48	.30
9	1	.50	70.	• 56	44	525	•68	. 43	.52	. 3.8	•58	0 7
2	54	٠. دي	. 37	77.	.22	.38	• 4 B	.35	.46	. 34	37.4	.31
	1111	.59		54	,46	•62	.67	.56	• 55	.53	67	5
5	_	617.	• 46	.35	, 3&	.51	.57	.47	.52	.41	60	. 41
o S		٠, د.	~	.47	.31	411	9	9	M	.35	52	33

 $^{\rm a}$ 1, Fire detection officer; 2, horizontal control operator; 3, computer, $^{\rm b}$ See Table 2 for task description.

Table E, 3. Tank crewmember performance.

Š	Symptom Complex	Ď	Crewmember Pos (P _K)	er Position ^a k)	e u)	Crewmember Tasks ^b (P _{jk})	ber Task jk)	qs		,	·
!		-	2	₩	e	-	~	₩	ø		9	7	· ec	6	9
-	111211	0	76.		949	.79	.93	85	98	.79	9	95	82	8	8
Λ	113111	06.	-92		.91	.78	.95	. A 5	06.	77	. 63	96	8	8	6
~	113121	. 84	.89	.74	E.	.72	9 R 9	. A 2	.83	.73	6	06	73	7	8
7	_	68	.79	.59	.67	.52	.71	9	77.	56	8	8	58	59	29
r ·	123111	• 76	2	68	.71	\$65	.80	.71	.79	99.	85.	.83	67	8	7.
.	-	. A 5	.87	18.	. A6	.70	9.	. A.	.86	7.4	38.	.89	7.9	. 32	86
~ (-	~7	æ.	99	.19	• 56	. A 0	.70	.74	.56	.85	.83	.65	99.	79
*	7	, 0	• 65	51	. 62	.42	. 62	.51	.58	447	.68	99	. 59	.50	.62
C		1	.82	74	.87	.63	.83	.72	.78	. 55	.85	.86	.71	74	87
-	1211	0.72	. 78	94.	.75	.57	.78	• 66	.73	•58	.81	.79	69.	.66	7.5
_ (5	0.75	.82		.77	.56	.82	69.	.78	.57	85	.84	74	.67	11
~	311	0.52	• 62	• 44	.57	. 30	• 60	. 47	.57	.37	.68	.64	.51	.43	.57
~		9.46	.57	.43	.53	.34	.53	39	.49	.38	.59	.58	.50	.42	53
7	1411	0.33	• 45	• 25	444	.22	• 36	30	.37	.25	47	49	.32	.24	44
<u>.</u>	1211	0.35	47	95.	.32	. 22	.39	•29	. 41	.28	51	4	31	.19	32
- 1	3423	0.31	. 43	. 33	•39	. 19	.37	.21	. 34	.30	. 45	44	.40	. 32	.39
_	1111	0.65	• 75	• 70	.78	.46	.74	9.	.71	• 44	.80	. 78	• 59	.73	.78
	=	S .	E,	• 68	11.	.61	.80	.71	.76	.61	.82	.83	.70	19.	11
	1511	0.0	۶. د	40.	• 76	46	• 78	•64	.71	• 50	.84	90	• 65	•64	• 16
	1411	56.0	֭֡֞֞֞֓֓֓֟֝֓֓֓֟֝֟֝֟֓֓֓֟֟֓֓֓֟֟֓֓֓֓֟֟֓֓֓֟֟֓֓	. 52	.63	47	.68	53	.65	64.	.74	174	• 58	• 50	.63
	141	0 .	היי	4 4	ָבָּ מַלְי	. 52	3	24.	52.	• 26	• 64	63	2.	44	. 56.
7	•) C	10 L	0.507	0000	C 6 0 0	64190	0.130	0.00	140.0 140.0	0.040	0.416	0.195	0.112	0.768
	1 4 1 1	0.48	5.4	49	9	40		. 4	. r) ·	• 4	5.7	. 0 C	•	, N
	1522	0.33	.43	24	36	2	37	26	38	22	2	4	28	24	36
	153	~	.51	. 32	.39	. 25	42	30	45	27	. 56	54	42	31	39
	154	•26	.39	20	.33	.13	.31	24	. 28	.17	44	.42	31	19	33
	7	•	.	.54	• 65	.43	.62	.51	.57	47	99.	. 65	54	54	.65
	5	.21	.37	24	.35	.18	•29	24	31	.23	. a 2	.36	35	.23	.35
	151	12.	.38		.33	• 20	.36	.24	.37	25.	44	.39	.29	.20	.33
,															

^a 1, Tank commander; 2, horizontal control operator; 3, loader; 4, driver. b See Table 2 for task description.

Table E.4. TOW crewmember performance.

	Symptom		ewmemb (P	er Positio	ona			Crewn	nember T (P _{jk})	asks ^b		
NO.	Complex	1	2	3	4	1	5	3	4	5	6	7 -
1	112111	0.899	0.865	0.964	0.872	0.906	0.883	0.799	0.886	0.964	0.876	0.869
S	112121	0.891	0.863	0.948	0.857	0.902	0.869	0.780	0.890	0.948	0.857	0.837
3	113111	0 868	0.830	0.917	0.882	0.871	0.860	0.758	0.853	0.417	0.874	0.070
Ã	113121	0.813	0.768	0.895	0.824	0.816	0.807	0.692	0.793	0.875	0.010	0.031
5	114111	0.718	0.596	0.786	0.558	0.695	0.767	0.428	0.672	0.705	0.566	0.220
6	123111	0 766	0.719	0.873	0.748	0.769	0.759	0.612	0.758	0.8/3	0.745	0.750
7	211111	0 879	0.853	0.945	0.876	0.982	0.873	0.801	0.869	0.945	0.864	0.000
P,	213111	n 791	627	n 856	0.703	0.800	0.774	0.477	0.689	0.756	0.713	0.675
9	224111	0 605	n 539	0.785	0.606	0.615	0.581	0.397	0.500	0.102	0,790	0.012
10	211111	n A26	A 75A	0.926	0.833	0.830	0.814	0.657	0.770	(1.760	U.057	11.0.21
11	212111	0 710	0.638	0.854	0.765	0.735	0.664	0.507	0.607	0.034	0.767	0.100
12	212111	704 0	0.656	0.901	0.730	0.711	0.670	0.505	0.718	0.401	U./54	0.767
13	212112	A 513	n 454	0.641	n.446	0.516	0.506	0.336	0.505	0.041	0.432	0.401
14	414112	A 498	n 412	0.586	0.397	0.517	0.464	0.201	0.474	0.200	0.507	(1,447
15	21 A 1 1 Z	0.402	0.316	0.455	0.207	0.405	0.390	0.196	0.384	V.433	0.197	0.514
16	315113	0.325	0.278	0.442	0.515	0.342	0.296	0.154	0.355	0.442	0.107	0.247
17	ママムコマイ	n 287	0.209	0.391	0.251	0.296	0.270	0.103	0.276	0.571	0.250	0.207
18	411111	0.743	0.658	0.923	0.785	0.735	0.750	0.76/	0.107	U.763	U. / 07	0.100
19	412111	0.770	0.750	0.893	0.756	0.781	0.747	0.642	0.701	0.073	0.750	0.133
20	413111	0.699	0.604	0.827	0.686	0.696	0.704	0.423	0.687	0.02/	0.501	0.071
21	414111	0.648	0.545	0.741	0.525	0.653	0.639	0.343	0.612	0.741	0.330	0.061
22	414112	0.495	0.415	0.586	0.398	0.499	0.488	0.248	0.514	0.500	0.303	0.414
23	415314	0.211	0.180	0.301	0.130	0.203	0.559	0.104	0.250	0.701	0.130	0.131
24	513111	0.592	0.511	0.729	0.567	0.624	0.751	0.362	0.200	0.740	0.370	0.565
25	514111	0.542	0.467	0.700	0.468	0.555	0.522	0.315	4 246	0.700	0.457	0.461
26	515223	0.318	0.1/0	0.315	0.136	0.290	0.3/1	0.0/3	0.787	0.530	Noll'	0.101
۲۶.	515311	0.402	0.179	0.730	0.237	0.377	0.407	0.147	0.301	0.330	0.152	0.188
85	515431 521111	0.267	0.179	0.344	0.100	V. 230	A 497	0.515	4 677	A 776	0 682	0.692
29	525111	0.722	0.033	0.760	0.00/	0.737	0.073	0.313	0.424	0.468	0.170	0.178
30	535111	0.3/7	0,337	0.467	0.174	0.371	0.377	6 174	0 351	0.457	0.227	0.240
31	111121	0,70.7	0.707	0.077	0.030	0.040	0 921	0 873	0 926	0.973	0.921	0.939
32	111131	V.734	0.714	0.784	0 KQ0	0 KA2	0 662	0.472	0.670	0.780	0.642	0.706
33	112131	V.010	7.013 A EE7	0.771	0.677	154 0	0.584	0.400	0.628	0.771	0.618	0.623
54 35	113131	U FUB	V 674	0 752	O ADA	0.672	0.604	0.444	0.629	0.753	0.632	0.624
วา 36	114112	A AAG	0.025	0 52A	0 344	0 496	0.477	0.284	0.492	0.528	0.326	0.365
37	212111	A A 22	0.742	0 882	0 788	0.844	0.814	0.669	0.766	0.882	0.793	0.763
31 31)	214112	0.053	0.414	0.574	0.377	0.459	0.43A	0.274	0.489	0.574	0.376	0.3/8
39	214113	0 7A7	n 256	0 455	0.191	0.347	0.335	0.146	0.325	0.455	0.185	0.198
37 40	617113	U . 373	0.491	0,701	0 501	A SAS	A 57A	0 339	0 563	0 701	0 507	0.494

 ^{1,} Squad leader; 2, gunner; 3, driver; 4, loader.
 See Table 2 for task description.

Appendix F

PERFORMANCE-DATA REGRESSION MODELING

G. Eall

INTRODUCTION

This appendix addresses the problem of fitting linear regression models to data, focusing on the task of fitting least squares regression equations and assessing the accuracy of the fit. Most basic texts describe the general least squares mode and the methodology used to obtain, for example, regression parameter estimates, standard errors, Student's t-statistics, and the analysis of variance table (e.g., Cook and Weisberg [1982], Draper and Smith [1982], Daniel and Wood [1980], Mosteller and Tukey [1977], and Seber [1977]). Although a review is provided here, we assume some familiarity with least squares models.

We discuss how to select and develop models that fit the data well, how to use regression diagnostics to detect model anomalies (e.g., outliers, leverage points), and what to do about them. We address multicollinearity, correlation among model error terms, and transformation of the response and factor variables.

GENERAL LINEAR MODEL

Assume a data set of n observations or cases, where the ith case consists of an observation of a response variable y_i and measures of p' explanatory (factor) variables $x_{i1}, x_{i2}, \ldots, x_{ip'}$. Let x_i be the vector $x_i' = (1, x_{i1}, \ldots, x_{ip'})$ and p = p' + 1. We assume that the response variable y_i is related to the factor variables x_i by a model of the form

$$y_i = G(x_i; \beta; \epsilon_i)$$
, (F.1a)

where the functional form of G is specified, β is a vector of unknown parameters to be estimated from the data, and ε_i is an *unobservable* random error. More generally, the left-hand side of Eq. (F.1a) may be replaced by a function F(y) of y; that is, we may have

$$F(y_i) = C(x_i; \beta; \epsilon_i)$$
, (F.1b)

where, for example, F(*) could be

$$F(y) = \log y , \qquad (F.2a)$$

$$F(y) = \log\left(\frac{y}{1-y}\right) , \qquad (F.2b)$$

$$F(y) = y^{1/2}$$
, (F.2c)

$$F(y) = \frac{y^{\lambda} - 1}{\lambda}$$
, some λ . (F.2d)

Choice of a transformation F is discussed below (pp. 384-386). For now, we assume F(y) = y.

Faced with the choice of specifying a form for G, and lacking any theoretical considerations that might suggest one, we initially assume that G is of the form

$$G(x_i; \beta; \epsilon_i) = x_i'\beta + \epsilon_i$$
.

Thus the model is

$$y_{i} = x_{i}'\beta + \varepsilon_{i}$$

$$= \sum_{j=0}^{p'} x_{ij}\beta_{j} + \varepsilon_{i} , \qquad (F.3)$$

where $\beta' = (\beta_0, \beta_1, \dots, \beta_p)$ is an unknown vector of regression parameters to be estimated from the data and ϵ_i is an unobservable random error term.

In matrix notation, let Y be the n x 1 vector of responses:

$$Y = \begin{bmatrix} y_1 \\ y_2 \\ \vdots \\ y_n \end{bmatrix}.$$

Let X be the $(n \times p)$ factor matrix whose ith row is x_i ,:

$$X = \begin{bmatrix} 1, & x_{11}, & \dots, & x_{1p}, \\ 1, & x_{21}, & \dots, & x_{2p}, \\ & & \vdots & & \vdots \\ 1, & x_{n1}, & \dots, & x_{np}, \end{bmatrix}$$

Finally, let ϵ be the n x 1 vector of unobservable error terms.

Then the linear model relating the response Y to the factor matrix \boldsymbol{X} is

$$Y = X\beta + \varepsilon$$
 (F.4)

The model is termed linear because it is linear in the regression vector β . If the model were, say,

$$y_{i} = e^{x_{i}'\beta} + \varepsilon_{i} , \qquad (F.5)$$

then it would be nonlinear because it is nonlinear in β . If some variables in X were nonlinear functions of other variables in X, the model would still be linear as long as Eq. (F.4) is the assumed model. For example, if X contains quadratic and cross-product terms involving other factor variables, Eq. (F.4) would still yield a linear model.

In addition to Eq. (F.4), the usual modeling assumptions are as follows:

- 1. $E\varepsilon_i = 0$ (appropriate model).
- 2. The unobservable error terms ϵ_1 , ϵ_2 , ..., ϵ_n all have the same variance, var $(\epsilon_i) = \sigma^2$.
- 3. The error terms are uncorrelated, cov $(\varepsilon_i, \varepsilon_i) = 0$, $i \neq \ell$.
- 4. The error in measuring x is small relative to var ε_i .
- 5. The error terms ϵ and factor variables X are uncorrelated.
- 6. The error terms ε_{i} are approximately normally distributed.

In the model developed here, assumptions 1, 4, and 5 are always true.

Standard least squares regression references show that the least squares estimate for $\boldsymbol{\beta}$ is

$$\hat{\beta} = (X'X)^{-1}X'Y , \qquad (F.6)$$

and the estimate for the variance σ^{2} of the error term is

$$\hat{\sigma}^2 = \frac{1}{n-p} \sum_{i=1}^{n} (y_i - \hat{y}_i)^2, \qquad (F.7)$$

where \hat{y}_{i} is the prediction of y_{i} ,

$$y_i = x_i'\hat{\beta}$$
,

and $e_i = y_i - \hat{y}_i$ is the *ith* residual. The vector of predictions \hat{Y} is $\hat{Y} = X\hat{\beta}$ and the vector of residuals is $e = Y - \hat{Y}$. Least squares methodology selects $\hat{\beta}$ to minimize the vector inner product

$$e'e = (Y - X\hat{\beta})'(Y - X\hat{\beta})$$

$$= \sum_{i=1}^{n} (y_i - x_i \hat{\beta})^2.$$

Since

$$\hat{\beta} = (X'X)^{-1}X'Y,$$

then

$$\hat{Y} = X\hat{\beta}$$

$$= X(X^{\dagger}X)^{-1}X^{\dagger}Y .$$

Thus, if

$$H = X(X^{\dagger}X)^{-1}X^{\dagger},$$

then

$$\hat{Y} = HY$$
,
 $e = Y - \hat{Y}$
 $= (I - H)Y$.

The matrix H is both symmetric (H' = H) and idempotent (H^2 = H), and is the linear transformation that orthogonally projects any n vector onto the space spanned by the columns of X.

Since the linear model is $Y = X\beta + \epsilon$ and $(I - H)X\beta = 0$, we compute

$$e = (I - H)Y$$

$$= (I - H)(X\beta + \varepsilon)$$

$$= (I - H)\varepsilon.$$

Then, if $H = (h_{ij})$, in scalar form we have

$$e_i = \epsilon_i - \sum_{j=1}^n h_{ij} \epsilon_j$$
.

Thus the relationship between the unobservable model errors (ε_i) and the computed residuals (e_i) depends solely on H = X(X'X)⁻¹X'--i.e., on the factor variables. If all the h_{ij} are sufficiently small, e will serve as a reasonable substitute for ε ; ε : rwise, the usefulness of e may be limited.

Returning to Eq. (F.6). \cdot e reexpress $\hat{\beta}$ as

$$\hat{\beta} = (X'X)^{-1}X'Y$$

$$= (X'X)^{-1}X'(X\beta + \epsilon)$$

$$= \beta + (X'X)^{-1}X'\epsilon.$$

Thus, since we assumed that $E\varepsilon = 0$, the expected value $E\hat{\beta}$ of $\hat{\beta}$ is

$$E\hat{\beta} = \beta + (X'X)^{-1}X'E\varepsilon$$

$$= \beta . \qquad (F.8)$$

That is, $\hat{\beta}$ is an unbiased estimate of β , whether or not the error terms ϵ have constant variance σ^2 , are uncorrelated, or are normally distributed. It is still essential that X and ϵ be uncorrelated. The estimate $\hat{\sigma}^2$ of σ^2 , however, is affected by violation of the model assumptions, as discussed below (pp. 19-25).

Since $\hat{\beta} = \beta + (X'X)^{-1}X'\epsilon$, if it is assumed that var $\epsilon = \sigma^2I$, where I is the n x n identity matrix (i.e., the error terms ϵ_i have the same constant variance σ^2 and are uncorrelated), then

$$\operatorname{var} \hat{\beta} = \operatorname{var} \left[(X'X)^{-1}X'\epsilon \right]$$

$$= (X'X)^{-1}X' \left(\operatorname{var} \epsilon \right) X(X'X)^{-1}$$

$$= \sigma^{2} \left(X'X \right)^{-1}. \tag{F.9}$$

Equation (F.9) is the expression for the variance/covariance matrix of $\hat{\beta}$. The corresponding estimated variance/covariance matrix is $\hat{\sigma}^2(x^*x)^{-1}$.

Again, if it is not the case that var $\varepsilon = \sigma^2 I$ (if, for example, var $\varepsilon = \sigma^2 V$, where V is not the identity matrix I), then Eq. (F.9) will give an incorrect assessment of the variance of $\hat{\beta}$.

Typical Output from Regression Package

In addition to providing the estimates $\hat{\beta}$ of β and $\hat{\sigma}^2$ of σ^2 , current computer packages also provide the standard errors (standard deviations) of the regression parameter estimates, the corresponding Student's t-statistics, and R^2 . These statistical parameters are described here.

Recall that the variance/covariance matrix of $\hat{\beta}$ is the p x p matrix

$$\sigma^2(x'x)^{-1}$$
,

and its estimate is $\hat{\sigma}^2(x^*x)^{-1}$. For each j, $1 \le j \le p$, the standard error of the estimate $\hat{\beta}_j$ --i.e., its standard deviation--is the square root of the jth diagonal element,

$$\hat{\sigma} \sqrt{[(X'X)^{-1}]_{ii}}.$$

We denote this as $\hat{\sigma}_{\beta_i}$.

The corresponding Student's t-statistic for $\hat{\beta}_i$ is

$$t_{j} = \frac{\hat{\beta}_{j}}{\hat{\sigma}_{\beta_{j}}}.$$

This statistic is used to test the null hypothesis H_0 : $\beta_j = 0$ against the alternative H_A : $\beta_j \neq 0$. The statistic is Student's t, with n - p degrees of freedom. If $t(n-p, 1-\alpha/2)$ is the value for which $\alpha/2$ percent of the t distribution is greater than $t(n-p, 1-\alpha/2)$ [and, by symmetry, $\alpha/2$ percent less than $-t(n-p, 1-\alpha/2)$] and if

$$|t_j| \ge t \left(n - p, 1 - \frac{\alpha}{2}\right)$$
,

then H_0 is rejected in favor of H_A . Generally, for $n-p \ge 12$, $t(n-p, i-\alpha/2) \approx 2.0$.

One global measure of the precision of the estimated regression is the multiple correlation coefficient R^2 . To derive R^2 , note that the *ith* residual e_i may be written

$$e_i = y_i - \hat{y}_i$$

= $y_i - \overline{y} - (\hat{y}_i - \overline{y})$.

Taking the square and summing over the n cases, we obtain [Draper and Smith, 1981]

$$\sum_{i} e_{i}^{2} = \sum_{i} (y_{i} - \overline{y})^{2} - \sum_{i} (\hat{y}_{i} - \overline{y})^{2}$$

or

$$\sum_{i} (y_{i} - \overline{y})^{2} = \sum_{i} e_{i}^{2} + \sum_{i} (\hat{y}_{i} - \overline{y})^{2}.$$

The left-hand side is referred to as the sum of squares about the mean, or the corrected sum of the squares of y. Since \mathbf{e}_i is the ith residual and $\hat{\mathbf{y}}_i = \bar{\mathbf{y}}$ is the deviation of the ith predicted value $\hat{\mathbf{y}}_i$ from the mean, this equation says that

 $\frac{\text{Sum of squares}}{\text{about the mean}} = \frac{\text{Sum of squares}}{\text{about regression}} + \frac{\text{Sum of squares}}{\text{due to regression}}.$

Thus, some of the variation in y about the mean can be ascribed to the regression and some, Σe_i^2 , to the fact that not all of the observed y lie on the regression line.

Now $\Sigma(y_i-\bar{y})^2$ is fixed, since it is a function of the observed data. The sums Σe_i^2 and $\Sigma(\hat{y}_i-\bar{y})^2$ depend on the model chosen (the form of the model, selection of x variables, outliers, etc.). We desire that Σe_i^2 , the sum of squared residuals, be small. Dividing both sides of the identity by $\Sigma(y_i-\bar{y})^2$, we obtain

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$$1 = \frac{\sum_{i=1}^{\infty} e_{i}^{2}}{\sum_{i=1}^{\infty} (y_{i} - \overline{y})^{2}} + \frac{\sum_{i=1}^{\infty} (\hat{y}_{i} - \overline{y})^{2}}{\sum_{i=1}^{\infty} (y_{i} - \overline{y})^{2}}.$$

Thus, the model may be regarded as "good" if R^2 is near unity, which is given as

$$R^{2} = \frac{\sum_{i=1}^{2} (\hat{v}_{i} - \bar{y})^{2}}{\sum_{i=1}^{2} (y_{i} - \bar{y})^{2}}$$

$$= 1 - \frac{\sum_{i=1}^{2} (y_{i} - \bar{y})^{2}}{\sum_{i=1}^{2} (y_{i} - \bar{y})^{2}}$$

Note that $0 \le R^2 \le 1$, always.

However, as seen below (p. 384), R^2 is not the only measure of the accuracy of the model. It should also be noted that the sum $\Sigma(y_i-\bar{y})^2$ has n-1 degrees of freedom, Σe_i^2 has $n-p^{i-1}$ degrees of freedom, and $\Sigma(\hat{y}_i-\bar{y})^2$ has p'degrees of freedom. Equivalently, Σy_i^2 has n degrees of freedom, $n\bar{y}^2$ has one degree of freedom, Σe_i^2 has n-p degrees of freedom (p = p'+1), and $\Sigma \hat{y}_i^2$ has p degrees of freedom. The statistical parameters discussed in this subsection provide the basis for the standard analysis of variance tables from regression packages.

Confidence Bounds

Here we discuss confidence bounds for the *conditional mean* of y, given x, and bounds on a *future* observed value, given x. If $y = x'\beta + \epsilon$ and $\hat{\beta}$ is a least squares estimate of β , then, as we saw earlier,

$$\operatorname{var} \hat{\beta} = \sigma^2(\mathbf{X}^{\dagger}\mathbf{X})^{-1} .$$

Thus, $x^{\dagger}\hat{\beta}$ is the predicted value of the conditional mean, $E(y|x)=x^{\dagger}\hat{\beta}$, and the variance is

$$var (x'\hat{\beta}) = x' (var \hat{\beta})x$$

$$= \sigma^2 x' (X'X)^{-1} x$$

$$= \sigma^2 h ,$$

where

$$h = x'(X'X)^{-1}x$$
.

A "two sigma" or "two standard deviation" confidence band on the conditional mean $E(y|x)=x^{\dagger}\beta$ is

$$(\mathbf{x}'\hat{\boldsymbol{\beta}} - 2\sigma \sqrt{\mathbf{h}}, \mathbf{x}'\hat{\boldsymbol{\beta}} + 2\sigma \sqrt{\mathbf{h}})$$
.

This confidence interval depends only on the uncertainty in the estimate $\hat{\beta}$ of β . If there were no uncertainty in $\hat{\beta}$, then var $(x^{\dagger}\hat{\beta})$ = 0 and the confidence interval would have zero width.

Regarded as a function of x, the band [L(x), U(x)] provides an approximate, 95 percent confidence band on the regression surface, if L(x) = $x^{\dagger}\hat{\beta} - 2\sigma \sqrt{h}$, U(x) = $x^{\dagger}\hat{\beta} + 2\sigma \sqrt{h}$.

A related, but different problem is that of predicting an actual response y, given a new x. The prediction of the observed $y = x^* \hat{\beta} + \epsilon$ is $x^* \hat{\epsilon}$, but its variance is ϵw

var
$$(x'\hat{\beta} + \varepsilon) = \text{var } (x'\hat{\beta}) + \text{var } \varepsilon$$

= $\sigma^2 h + \sigma^2$
= $\sigma^2 (1 + h)$.

Thus, the upper and lower 95 percent confidence bounds on a future observed value are

$$L_0 = x^{\dagger} \hat{\beta} - 2\sigma \sqrt{1 + h} ,$$

$$U_0 = x^{\dagger} \hat{\beta} + 2\sigma \sqrt{1 + h} ,$$

which can be much wider than the earlier interval, if h << 1. For the actual data, the interval (U_0, L_0) should contain roughly 95 percent of the observed values of y, whereas [L(x), U(x)] will contain a much smaller percentage.

REGRESSION DIAGNOSTICS

This section discusses various diagnostics used for assessing the accuracy of linear regression models. The diagnostics include two basic components, described above (p. 373). The two basic building blocks for assessing accuracy are

1. The computed residuals,

$$e = Y - \hat{Y}$$
$$= (I - H)Y.$$

2. The Tukey hat matrix H,

$$H = X(X^{\dagger}X)^{-1}\dot{x}^{\dagger} .$$

The ith elements of the two building blocks are, respectively,

1.
$$e_i = y_i - \hat{y}_i$$

 $= y_i - x_i^* \hat{\beta}$,
2. $h_{ij} = x_i^* (X^* X)^{-1} x_j$, $1 \le j \le n$.

All commonly used current regression diagnostics are based on these two quantities or slight modifications. Among the most useful of diagnostics using residuals are

- 1. The residuals $e_i = y_i \hat{y}_i$ themselves, which can be used in
 - Plot e versus y.
 - Plot e versus each individual x
 - Plot e against other variables left out of the model.

Unfortunately, var $e_i = \sigma^2(1 - h_{ii})$, so these residuals do not have constant variance.

2. The internal studentized residuals,

$$r_{i} = \frac{e_{i}}{\hat{\sigma} \sqrt{1 - h_{i}}}.$$

Unlike the ordinary residuals in diagnostic 1, the $\mathbf{r_i}$ have common constant variance 1. Therefore, the plots mentioned in diagnostic 1, using the $\mathbf{r_i}$ rather than the $\mathbf{e_i}$, are more useful. Normal probability plots of the $\mathbf{r_i}$ plotted on normal probability paper are also more useful for assessing normality than plots of the $\mathbf{e_i}$.

Residuals are also used to discover which cases [i.e., pairs (x_i, y_i)] are outliers in the response space Y, i.e., cases for which $e_i = y_i - x_i^* \beta$ is large. But if $|e_i|$ is large, does case i have a significant effect on the estimates β and/or $\hat{\sigma}$? What would happen if the iterate were removed from the data base (as is frequently done with

outliers)? If $\hat{\beta}_{(i)}$ and $\hat{\sigma}_{(i)}$ are the estimates of β and σ with case i removed, how different are $\hat{\beta}_{(i)}$ and $\hat{\beta}_{i}$, $\hat{\sigma}_{(i)}$ and $\hat{\sigma}$?

The answers to those questions depend in part on the position of \mathbf{x}_i in the factor (explanatory variable) space. Ultimately, they depend on the hat matrix H. Recall that $\mathbf{H} = \mathbf{X}(\mathbf{X}^t\mathbf{X})^{-1}\mathbf{X}^t$ is an idempotent symmetric projection matrix, and that

$$\hat{Y} = HY,$$

$$e = (I - H)Y$$

$$= (I - H)\epsilon.$$

Since (I - H)H = 0 (idempotency), the predicted value \hat{Y} and the residuals e are orthogonal.

Also, since H is idempotent and symmetric, it follows that

$$tr(H) = rank(H) = p$$
,

$$\sum_{i=1}^{n} h_{i,j}^{2} = h_{i,i}.$$

Note that

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$$tr (H) = \sum_{i=1}^{n} h_{ii}$$
.

Moreover, it can be shown [Cook and Weisberg, 1982] that, if c is the number of times the ith row of $X-x_i^*$ --is replicated, then

$$\frac{1}{n} \le h_{11} \le \frac{1}{c}.$$

For the IDP regression analysis, each row is replicated only once, so

$$\frac{1}{n} \leq h_{ij} \leq 1.$$

Since

$$\sum_{i=1}^{n} h_{i,i} = p^{-i},$$

then

$$\frac{1}{n} \sum_{i=1}^{n} h_{i,i} = \frac{p}{n} = h ,$$

the average. Recall that var $e_i = \sigma^2(1-h_{ii})$. Thus, if $h_{ii} = 1$, then var $e_i = 0$, so $\hat{y}_i = y_i$ —i.e., the ith case is fitted perfectly. Such extreme cases are rare but possible. The farther a value h_{ii} is from the average p/n toward 1, the more influential is the ith case on the estimates $\hat{\beta}$ and σ . For the models selected in the Intermediate Dose Program, p = 7 and n = 30, so $h = p/n \approx 0.23$. But there are three cases (symptom complexes 16, 22, 27) for which h_{ii} is greater than 0.6. Those cases are high-leverage points. Thus, the residuals e_i and r_i are measures of outliers in the response space Y, and high-leverage points are measured by the diagonal elements h_{ii} of the Tukey hat matrix $H = X(X^iX)^{-1}X^i$, which depends only on the factor variable matrix X. The elements $\{h_{ii}\}$ are a measure of how far out in the factor space X each factor variable x_i lies.

A third class of diagnostics combines measures of extremeness in the response space Y with measures of extremeness in the factor space X. These are referred to as influence diagnostics or influence measures. As mentioned earlier, a case i is important or influential if deletion of case i from the data base causes a significant shift in the estimate of β . Letting

 $\hat{\beta}$ = estimate of β based on full data set, $\hat{\beta}_{(i)}$ = estimate of β with ith case deleted,

we seek the difference

$$\Delta \beta_{(i)} = \hat{\beta}_{(i)} - \hat{\beta}$$
, $1 \le i \le n$.

If $\Delta \beta_i$ is large relative to some suitable scale, then case i is deemed influential and should be examined to see if something unique or unusual might justify its permanent exclusion from the data base.

Alternatively, the relationship between y and x may be somehow different from the model specification in a neighborhood of the case $(\mathbf{x_i}, \mathbf{y_i})$. Consequently, we seek a suitable norm, $\|\Delta \mathbf{\beta_i}\|$, to assess the significance of $\Delta \mathbf{\beta_i}$. Since $\Delta \mathbf{\beta_i}$ is a p-dimensional vector, from vector-space theory a general class of useful norms is determined by a symmetric, positive semidefinite p \times p matrix M and a positive scale factor c:

$$\|\Delta\beta_{i}\| = D_{i}(M, c)$$

$$= \frac{(\Delta\beta'_{i})M(\Delta\beta_{i})}{c}$$

$$= \frac{(\hat{\beta}_{(i)} - \hat{\beta})'M(\hat{\beta}_{(i)} - \hat{\beta})}{c}$$

One of the most useful choices is M = X¹X and c = $p\hat{\sigma}^2$. We obtain

$$D_{i} = D_{i}(X^{\dagger}X, p\hat{\sigma}^{2})$$

$$= \frac{(\hat{\beta}_{(i)} - \hat{\beta})(X^{\dagger}X)(\hat{\beta}_{(i)} - \hat{\beta})}{p\hat{\sigma}^{2}}.$$

This metric norm, known as Cook's distance, is algebraically equivalent

$$D_{i} = \frac{1}{p} r_{i}^{2} \frac{h_{i i}}{1 - h_{i i}}$$

where r_i are the studentized residua,, and $b_{i\,i}$ are the diagonal elements of the hat matrix. Case i is influential if D_i is large, and D_i is large if

- 1. $|\mathbf{r}_{i}|$ is large and \mathbf{h}_{ii} is moderate (an outlier in response space).
- 2. $|\mathbf{r}_i|$ is moderate and $\mathbf{n}_{i\,i}$ is large (a high-leverage point in factor space).
- 3. Both $|r_i|$ and h_{ij} are moderately large.

The exact definition of "large" will depend on the problem, but a basis for comparison is usually obtained with D_i greater than 1, corresponding to distances between $\hat{\beta}$ and $\hat{\beta}_{(i)}$ beyond a 50 percent confidence region (using an F distribution with p and n - p degrees of freedom).

In the IDP, the largest Cook's-distance values for the linear model with the six factor variables were around 0.6 to 0.7. A value of 0.6 corresponds to a 25 percent confidence ellipsoid for an F distribution with 7 and 23 degrees of freedom. Thus, none of the 30 symptom complex combinations would be considered particularly influential, indicating that the n Lel is reasonable.

TRANSFORMING THE RESPONSE VARIABLE

When the original response variable is not normal, a transformation of it may be sufficiently close to normal to allow application of the appropriate normal theory methods. Ideally, a transformation should permit a model with constant error variance, approximately normal errors, and an easily interpreted and scientifically meaningful structure.

In the IDP, the selected response variable y is basically a ratio of two times, and is always in the closed interval [0, 1], i.e., $0 \le y \le 1$. Thus, the response variable is restricted in range. If the usual linear model is selected, i.e.,

$$y = x'\beta + \varepsilon$$
,

then it is quite possible to obtain predicted values $x^{\dagger}\hat{\beta}$ that lie outside the interval [0, 1]. Moreover, even if $x^{\dagger}\hat{\beta}$ were in [0, 1] for values of x of practical interest, upper and lower 95 percent confidence bounds of $x^{\dagger}\hat{\beta}$ could still lie outside the interval. Further, if y is near 0 or 1, less variability would be expected than if y were near 0.50--that is, var ε should be nonconstant.

The typical transformation used to ensure the (0, 1) interval is the logit transformation,

logit
$$(y) = ln\left(\frac{y}{1-y}\right)$$
, $0 < y < 1$.

This transformation is symmetric about the value y = 0.5 and roughly linear in the region $0.2 \le y \le 0.8$, which contains most of the IDP responses averaged over individuals. In that region, the logit model will give predicted values and upper and lower confidence bounds similar to those of the usual model, $y = x^{\dagger}\beta + \epsilon$. The two models will differ when y is near 0 or 1 (say, $y \le 0.1$ or $y \ge 0.9$).

Thus, the logit model specifies that

$$y^* = \mathcal{L}_i \left(\frac{y}{1-y} \right) = x^* \beta + \epsilon$$
,

where

$$y^* = \omega_i \left(\frac{y}{1-y} \right)$$

is the response variable. Once the model is fitted, the predicted value of y^* is

$$\hat{y}^* = x^* \hat{\beta}$$

and upper and lower 95 percent confidence bounds are

$$L_{95}^{\star} \cong x'\hat{\beta} - 2 \sqrt{h} \hat{\sigma} ,$$

$$U_{95}^{\star} \cong x'\hat{\beta} + 2 \sqrt{h} \hat{\sigma} ,$$

where $h = x'(X'X)^{-1}x$.

Thus, the predicted value $\hat{\boldsymbol{y}}$ for \boldsymbol{y} and upper and lower confidence bounds are

$$\hat{y} = \frac{e^{\hat{y}^*}}{1 + e^{\hat{y}^*}} = \frac{e^{x'\hat{\beta}}}{1 + e^{x'\hat{\beta}}} = \frac{1}{1 + e^{-x'\hat{\beta}}},$$

$$l_{.95} = \frac{e^{L^*}}{1 + e^{L^*}} = \frac{1}{1 + e^{-(x^*\hat{\beta} - 2\sqrt{h}\hat{\sigma})}},$$

$$U_{95} = \frac{e^{U^*}}{1 + e^{U^*}} = \frac{1}{1 + e^{-(x^*\hat{\beta} + 2\sqrt{h}\hat{\sigma})}}$$

Hence, \hat{y} , L_{95} , and U_{9} will always be in the interval (0, 1), as desired.

MULTICOLLINEARITY

Again let the linear model in matrix form be

$$Y = XB + \varepsilon$$
.

where X is an n \times p matrix, the ith row (1 \le i \le n) being the factor variable (vector) for the ith case and the jth column (1 \le j \le p) corresponding to the jth explanatory variable. For the IDP, p \ge 7, so we allow X to contain quadratic and cross-product terms involving the original six explanatory variables.

Problems involving multicollinearity arise when one or more columns of X are nearly linear combinations of other columns of X. In that case,

 $(X'X)^{-1}$ becomes unstable, since X'X has rank p. If one column of X (say, i_0) is a perfect linear combination of other columns, then X'X is not invertible—i.e., it is singular. In that case, the effects of the factor variable \mathbf{x}_{i_0} on the response cannot be ascertained, since \mathbf{x}_{j_0} is a perfect linear combination of several other factor variables.

Multicollinearity of several factor variables has the following effects on the overall regression analysis:

1. Perfect multicollinearity implies that (X'X) is singular; hence, there are no unique unbiased least squares estimates of B.

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- 2. If there is multicollinearity even though (X'X) is invertible, the individual effects of the separate factor variables on the response variable cannot be reliably ascertained.
- 3. Estimates of variances of individual regression coefficients will be large, yielding wide confidence intervals.

Consequently, it is important to determine whether a particular regression model is adversely affected by multicollinearity. Many different measures have been proposed. Most, however, have one or more serious drawbacks. For example, examining the correlation matrix of $\mathbf{x}_1,\dots,\mathbf{x}_p$ reveals only pairwise collinearity. One of the best procedures is to scale X'X so as to have ones along the diagonal, then compute the ordered eigenvalues $\mu_1 \geq \mu_2 \geq \cdots \geq \mu_p$ for the scaled matrix [Belsley, Kuh, and Welsch, 1980]. The jth condition index is

$$k_{j} = \left(\frac{\mu_{1}}{\mu_{j}}\right)^{1/2}.$$

If any k, exceeds roughly 30, collinearity will be a problem.

For the IDP, the largest condition index was about 12.7, using the six basic symptom variables. Thus, for those six factor variables, collinearity is not a problem.

CORRELATION AMONG MODEL ERROR TERMS

Until now, we have assumed that the regression model is of the form

$$y_i = x_i^{\dagger} \beta + \epsilon_i$$
, $1 \le i \le n$,

where $\cos(\epsilon_i, \epsilon_l) = 0$, $i \neq l$ --i.e., that the model error terms are uncorrelated. For the IDP, however, since each respondent gives an answer to each symptom complex, it is reasonable to assume that each person's set of answers should be correlated--hence, that $\cos(\epsilon_i, \epsilon_l) \neq 0$, for $i \neq l$.

It can be shown that, although the least squares estimate of $\hat{\beta}$ is still an unbiased estimate for β , $\hat{\sigma}^2$ is biased when there is nonzero error covariance. Assume that the model now is

$$\text{var } \varepsilon_i = \sigma^2 \ , \qquad \text{$l \le i \le n$, }$$

$$\text{cov } (\varepsilon_i, \ \varepsilon_\ell) = \rho \sigma^2 \ , \qquad \text{$l \le i \ne \ell \le n$, }$$

where $0 \le \rho \le 1$. This model belongs to a class termed generalized least squares. If ρ is known, estimates for β and σ^2 can be obtained without too much difficulty. When ρ is unknown, maximum likelihood (ML) techniques must be used. Unfortunately, use of ML strongly depends on multivariate joint normality assumptions for large n, which cannot be justified for our data. Therefore, we resort to the alternative of computing the expected bias in $\hat{\sigma}^2$, then using a correction factor (inflation factor) to adjust for the bias.

Since the ordinary least squares (OLS) estimate of β is

$$\hat{\beta} = (x^*x)^{-1}x^*Y$$

$$= (x^*x)^{-1}x^*(x\beta + \epsilon)$$

$$= \beta + (x^*x)^{-1}x^*\epsilon,$$

and since $E\epsilon \in 0$, we see that we get

$$E\hat{\beta} \equiv \beta$$
.

Thus, $\hat{\beta}$ is still unbiased. However, as we now show, the estimate $\hat{\sigma}^2$ of σ^2 is biased downward. We show that in fact

$$E\hat{\sigma}^2 = \sigma^2(1 - \rho) .$$

Recall that

$$\hat{\sigma}^2 = \frac{(Y - X\hat{\beta})!(Y - X\hat{\beta})}{n - p}.$$

Let

$$S = (Y - X\hat{\beta})^{*}(Y - X\hat{\beta})$$

$$= [Y - X \cdot (X^{*}X)^{-1}X^{*}Y]^{*}[Y - X \cdot (X^{*}X)^{-1}X^{*}Y]$$

$$= [(I - H)Y]^{*}[(I - H)Y]$$

$$= [(I - H)(X\beta + \epsilon)]^{*}[(I - H)(X\beta + \epsilon)]$$

$$= \epsilon^{*}(I - H)\epsilon,$$

since

$$(I - H)X = 0$$
 and $(I - H)^2 = I - H$.

Letting $\ddagger = \sigma^2 V = cov \ \epsilon$, and using a theorem from random quadratic forms [Searle, 1971], we obtain

ES = tr
$$[(I - H)^{\ddagger}]$$

= σ^2 tr $[(I - H)^{\dagger}]$,

where tr (*) is the trace of a matrix (i.e., the sum of its diagonal elements), and

$$\mathbf{V} = \begin{bmatrix} 1 & \rho & \rho & \dots & \rho \\ \rho & 1 & \rho & \dots & \rho \\ \rho & \rho & 1 & \dots & \rho \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ \rho & \rho & \rho & \dots & 1 \end{bmatrix}$$

If ρ = 0, then V = I (the identity matrix) and

$$ES = \sigma^{2} \text{ tr } (I - H)$$
$$= \sigma^{2}(n - p) ,$$

since

$$tr I = n$$
 and $tr H = p$ (H has rank p),

implying that $\hat{\sigma}^2$ is unbiased. But if $\rho\neq 0$, write

$$V = I + oL$$

where

$$I = \begin{bmatrix} 1 & 0 & 0 & \dots & 0 \\ 0 & 1 & 0 & \dots & 0 \\ \vdots & \vdots & \vdots & & & \vdots \\ 0 & 0 & 0 & \dots & 1 \end{bmatrix}$$

and

$$L = \begin{bmatrix} 0 & 1 & 1 & \dots & 1 \\ 1 & 0 & 1 & \dots & 1 \\ \vdots & \vdots & \vdots & & \vdots \\ 1 & 1 & 1 & \dots & 0 \end{bmatrix}$$

Thus,

ES =
$$\sigma^2$$
 tr [(I - H)(I + ρ L)]
= σ^2 {tr (I - H) + ρ tr [(I - H)L]}
= σ^2 [n - p - ρ tr (HL)],

since

$$tr(I-H) = p$$
 and $trL = 0$.

However,

$$H = (h_{ij})$$
,

so

$$\text{HL} = \begin{bmatrix} \sum_{j=2}^{n} \mathsf{h}_{1\,j} & \dots & \dots & \dots \\ & \dots & \sum_{j\neq 2}^{n} \mathsf{h}_{2\,j} & \dots & \dots \\ & \dots & \dots & \sum_{j\neq 3}^{n} \mathsf{h}_{3\,j} & \dots \\ & \dots & \dots & \dots & \sum_{j\neq n}^{n} \mathsf{h}_{n\,j} \end{bmatrix}$$

Therefore,

tr (HL) =
$$\sum_{i=1}^{n} \sum_{j\neq i}^{n} h_{ij}$$
.

Since

$$\sum_{i=1}^{n} e_i = 0 .$$

then

$$0 = var \left(\sum_{i=1}^{n} e_{i}^{i} \right)$$

$$= \sum_{i=1}^{n} \operatorname{var} e_{i} + \sum_{i \neq j}^{n} \operatorname{cov} (e_{i}, e_{j})$$

$$= \sigma^2 \sum_{i=1}^{n} (1 - h_{ii}) + \sigma^2 \sum_{i \neq j}^{n} (-h_{ij})$$

or

$$\sum_{i \neq j}^{n} h_{i,j} = \sum_{i=1}^{n} (1 - h_{i,i}) = n - p.$$

Thus,

$$tr(liL) = n - p$$

Hence,

ES =
$$\sigma^2(n + p - \rho(n - p))$$

= $\sigma^2(n - p)(1 - \rho)$

$$E\hat{\sigma}^2 = \sigma^2(1 - \rho) .$$

Thus, if $\hat{\sigma}^2$ is an estimate of σ^2 based on ordinary least squares and $\hat{\rho}$ is a reasonable estimate for ρ , then an inflation-factor-adjusted estimate for σ^2 is

$$\sigma^2 = \frac{1}{1 - \hat{\rho}} \hat{\sigma}^2$$

or

$$\tilde{\sigma} = \frac{\hat{\sigma}}{(1 - \hat{\rho})^{1/2}}.$$

Using a package from STATLIB, an estimate for ρ between 0.2 and 0.4 was obtained. Thus, the inflation (correction) factor $(1 - \hat{\rho})^{-1/2}$ varies from 1.12 to 1.30--i.e., $\hat{\sigma}$ is too low by about 10 to 30 percent.

TRANSFORMING FACTOR VARIABLES

As indicated above (p. 12), it is useful to plot the residuals (either ordinary or studentized) against each factor variable \mathbf{x}_j . A uniform horizontal band in the individual plots indicates a satisfactory model. If, however, a residual plot against \mathbf{x}_j displays some sort of curvature, a transformation of \mathbf{x}_i is in order.

Further, for data like those of the IDP, it is important to determine the effect, if any, of combinations of variables as opposed to individuals. That is, cross-product effects between explanatory (factor) variables may have a greater influence on the response variable than does the appearance of either variable alone.

Thus, in addition to using the standard six variables x_1, \ldots, x_6 (corresponding to upper GI, etc.), we tried to incorporate quadratic terms x_1^2, \ldots, x_6^2 and cross-product terms $x_1 x_j, 1 \le l \ne j \le 6$. Unfortunately, because there were only 30 combinations of the six symptom

complexes in the data, with little variation in the last three of the six factor variables, the analysis was beset with extreme problems caused by both multicollinearity and high-leverage cases.

Many of the quadratic and cross-product terms were found to be either exactly collinear with linear combinations of the original six variables, or so close to perfectly collinear that only one symptom complex combination of the 30 prevented exact collinearity. That is, if the one combination were removed from the data, perfect collinearity would result. Consequently, the one combination would be classed as both a high-leverage and extremely influential data point. Cook's distances of greater than 15 were observed, whereas a value of one normally causes concern. Consequently, we decided that introducing higher-order terms in the model would be fruitless, since the factor variables were so sparse in range variability. Thus, only the original six factor variables were retained.

Appendix G

PERFORMANCE PREDICTIONS FOR CREWMEMBER TASKS

This appendix gives performance data for the separate crewmember tasks. Regression parameters are also listed for fitting the performance prediction (logit) model to the task data.

Figures C.1 through G.12 are plots of crewmember separate task and position performance shown for comparison. Performance values for crewmember position, determined from the separate tasks as given in Sec. 3, lie along the straight line plotted against performance degradation (1 - P). The tick marks along the top of the abscissa correspond to symptom complexes ordered as given in Tables 12 through 27 in Sec. 3. The performance plots and regression parameters are given for crewmembers who have two or more tasks; the artillery chief of section, tank driver and TOW driver are not included, since they perform a single task.

Tables G.1 through G.4 list the regression relationship parameters for fitting the task data. Like the performance prediction relationships for the crewmembers given in Sec. 3, task performance predictions are given by

$$\hat{P}_{k,j} = \frac{1}{\left[1 + \exp\left(-\frac{x_{k}'\hat{\beta}_{i}}{2}\right)\right]},$$

where $x_k' = (1, x_{k1}, x_{k2}, \dots, x_{k6})$ is a vector of integers $(1 \le x_{kl} \le 5)$, denoting symptom severity level for the kth symptom complex and the lth symptom category, and $\hat{\beta}_j$ are the beta parameters given in Tables G.1 through G.4, for a particular task j.

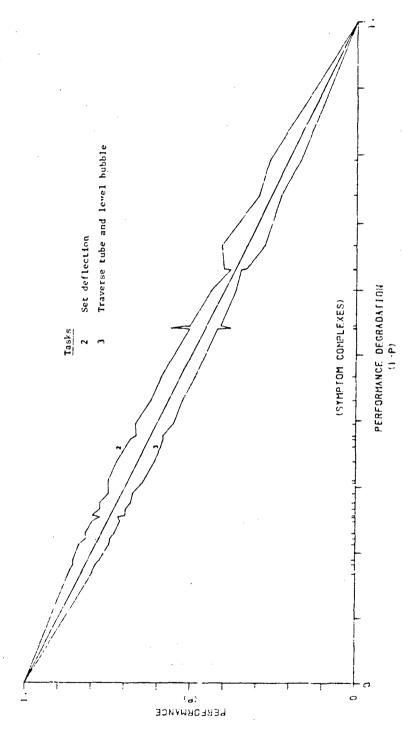
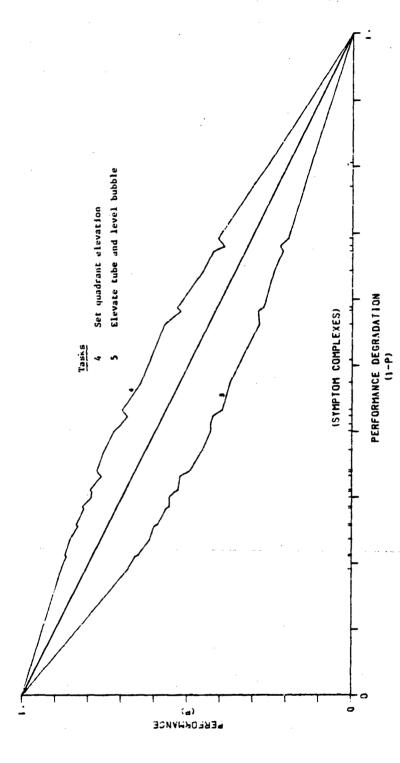


Figure G.1. Task/position performance: gun crew, gunner.



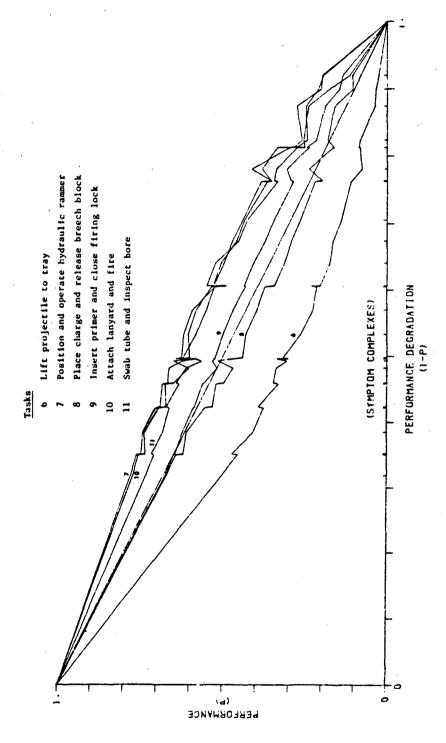
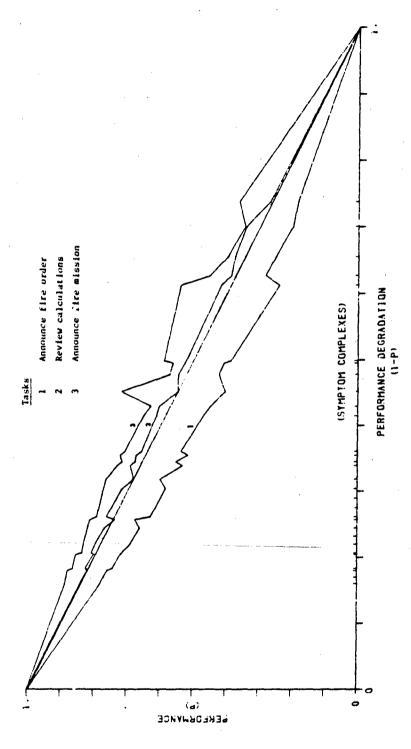


Figure G.3. Task/position performance: gun crew, loader.



Task/position performance: FDC crew, fire direction officer. Figure 6.4.

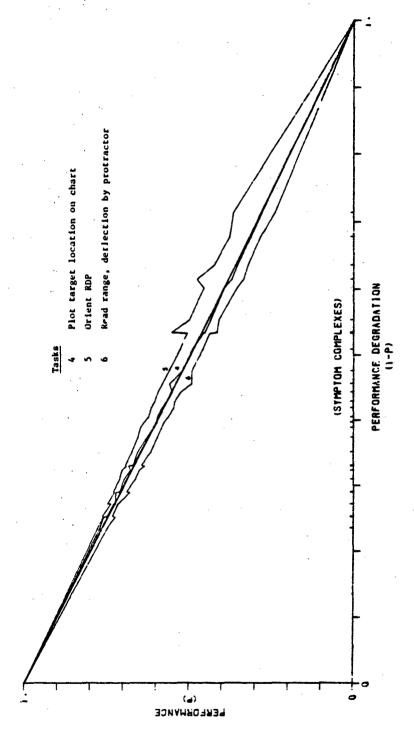


Figure G.5. Task/position performance: FDC crew, horizontal control operator.

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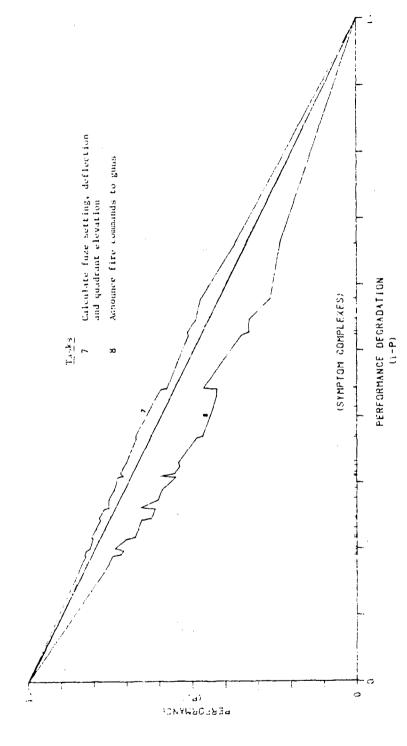


Figure G.6. Task/position performance: FDC crew, computer.

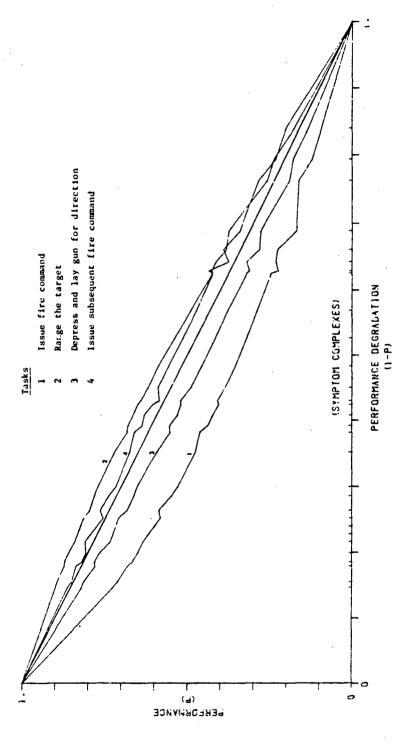


Figure G.7. Task/position performance: tank crew, tank commander.

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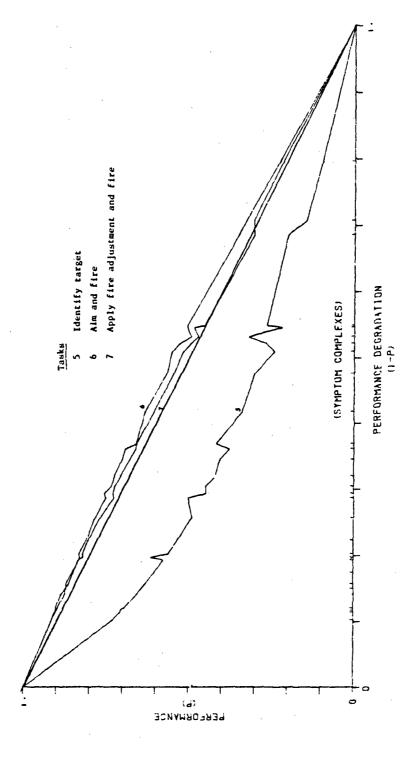


Figure G.8. Task/position performance: tank crew, gunner.

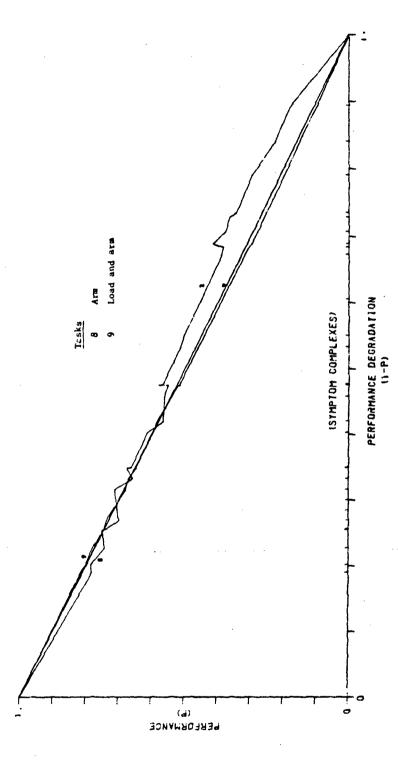


Figure G.9. Task/position performance: tank crew, loader.

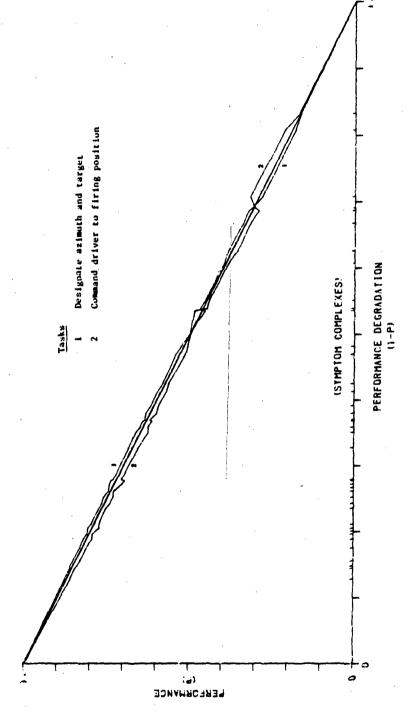


Figure G.10. Task/position performance: TOW crew, squad leader.

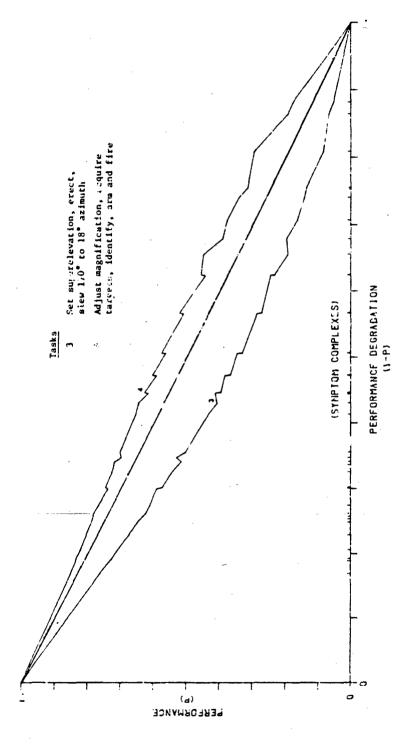


Figure G.11. Task/position performance: TOM crew, gunner.

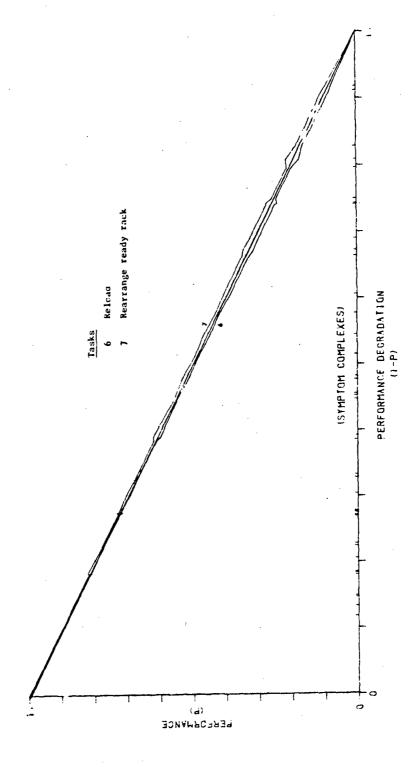


Figure G.12. Task/position performance: TOW crew, loader.

Table G.1. Regression results, gun crew.a

	TASK	NUMBER	2	FAS	K NUMBER	3
	RETA .	STANDARD	STUDENT	BETA	STANDARD	STUDENT
SYMPTOM	PARAMETER	FHROR	T	PARAMETER	ERHOR	ī
INTERCEPT	₹.689165	0_278924	13.226	3.040915	0.209406	14,522
HPPER GASTRU	-0.133953	0.053964	-2.482	-0.154725	0.040514	-3.819
LUWER GASTRO	-0.412253	0.136164	-3.028	-0.335025	0.102228	-3.277
FATIGUE/WEAK	-0.269009	0.067568	- 7.981	-0.235993	0.050728	-4.652
HYPOTENSTON	-0.088056	0.140524	-0.627	-0.22dA13	0.105501	-2.169
THEETT/ALEFD	-0.267431	0.171796	-1.557	-0.121214	0.124979	-0.940
FLHIR LOSS	-0.470530	0.100484	-4.683	-0.419712	0.075440	-5.564
	R SQUARED =	0_8629		P SUHARED	= 0.9123	
	RMS ERKOR =			RMS ERROR		
	UGF =			nGF		
	FACK	NUMBER 4		TAN	C MUMBER 5	
			,	, , ,	, , , , , , , , , , , , , , , , , , ,	•
	RETA	STANDARD	STUDENT	BFTA	STANDARU	STHEENT
SYMPTOM	PARAMETER	FRRUR	Ť	PARAMETER	ERROR	T
THTERCEPT	3.871579	U.281584	13.749	2.317021	0.173881	13.525
UPPER GASTRU	-0.120934	U.05447A	-5.220	-0.146709	0.033641	-4.361
LUWER GASTRO	-0.437978	0.137462	-3.186	-0.319346	0.184884	-3.762
FATIGUE/WEAK	-0.272550	515890.0	-3.996	-0.248783	0.042121	-5.900
HYPOTENSTON	-0.140113	0.141864	-0.98 8	-0.124267	0.087602	-1.427
THECT/ALEED	-0.258543	0.173435	-1.491	-0.183087	0.107097	-1.710
FLUID LUSS	-0.497201	0.101442	-4.901	-0.389378	0.062641	-0.216
	R SQUARED =	0.8703		R SQUARED =	0.9305	
	RMS ERHOR =	0.371217		RMS ERROR =	-	
	DGF =			DGF =		
	TARK	NUMBER 6		7.0		
				1.43	NUMBER 7	
	RETA	STANDARD	STUDENT	BFTA	STANDARD	STUDENT
SYMPTOM	PARAMETER	FRROR	Ť	PARAMETER	ERROR	T
INTERCEPT	1.982098	0.229575	8.654	3.060085	0.187109	16.355
HEPER GASTRO	-0.195948	0.044416	-4.412	-0.104743	0.036260	-2.693
LOWER GASTRO	-0.244156	0.112073	-2.179	-0.448053	0.091342	-4.905
FATIGUE/WEAK	-0.325548	0.055613	-5.854	-0.285835	0.045326	-6.306
HYPOTENSION	-0.304213	0,115662	-2.630	-0.238311	0.094267	-2.528
TNFECT/BLEFD	-0.233430	0.141401	-1.651	-0.119442	0.115245	-1.076
FLUID LUSS	-0.463313	0.082706	-5.602	-0.493279	0.067407	-7.318
	R SOUARED =	0.9324		R SQUARED =	0.9405	
	RMS ERROR =			RMS ERROR =		
	UGF =			ngf =		

Table G.1. Regression results, gun crew (Concluded).

	TASK	NUMBER &	3	TASK	NUMBER 9	
	RETA	STANDARD	STUDENT	BFTA	STANDARD	STUDENT
SYMPTOM	PARAMETER	FRRUR	Ť	PARAMETER	ERROR	Ť
INTERCEPT	2.226995	0.170504	13.061	2.217452	0.195405	11.348
IPPER GASTRU	-0.135262	0.032988	-4.100	-0.116195	0.037805	-3.074
LUWEP GASTRU	-0.248694	0.083236	-2.988	-0.251282	0.095392	-2.634
FATIGUE/WEAK	-0.363318	0.041303	-3.796	-0.250744	0.047336	-5.297
HYPOTENSION	-0.004918	0.085901	-0.057	-0.094368	0.098446	-0.459
INFECT/BLEED	-0.247384	0.105017	-2.356	-0.273690	0.120354	-2.274
FLUID LOSS	-0.374360	0.061425	-6.095	-0.384500	0.070395	-5.462
	R SQUARED =	0.9430		R SQUARED =	0.9079	
	HMS ERHOR =			RMS ERROR =	0.257605	
		24		ngf =	23	
	TASK	NUMBER 10	ı	TASK	NUMBER 11	
	BETA	STANDARD	STUDENT	BFTA	STANDAPD	STUDENT
SYMPTOM	PARAMETER	FRROR	Ť	PARAMETER	ERROR	1
INTERCEPT	2.753800	0.235600	11.688	2.584123	0.166072	15.560
UPPER GASTRU	-0.096342	0,045562	-2.114	-0.126504	0.032170	-3.937
LOWER GASTRO	-0.323004	0.115014	-2.808	-0.369957	0.081072	-4.563
FATIRUF/WEAK	-0.304344	0.657073	-5.333	-0.215333	0.040230	-5.353
HYPUTENSTON	-0.034336	0.114697	-0.289	-0.126132	0.083668	-1.508
INFECT/BLEED	-0.290475	0.145112	-2.002	-0.250991	0.102287	-2.454
FLUID LOSS	-0.381880	0.084876	-4.499	-0.354653	0.059828	-5.928
	R SQUARED =	0.8822		R SUHARED =	0.9287	
	RMS ERHOR 3	0.310595		RMS FRRUR =	0.218935	
	UGF 3	24		ngF =		

^aTask number 1 regression parameters are those given for the chief of section in Sec. 3.

Table G.2. Regression results, FDC crew.

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	TAS	K NUMBER		TASK	NUMBER	2
SYMPTOM	BETA Parameter	STANDARD ERROR	STUDENT	RETA PARAMETER	STANDARF ERROR	STUDENT T
THTERCEPT	3.068488	0.359570	8.534	3.407176	0 275770	
HPPER GASTRO	-0.269195	0.069568	-3.870		0.335379	
LOWER GASTRO	-0.468424	0.175533	-1.669	-0.194729	0.064886	
FATIGUE/WEAK	-0.063502	0.087104		-0.550326	0.163724	
HYPUTENSTON	-0.195820	0.181154	-0.729	-0.082766	0.081243	
THEET/BLEED	-0.2A305A		-1.081	-C.225097	0.168966	
FLUID LUSS	-0.457986	0.221468	-1.278	-0.148599	U.206568	
(COAD LOGG	-0.43/400	0.129537	-3.576	-0.461945	0.150455	-3.823
	P SQUARED :	. 0.7774		R SOUARED =	0 7778	
	RMS ERROR :	0.470027		RMS ERROR =	•	
	NGF =			UGF =		
				40.		
	TASK	NUMBER 3	;	TASK	NUMBER	4
,	BETA	STANDARD	STUDENT	8574		
SYMPTOM	PARAMETER	ERROR	1 100 6 14 1	RETA Parameter	STANDARD	STUDENT
# · · · · · · · · · · · · · · · · · · ·	MARKET E	LANDA	•	PARAMEIRA	FRRUR	T
TNTEPCEPT	3.918948	0.400721	9.780	2.537191	0 174543	14 624
HPPER GASTRO	-0.256229	1.077528	-3.305	-0.188812	0.173542	14.620
LOWER GASTRO	-0.552430	0.195622	-2.424	-0.1338537	0.033777	-5.623
FATIGUE/HEAK	-9.041489	0.097072	-0.427	-0.124433	*	+3.996 -3.960
HYPUTENSTON	0.013608	0.201887	0.067	-0.135473	0.042040	-2.96n
INFECT/BLEED	-0.396276	0.246814	-1.606	-0.099580	0:106869	-1.549
FLUID LUSS	-0.587077	0.144362	-4.067	-0.315565	-	-0.932 -4.095
		,	-4.007		0.062520	-4.995
	R SQUARED =	0.7303		R SQUARED =	0 4976	
	RMS FRROR =			RMS ERROR =		
	ngF =			UGF =		
				-		
	TASK	NUMBER 5		TASK	NUMBER (5
	BETA	STANDARD	STHOENT	BETA	STANDARD	STUDENT
SYMPTOM	PARAMETER	ERHOR	I	PARAMETER	FRROR	T
			•	T ANALYSE TEN	FREGE	'
THTERCEPT	2.378963	0.182964	13.002	2.439342	0.262973	9.276
UPPER GASTRO	-0.175230	0.035398	-4.950	-0.204814	0.050878	-4.026
LOWER GASTRO	-0.301139	0.089319	-3.371	-0.380811	0.128377	-2.966
FATIGUE/WEAK	-0.081759	0.044322	-1.845	-0.082486	0.1203.7	~1.295
HYPOTENSTON	-0.043004	0.092179	-0.467	-0.179482	0.132488	*1.355
THECT/BLEED	-0.131882	0.112692	-1.170	-0.081187		
FLITTO LOSS	-0.311628	0.065914	-4.728	-0.337566	0.161971	-0.501
	2 6 2 5 6 10 40 10		- 4.750	-0 - 33 L 100	0.094737	-3.563
	R SQUARED =	0.8476		R SQUARED =	0 7944	•
	PMS ERROR =			RMS ERROR =		
	DGF =			UGF =		
		• •		, ver -	<u>د ۲</u> .	

Table G.2. Regression results, FLC crew (Concluded).

•	TASK	NUMBER 7		TASK NUMBER &		
SYMPTOM	BFTA PARAMETER	STANDARD ERROR	STUDENT	META Parameter	STANUARD ERROR	STUDENT T
INTERCEPT HPPER GASTRU LOWER GASTRU FATIGUE/WEAK MYROTEMSION INFECT/OLEFU FLUID LUSS	2.952502 -0.142595 -0.475095 -0.043908 -0.248592 -0.007846 -0.325918 R SUNARED =		16.031 -4.002 -4.739 -1.881 -2.679 -0.069 -4.927	2.558462 -0.217167 -0.816009 -0.044161 -0.124583 -0.175913 -0.421898 R SQUARED RMS ERROR	= 0.294233	11.463 -5.029 -3.818 -0.817 -1.108 -1.280 -5.247

Table G.3. Regression results, tank crew. a

	TASK	NUMBER 1		TASH	NUMBER - 2	!
•	BETA	STANDARD	STUDENT	8E∴A	STANDARD	STUDENT
SYMPTOM	PARAMETER	ERROR	Τ΄	PARAMETER	FRROR	T
INTERCEPT	2.824024	0.271434	10.404	4.352746	0.313823	13.870
UPPER GASTRU	-U.286400	0.052515	-5.454	-0.327168	0.06071	-5.389
LUWER GASTRO	-0.412689	0.132507	-3.114	-0.571206	0.153201	-3.728
FATIGUE/WEAK	-0.213909	0.065753	-3.253	-0.265402	0.076022	-3.491
HYPOTENSION	-0.214144	0.136751	-1.566	-0.192390	0.158106	-1.217
INFECT/BLEED	-0.068180	0.167183	-0.408	-0.012041	0.193291	-0.062
FLITT LUSS	-0.439119	0.097785	-4.491	-0.525015	0.113054	-4.644
	R SQUARED =	0.8871		R SQUARED =	0_8879	
Í	PMS ERROP =			RMS ERHOR =	•	
	nGF ≠			DGF =		
:	TASK	NUMBER 3		TASK	NIMBER 4	
	BETA	STANDARD	STUDENT	BETA	STANDARD	STUDENT
SYMPTOM	PARAMETER	ERHOR	T	PARAMETER	FRROR	T
THTEPCEPT	3.461919	0.231725	14.940	3.762089	0.237709	15.826
HPPER GASTRO	-0.297045	0.044832	-6.626	-0.305305	0.045990	-6.639
LOWER GASTRO	-0.504297	0.113122	-4.458	-0.473994	U.116044	-4.005
FATIGUE/WEAK	-0.255146	0.056134	-4.545	-0.197353	0.057584	-3.427
HYPOTENSION	-0.179685	0.116745	-1.539	-0.143962	0.119760	-1.202
INFECT/BLEFD	0.009123	0.142725	0.064	-0.128056	0.146411	-0.875
FLIIIN LOSS	-0.458394	0.083480	-5.491	-0.474361	0.085636	-5.539
	R SUHARED #	0.9233		R SQUARED =	0.9128	
ì	RMS ERROR =	0.305487		RMS ERROR =	0.313376	
	ngF ±	23		URF =	23	
	TASK	NUMBER 5		TASK	NUMBER 6	
	BFTA	STANDARD	STUDENT	BETA	STANDARD	STUDENT
SYMPTOM	PARAMETER	ERROR	1	PARAMETER	FHRUR	1
INTERCEPT	2.610335	0.227222	11.488	4.419381	0.242622	18.215
HPPER GASTRO	-0.286496	0.043961	-6.517	-0.309911	0.046940	-6.603
LUMER RASTRO	-0.352076	0.110924	-3.174	-0.633196	0.118442	-5.346
FATIGUE/WEAK	-0.172275	0.055043	-3.130	-0.159524	0.058774	-2.714
HYPOTENSION	-0.237827	0.114476	-2.078	-0.222908	U_122235	-1.824
INFECT/BLEFO	0.059603	0.139951	0.426	0.017539	0.149437	0.117
FLUID LUSS	-0.456446	1.081858	-5.576	-0.579837	0.087406	-6.634
	R SQUARED =	0.9084		R SQUARED =	0.9192	
•	RMS ENROR =			RMS ERROR =	•	
	ngF =			UGF =		

Table G.3. Regression results, tank crew (Concluded).

TASK NUMBER :

	BETA		STANDARD	STUDENT
SYMPTOM	PARAMETER		ERROR	T -
INTERCEPT	4.180210		0.303280	13.783
HPPER GASTRO	-0.248242		0.058148	-4.269
LOWER GASTRO	-0.260567		0.149415	-1.744
FATIGUE/WEAK	-0.517479		0.070561	-7.334
HYPOTENSION	0.079068		0.144651	0.547
THECT/BLEED	-0.371420		0.122143	-3.041
FLHID LUSS	-0.597669		0.107218	-5.574
	R SUHARED	=	0.8933	
	PMS FRROR	1	0.427812	
	ngF	=	7.7	

TASK NIMBER &

TASK NUMBER 9

			•	1-01 101021 4			
SYMPTOM	RETA Parameter	STANDARN FROOR	STUDENT T	HETA Parameter	STANDARD ERROR	STUDENT	
TNTEPCFPT UPPER GASTRU LOWER GASTRU FATIGUF/WEAK MYPOTENSTUN INFECT/OLEFO FLUID LOSS	2.883474 -0.212662 -0.367667 -0.192157 -0.100430 -0.060938 -0.468161	0.194320 0.037595 0.04762 0.047673 0.097906 0.119687	14.839 -5.657 -3.876 -4.082 -1.026 -0.509	3,441871 -0,276692 -0,462628 -0,322628 -0,19425 0,004835 -0,528678	0.219059 0.042382 0.106939 0.053066 0.110364 0.134924	15.712 -5.349 -4.326 -6.080 -1.725 0.006 -6.699	
	R SQUAKED = RMS ERKOR = DGF =	0.256176		R SQUARED			

^aTack number 10 regression parameters are those given for the driver in Sec. 3.

Table G.4. Regression results, TOW crew.^a

	TASK	NUMBER 1		TASK	NIIMBER	2
	BETA	STANDARD	STUDENT	BETA	STANDARD	STUDENT
SYMPTOM	PARAMETER	ERROR	T	PARAMETER	FRROR	Ť
INTERCEPT	3.944742	0.280672	14.053	3.704884	U_294205	13.056
UPPER GASTRO	-0.225626	0.053813	-4.193	-0.233399	0.054491	-4.283
LUWER GASTRO	-0.263445	0.138276	-1.905	-0.288117	0.140017	-2.058
FATIGUE/WEAK	-0.374660	0.065301	-5.737	-0.354899	0.066123	-5.367
HYPOTENSTON	0.012139	0.133848	0.091	0.124455	V.135553	0.918
INFECT/BLEED	-U.384484	0.113037	-3.401	-0.413633	U.114460	-3.614
FLHID LOSS	-0.516037	0.099225	-5.201	-0.493189	U.100474	-4.909
	R SQUARED =	0.8683		R SQUARED =	0 4212	
	RMS ERROR =			RMS ERHOR =		
	ngF =	-		UGF =	•	
·	TASK	NUMBER 3		TARK	NUMBER 4	
				7 701		•
	BFTA	STANDARU	STUDENT .	META	STANDARD	STUDENT
SYMPTOM	PARAMETER	ERHOR	ī	PARAMETER	ERROR	Т
INTERCEPT	3.379075	0.701455	11.077	3.565372	0.267341	13.336
UPPER GASTRO	-0.279193	0.057798	-4.830	-0.216770	0.051258	-4.229
LUMER GASTRO	-0.207870	0.148516	-1.400	-0.253533	0.131709	-1.925
FATIRUE/WEAK	-0.438429	0.070137	-6.251	-0.335201	0.062200	-5.349
HYPOTENSION	-0.003845	0.143780	-0.027	0.022988	0.127510	0.100
INFECT/BLEFO	-0.473434	0.121406	-3.900	-0.344564	0.107668	-7.200
FLHIP LUSS	-0.488139	0.106573	-4.580	-0.481393	0.094512	-5.093
	R SQUAPED =			R SQUARED =	0.8593	
	RMS ERROR =			RMS ERROR =	U.377116	
	ngF ≠	33		DGF =	33	
	7.0	* **********				
	1 4 3 1	NIMBER (6	TASK	NUMBER 7	
	BETA	STANDARD	STUDENT	BETA	STANDARD	STUDENT
SYMPTOM	PARAMETER	FRROR	r	PARAMETER	ERROR.	T
INTERCEPT	4.335487	0.287865	15.061	4.464494	0.276733	16.133
HPPER FASTRU	-0.254126	0.055193	-4.604	-0.319320	0.053540	-5.964
LUWER GASTRO	-0.272422	0.141820	-1.921	-0.641741	0.135094	-4.750
FATIGUE/WEAK	-0.527975	0.066975	-7.783	-0.210481	0.067037	-3.140
HYPUTENSION	0.038926	0.137298	0.1	+0.192817	0.139420	-1.383
INFECT/BLEFD	-0.408598	0.115934	~3. 52°	0.032442	0.170447	0.190
FLUID LUSS	-0.643662	0.101768	-6.325	-0.557558	0.099695	-5.593
	R SQUAHED =	0.9111		R SUHARED =	0.9039	
	HMS ERHOR =			RMS FRRUR =		
	DRF =	33			53	

^aTask number 5 regression parameters are those given for the driver in Sec. 3.

Appendix H

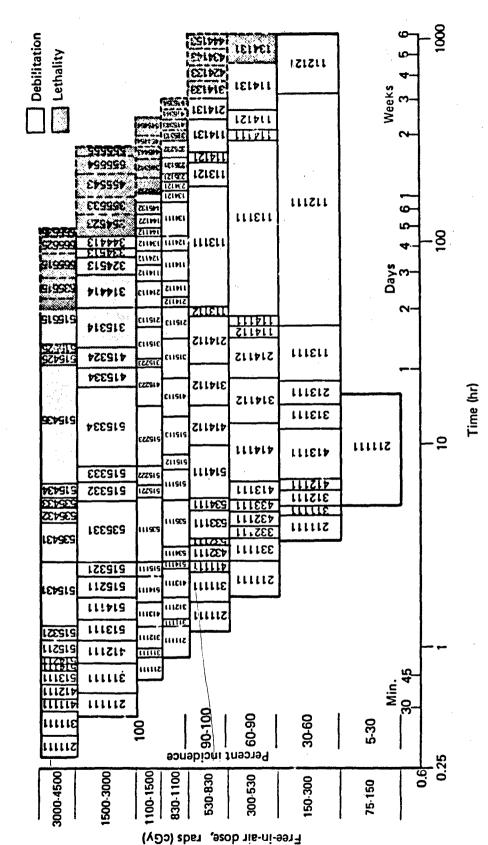
EARLY LOWER GASTROINTESTINAL DISTRESS EFFECT ON PERFORMANCE

This appendix shows the effect of early lower gastrointestinal distress (LG) on performance. As discussed in Sec. 4, that effect is due to one or two brief episodes of diarrhea that may occur in a minority of individuals—about 10 percent with a maximum of 30 percent at high doses of the intermediate dose range.

Figures H.1 and H.2 give the symptom complexes, including the early LG effect. Figures H.3 through H.6 are three-dimensional plots for the gun crew loader, FDC computer, tank commander, and TOW loader, chosen to illustrate the early LG effect on performance. Beginning with doses from around 300 to 450 rads (cGy) and for times between about 2 to 6 hr, the initial surface depression is largely attributable to early LG effects.

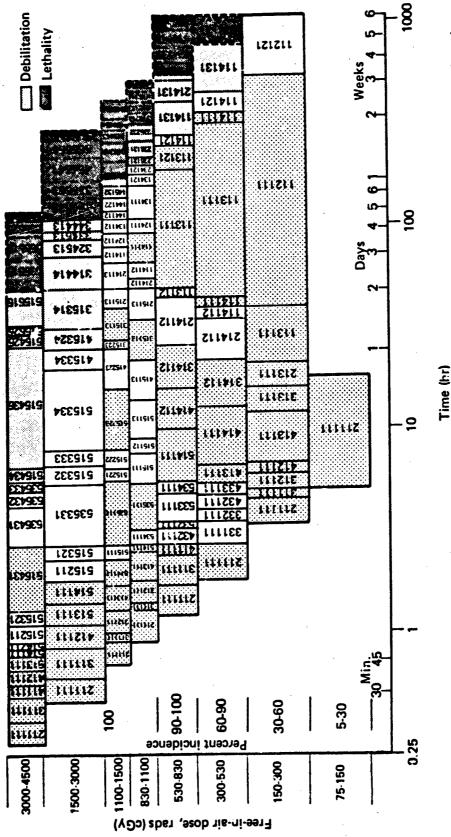
Figures H.7 through H.10 show the early LG effect on performance given in the contour plots of the same four crewmembers. This is indicated by the dipping in the performance contours at the doses and times indicated above.

の人の名の間でいった人の人を関係なっての人が大学問題ではない



gure H.l. Symptom complexes--with early LG.

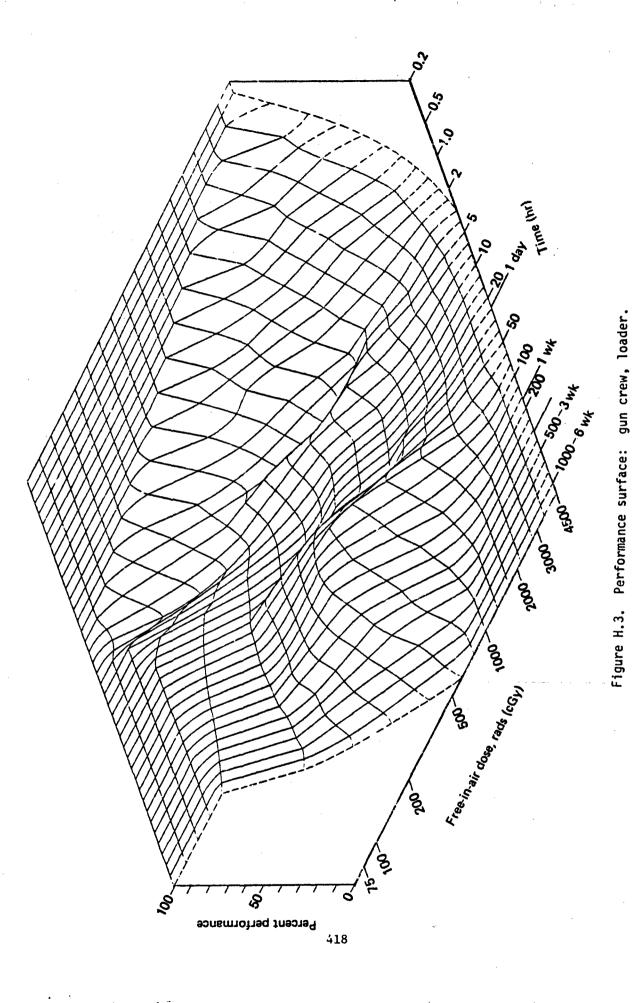
マクドル自己というのか。自己のうじかは自然などがない。 かんじかん 国際のできない 原理できならならない 国際できない ないない 大学 国際できない



Symptom complexes including those from questionnaires--with early LG. Figure H.2.

Complexes used in questionnaires

の位置が対象がは異ならののは、対象に対象が対象を関係されている。



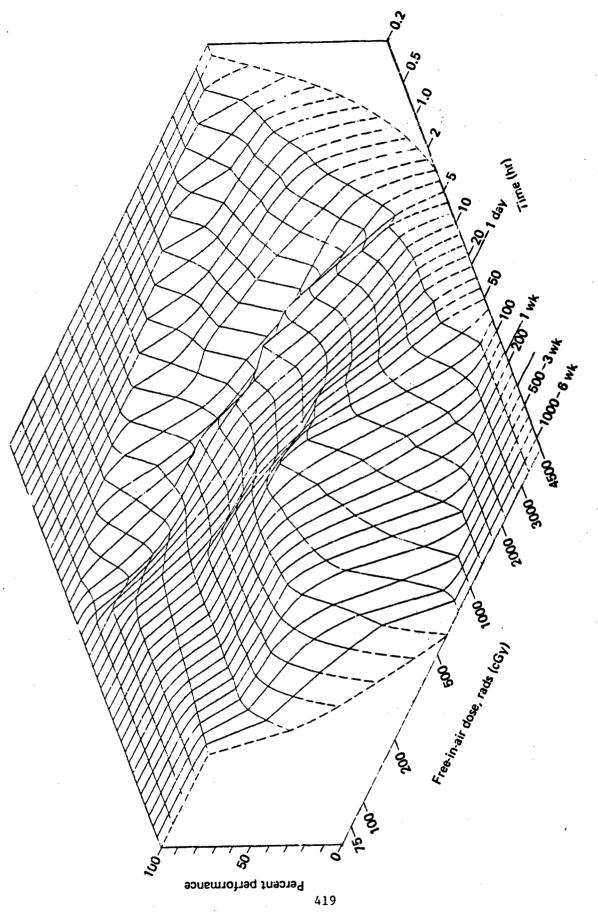


Figure H.4. Performance surface: FDC crew, computer.

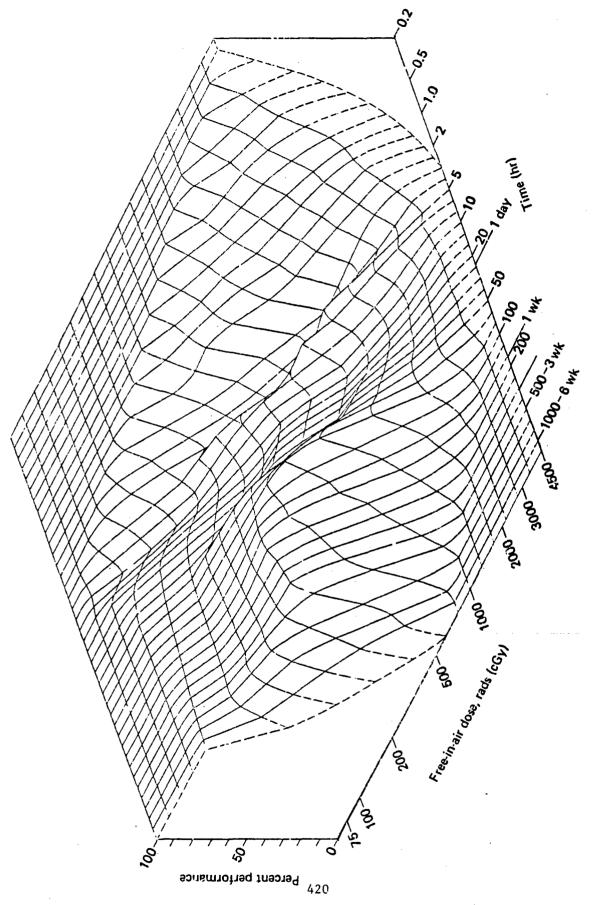
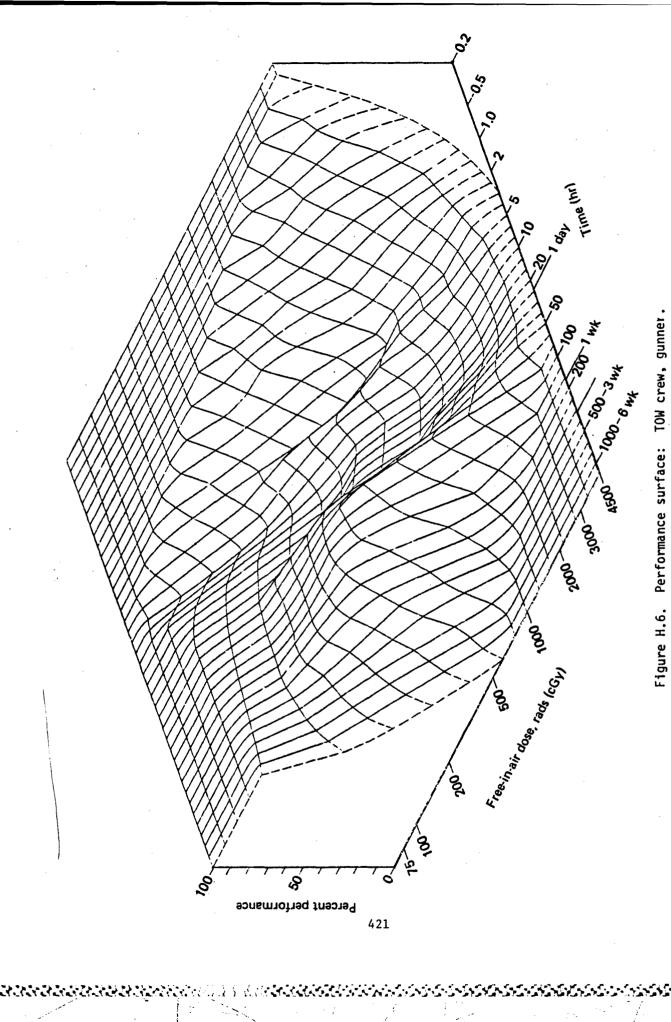


Figure H.5. Performance surface: tank crew, tank commander.



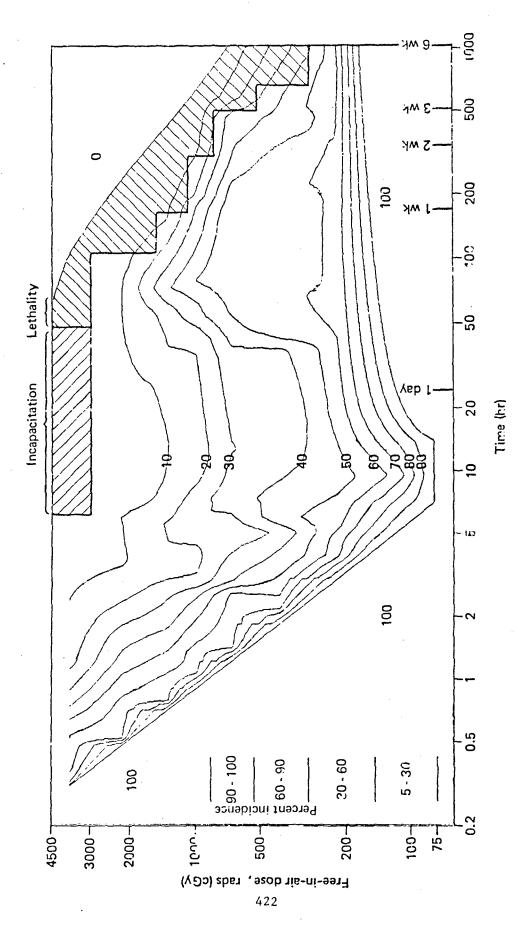
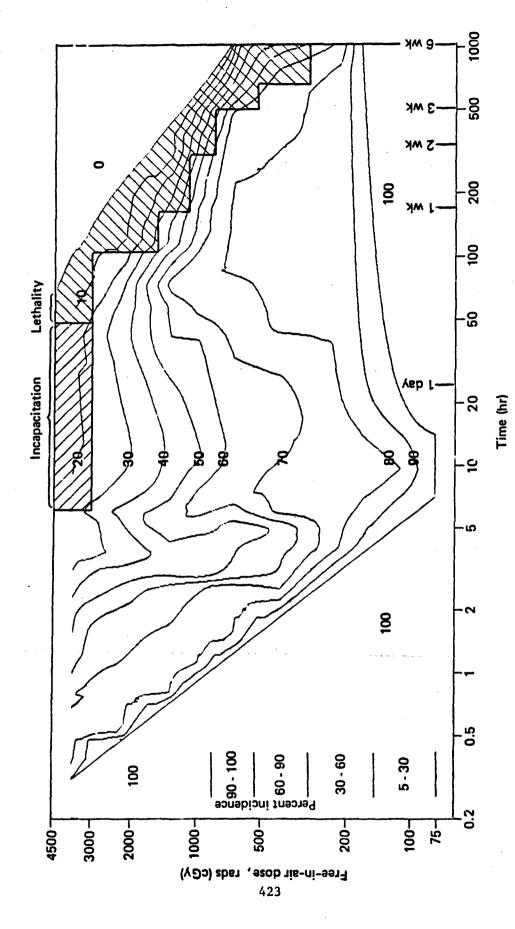
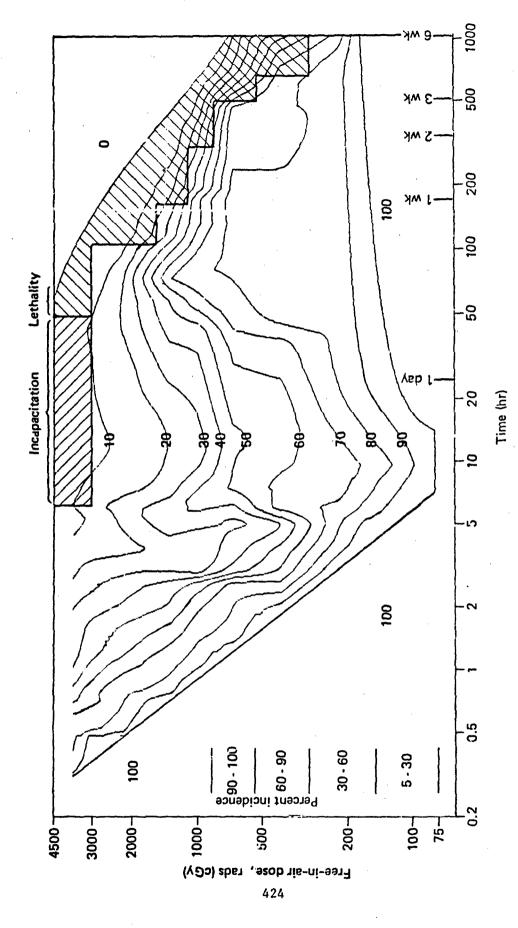


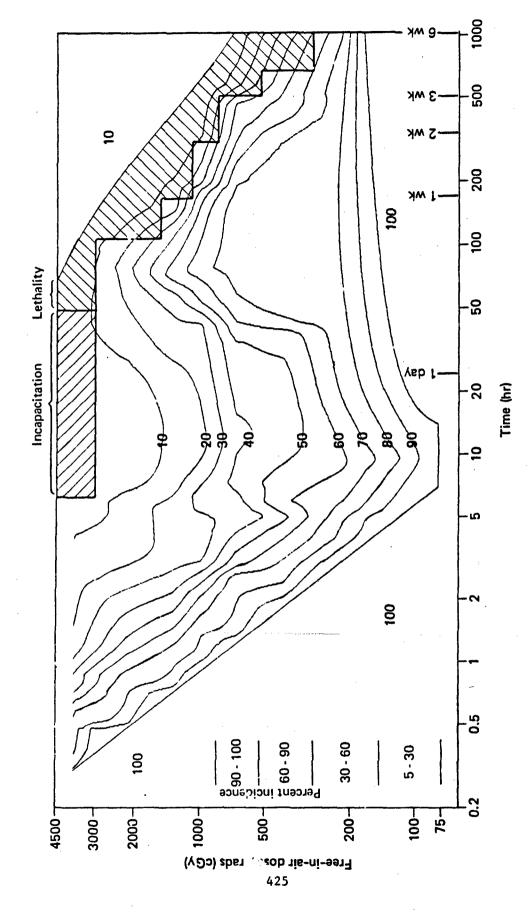
Figure H.7. Performance contours: 10 percent performance intervals, gun crew, loader.



Performance contours: 10 percent performance intervals, FDC crew, computer. Figure H.8.



Performance contours: 10 percent performance intervals, tank crew, tank commander. Figure H.9.



10 percent performance intervals, TOW crew, gunner. Performance contours: Figure H.10.



DOSE, TIME, AND CREWMEMBER PERFORMANCE INPUT VALUES FOR MAPPING

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Table I.l. Initial performance data, gun crew.

DOSE-R Rads (SYMPTOM COMPLEX		E-RANGE	TIME	CHIEF OF SECTION	GUNNER	ASSISTANT GUNNER	LOADER
75-	150	211111	5.0	18.0	9.49	0.7226	0.8320	0.8083	0.681
150-	300	211111	3.4	4.5	3.91	0.7226	0.8320	0.8083	0.6814
		311111	4.5	5.0	4.74	0.6751	U.8106	0.7665	0.6487
		312111	5.0	6.0	5.48	0.6341	0.7701	0.7403	ù.5777
		412111	0.0	6.8	6.39	0.5804	0.7432	0.7135	0.541
		413111	6.8	12.0	9.03	0.5357	0,6937	0.6583	0.4667
		313111	12.0	16.0	13.66	0.5912	0.7239	0.6880	0.503
		213111	10.0	21.0	18.33	0.5444	0.7522	0.7162	0.5399
		113111	21.0	40.0	20.98	0.6943	0.7784	0.7428	0.575
		112111	40.0	540.0	146.97	0.7314	0.8178	0.7888	0.647
		112121	540.0	1060.0	756.57	0.6568	0.7874	0.7506	0.5916
300-	530	211111	1.8	2.7	2.20	0.7226	0.8320	0.8083	0.6814
		311111	2.7	3.5	3.07	0.6751	0.8106	0.7665	0.648
		312111	3.5	3.9	3.69	0.6341	ú.77ú1	0.7403	0.57/
		412111	3.9	4.6	4.24	0.5804	U.7432	0.7135	0.541
		413111	4.6	6.6	5.51	0.5357	0.6937	0.6583	U.466
		414111	6.6	13.0	9.26	0.4904	V.6394	0.5985	0.395
		314112	13.0	22.0	16,91	0.4386	0.5694	0.5247	0.325
		214112	22.0	35.0	27.75	0.4947	0.504A	0.5582	0.3569
		114112	35.0	40.0	37.42	0.5510	0.6392	0.5912	0.393
		114111	40.0	45.0	42.43	0.6545	0.7333	0.6909	U.5016
		113111	45.0	320.0	120.00	0.6943	0.7784	0.7428	0.576
		114111	320.0	360.0	339.41	0.6545	6.7333	0.6909	0.5016
		114121	360.0	450.0	402.49	0.5712	0.6967	0.6430	0.442
		114131 134131	450.0 780.0	780.0 1080.0	592.45 917.82	0.4836 0.3106	0.6574 0.4821	0.5921 0.4108	0.3857 0.2568
530-	830	211111	1.2	. 7	1.43	0.7226	0.8320	0.8083	0.6814
J J ()	030	311111	1.7	1.7 2.4	2.02	0.6751	0.8106	0.7865	0.6487
		411111	2.4	2.7	2.55	0.6238	0.7871	0.7630	0.6146
		412111	2.7	3.3	2.96	0.5804	0.7432	0.7135	0.5415
		512111	3.3	3.5	3.37	0.5246	0.7143	0.6852	0.5050
		513111	3.5	4.8	4.10	0.4793	0.6618	0.6274	0.4304
		514111	4.8	10.0	6.93	0.4343	0.6050	0.5657	0.3568
		414112	10.0	16.0	12.65	0.3840	0.5332	0.4910	0.2445
		314112	16.0	26.0	20.40	0.4380	0.5694	0.5247	Ú.325
		214112	56.0	45.0	34.21	6.4947	0.6048	0.5582	Ü.3589
		113112	45.0	50.0	47.43	0.5953	0.6936	0.6515	0.4607
		113111	50.0	190.0	97.47	0.6943	0.7784	0.7428	0.5761
		113121	190.0	250.C	217.95	0.6149	v.7458	0.6995	0.5176
		114121	250.0	0.085	264.58	0.5712	0.6967	0.6430	0.4429
		114131	280.0	410.0	338.82	0.4830	0.6574	0.5921	0.3857
		214131	410.0	520.0	461.74	0.4276	0.6237	0.5591	0.3516
		314133	0.052	630.0	572.36	0.2000	0.3728	0.3169	0.1626
		424133	630.0	760.0	691.95	0.1216	0.2634	0.2193	0.1112
		434143	760.0	910.0	831.62	0.0633	0.1722	0.1356	0.0686
		444153	910.0	1080.0	991.36	0.0319	0.1079	0.0805	0.0416

Table I.1. Initial performance data, gun crew (Continued).

DOSE-RANGE RADS (CGY)	SYMPTOM COMPLEX	TIME	-RANGE	TIME	CHIEF OF SECTION	GUNNER	ASSISTANT CUNNER	LOADER
830- 1100	211111	0.9	1.3	1.08	0.7226	0.8320	0.8083	0.6814
	311111	1.3	1.4	1.35	0.6751	0.0106	0,7865	0.0487
	312111	1.4	1.8	1.59	0.6341	0.7791	0.7403	0.5777
	413111	1.8	2.5	5.15	0.5357	0.6937	0.6583	v.4667
	514111	2.5	3.2	2.83	0.4343	0.6050	0.5657	0.3508
	515111	3.2	7.6	4.93	0.3904	0.5452	0.5019	0.2931
	515112	7.6	9.0	8.27	0.2932	0.4358	0.3746	8u15.u
	515113	9.0	14.0	11.22	0.2118	0.3322	0.2967	0.1468
	415113	14.0	22.0	17.55	0.2519	0.3655	0.3250	0.1601
	315113	22.0	35.0	27.75	0.2968	0.4000	0.3559	0.1874
	215113	35.0	50.0	41.83	0.3460	u.4356	0.3874	6.2198
	214112	50.0	56.0	52.91	0.4947	0.6048	0.5582	0.3509
	114112	56.0	67.0	61.25	0.5510	0.6392	0.5912	0.3933
	114111	67.0	92.0	78.51	0.6545	0.7333	0.6909	0.5016
	124111	92.0	110.0	100.60	0.5680	0.6570	0.6076	0.4288
	134111	110.0	160.0	132.66	0.4771	0.5716	9.5177	0.3509
	134121	160.0	180.0	169.71	0.3905	0.5270	0.4638	0.3065
	234121	180.0	190.0	184.93	0.3386	0.4905	0.4304	0.2763
	235121	190.0	200.0	194.94	0.2992	0.4297	0.3689	0.2204
	235131	200.0	260.0	228.04	0.2309	0.3863	0.3203	0.1826
	325232	260.0	320.0	288.44	0.1730	0.2972	0.2523	0.1505
	315343	320,0	360.0	339.41	0.1130	0.2155	0.1823	0.0714
	415343	360.0	410.0	384.19	0.0930	0.1918	0.1630	0.0622
	415344	410.0	460.0	434.28	0.0622	0.1326	0.1119	0.0410
	515354	460.0	520.0	489.08	0.0359	0.0994	0.0815	0.0283
1100- 1500	211111	0.7	0.9	0.79	0.7226	0.8320	0.8083	0.6514
	311111	0.9	1.0	0.95	0.6751	0.8106	0.7865	0.6487
	312111	1.0	1.3	1.14	0.6341	0.7701	0.7403	u.5777
	413111	1.3	1.7	1.49	0.5357	0.6937	0,6583	0.4667
	514111	1.7	2.3	1.98	0.4343	U.6050	0.5657	0.3588
	515111	2.3	5.3	3.49	0.3904	0.5452	0.5019	0.2931
	515221	5.3	5.7	5.50	0.2965	0.4572	0.4162	0.2121
	515222	5.7	8.0	6.75	0.2144	0.3517	0.3157	0.1478
	515223	8.0	16.0	11.31	0.1502	0.2590	0.2299	0.1005
	415223	16.0	25.0	20.00	0.1814	0.2860	0.2546	0.1145
	315223	25.0	27.0	25.98	0.2174	0.3189	0.2811	0.1303
	315113	27.0	40.0	32.66	0.2968	0.4000	0.3559	0.1874
	215113	40.0	50.0	44.72	0.3460	0.4356	0.387;	0.2108
	214113	50.0	66.0	57.45	0.3881	0.4965	0,4498	0.2650
	114112	66.0	80.0	72.66	0.5510	0.6392	0.5912	0.3933
	124112	80.0	95.0	85.79	C.4600	g.5524	0.5005	0.3259
	134112	92.0	110.0	100.60	0.3715	0.4622	0.4098	0.2650
	144112	110.0	120.0	114.89	0.2909	0.3744	0.3249	0.2119
	144122	120.0	140.0	124.61	0.2236	0.3333	0.2795	0.1752
	145132	140.0	160.0	149.67	0. 446	0.2463	0.1947	0.1105
	245232	160.0	510.0	183.30	0.1121	0.1919	0.1565	0.0311
	345342	210.0	260.0	233.67	0.0682	0.1260	0.1029	0.0472
	445443	260.0	300.0	279.29	0.0311	0.0632	0.0539	0.0221
	454454	300.0	340.0	319.37	0.0120	0.0313	0.0259	0.0115 0.0048
	545454	34ú.0	420.0	377.89	0.0115	0.0304	0.0253	J. U V 70

Table I.1. Initial performance data, gun crew (Concluded).

								
DOSE-RANGE	_			_	CHIEF OF		ASSISTANT	
RADS (CGY)	COMPLE	X TIM	IE-RANGE	TIME	SECTION	GUNNER	GUNNER	LOADER
1500- 3000	211111	0.4	0.6	0.52	0.7226	0.8320	0.8083	A 4010
	311111	0.6	-, -		0.6751	0.8106	0.7665	0.6814 0.6487
	412111	0.8		0.96	0.5804	0.7432	0.7135	0.5415
	513111	1.1		1.24	0.4793	V.6618	0.6274	0.4304
	514111	1.4			0.4343	0.6050	0.5657	0.4304
	515211	1.8		2.03	0.3748	0.5020	0.4694	0.2543
	515321	2.3			0.2824	U.4146	0.3650	U.1813
	515331	2.7		3.62	0.2171	0.3717	0.3353	0.1489
	515332	5.4		5.97	0.1523	0.2759	0.2461	0.1012
	515333	6.6		7.27	0.1042	v.1971	0.1744	U. U677
	515334	8.0		12.65	0.0701	0.1366	0.1202	0.0447
	415334	20.0	24.0	21.91	0.0863	0.1547	0.1352	0.0513
	415324	24.0	32.0	27.71	0.1184	0.1798	0.1625	0.0641
•	315314	32.0	50.0	40.00	0.1932	0.2330	0.2161	0.0913
	314414	50.0	72.0	60.00	0.2118	0.2461	0.2383	Ú.10U4
	324513	72.0	86.0	76.69	0.2123	8855.0	0.2273	0.0960
	334513	86.0	96.0	90.06	0.1576	0.1713	0.1693	0.0734
	344413	96.0	110.0	102.76	0.1218	0.1461	0.1386	0.0670
	354523	110.0	140.0	124.10	0.0596	0.0773	0.0731	0.0336
	35553 3	140.0	170.0	154.27	0.0358	0.0519	0.0469	0.0199
	455543	170.0	220.0	193.39	0.0204	0.0380	0.0335	0.0137
	555554	220.0	270.0	243.72	0.000	0.0000	0.0000	0,0000
	\$55555	270.0	300.0	264.61	0.0000	0.0000	0.0000	0.0000
3000- 4500	211111	0.3	0.4	0.32	0.7226	0.8320	0.8083	0.6814
	311111	Ú.4	0.5	0.42	0.6751	0.8106	0.7865	0.6487
	411111	0.5	0.6	0.52	0.6238	0.7871	0.7630	U.6146
	412111	0.6	0.7	0.61	0.5804	0.7432	0.7135	0.5415
	513111	0.7	0,8	0.71	0.4793	0.6618	0.6274	0.4304
	51 1111	0.8	0.5	0.80	0.4343	0.6050	0.5657	0.3588
	514211	0.8	0.9	0.87	0.4181	0.5630	0.5335	0.3152
	515211	0.9	1.1	0.99	0.3748	0.5020	0.4694	0.2543
	515321	1.1	1.3	1.20	0.2829	0.4146	0.3850	0.1813
	515431	1.3	2.7	1.87	0.2061	0.3322	0.3070	0.1257
	535431	2.7	4.2	3.37	0.1111	0.1944	0.1754	0.0741
	535432	4.2	5.0	4.58	6.0749	0.1345	0.1210	0.0490
	535433	5.0	5,6	5.29	0.0498	0.0910	0.0818	0.0321
	515434	5.6	6.6	6.08	0.0659	0.1174	0.1071	0.0370
	515435	9.0	26.0	13.10	0.0437	0.0789	0.0720	0.0242
	515425	50.0	30.0	27.93	0.0610	0.0930	0.0879	0.0304
	515525	30.0	33.0	31.46	0.0573	0.0794	0.0780	0.0251
	515515	33.0	55,0	42.60	0.0796	0.0936	0.0950	0.0316
	535515	55.0	70.0	62.05	0.0400	0.0477	0.0480	U.U178
	555515	70.0	91.0	79.81	0.0197	0.6237	0.0236	0.0100
	555525	91.0	110.0	100.05	9.0139	U.0199	0.0191	Ú. U079
	555535	110.0	120.0	114.89	0.0000	0.0000	0.0000	0.0000
	-							

Table I.2. Initial performance data, FDC.

						FIRE	HORIZONTAL	L
DOSE-R	ANGE	SYMPTOM				DIRECTION	CONTROL	
RADS (COMPLEX	TIM	E-RANGE	TIME	UFFICEK	OPERATOR	COMPUTER
75-	150	211111	5.0	18.0	9,49	0.8168	0.7479	0.8076
150-	300	211111	3.4	4.5	3.91	0.8168	U.7479	0.8076
•		311111	4.5	5.0	4.74	0.7800	0.7105	0.7811
		312111	5.0	6.0	5.48	0.7678	0.6900	0.7682
		412111	6.0	6.8	6.39	0.7244	0.6480	0.7381
		413111	6.5	12.0	9.03	0.7102	0.6254	0.7236
		313111	12.0	16.0	13.86	0.7551	0.6687	0.7548
		213111	16.0	21.0	18.33	0.7950	0.7093	0.7836
		113111	21.0	40.0	26.98	0.8299	U.7468	0.8099
		112111	40.0	540.0	146.97	0.8395	0.7648	0.8210
		112121		1060.0	756.57	0.8043	¥.7469	0.8131
300-	530	211111	1.8	2.7	2.20	0.8168	4.7479	0.8076
		311111	2.7	3.5	3.07	0.7800	0.7105	0.7811
		312111	3.5	3.9	3.69	0.7678	(: . 6900	0.7682
		412111	3.9	4.6	4.24	0.7244	U.648N	0.7381
		413111	4.6	6.6	5.51	0.7102	0.6254	0.7236
		414111	0.6	13.0	4.26	0,6957	0.0023	0.7086
		314112	15.0	22.0	16.91	0.6391	0.5705	0.6679
		214112	55.0	35.0	27.75	0.6902	0.0162	0.7029
		114112	35.0	40.0	37.42	0.7370	0.5599	0,7356
		114111	40.0	45.0	42.43	0.8198	U.7279	0.7983
		113111	45.0	320.0	150.00	0.8299	U.7468	0.8099
		114111	320.0	360.0	339.41	0.8198	0.7279	0.7983
		114121	360.0	450.0	402.49	0.7814	0.7082	0.7696
		114131	450.0	780.0	592.45	0.7375	0.6877	0.7807
		134131	780.0	1080.0	917.82	0.4958	0.5249	0.6045
530-	830	211111	1.2	1.7	1.43	0.8168	0.7479	0.8076
		311111	1.7	2.4	2.02	0.7800	0.7105	0.7811
		411111	2.4	2.7	4.55	0.7381	0.6700	0.7521
		412111	2.7	3.3	2.96	0.7244	0.6480	0.7381
		512111	3.3	3.5	3,37	0.6763	0.6037	0.7055
		513111	3.5	4.8	4.10	0.6609	0.5AU1	0.6900
		514111	4.8	10.0	6.93	0.6451	0.5561	0.6740
		414112	10.0	16.0	12,65	0.5847	0.5235	0.6310
		314112	16.0	26.0	20.40	0.6391	0.5705	0.6679
		214112	26.0	45.0	34.21	0.6902	0.6162	0.7029 0.7497
		113112	45.0	50.0	47.43	0.7503	0.6815	0.8099
		113111	50.0	190.0	97.47	0.8299	0.7468	
		113121	190.0	250.0	217.95	0.7931 0.7814	0.7279 U.7082	0.8016 0.7896
		114121	250.0	280.0		0.7375	0.7082 0.6877	0.7897
		114131	280.0	410.0 520.0	336.82 461.74	0.6907	0.0456	0.7516
		214131 314133	410.0	630.0	572.36	0.4025	0.4423	0.5599
		424133	630.0	760.0	691.95	0.2406	0.3173	0.4148
		434143	760.0	910.0	831.62	0.1484	v.2300	0.3058
		444153		1080.0	991.36	0.0641	6.1610	0.2149
		444133	710.0	*000*0	776.30	0.0041	A. 1010	110-17

Table I.2. Initial performance data, FDC (Continued).

				استناست هي	FIRE HORIZONTAL			
005E-B.MCE	SYMPTOM				DIRECTION	CONTROL		
RADS (CGY)	COMPLEX	TIME	-RANGE	TIME	OFFICER	OPERATOR	COMPUTE	
830- 1100	211111	0.9	1.3	1.08	0.8168	0.7479	0.8076	
930- 1100	311111	1.3	1.4	1.35	0.7800	0.7105	0.7811	
		1.4	1.8	1.59	0.7676	0.0900	0.7682	
	312111	1.8	2.5	2,12	0.7102	U.6254	0.7236	
	413111			2.83	0.6451	0.5561	0.6740	
	514111	2.5	3.2	4.93	0.6290	0.5319	0.6576	
	515111	3.2	7.6	6.27	0.5108	0.4519	0.5745	
	515112	7.6	9.0		0.3913	0.3743	0.4871	
•	515113	9.0	14.0	11.22	0.4471	0.4196	0.5276	
	415113	14.0	55.0	17.55		ŷ.4664	0.5678	
	315113	22.0	35.0	27.75	0.5043		0.6071	
	215113	35.0	50.0	41.83	0.5613	0.5137	0.7029	
	214112	50.0	56.0	52.91	0.6902	0.6162	0.7356	
	114112	56.0	67.0	61.25	0.7370	0.6599		
	11 (11	67.0	92.0	76.51	0.8190	0.7279	0.7983	
	124111	92.0	110.0	100.60	0.7291	U.6545	0.7217	
	134111	110.0	160.0	132.66	0.6142	0.5730	0.6295	
	134121	160.0	180.0	169.71	0.555ø	0.5491	0.6170	
	234121	180.0	190.0	184.93	0.4987	0.5018	0.5780	
	235121	190.0	200.0	194.94	0.4813	0.4774	0.5599	
	235131	200.0	260.0	226.04	0.4217	0.4532	0.5469	
		260.0	320.0	288.44	0.3377	0.3804	0.4705	
	325232		360.0	339.41	0.2605	0.3328	0.4219	
	315343	320.0	410.0	384.19	0.2188	0.2921	0.3829	
	415343	360.0		434.28	0.1471	0.2304	0.3037	
	415344 515354	410.0 460.U	460.0 520.0	489.08	0.0973	0.1835	0.5605	
	0.000	_				0.7479	0.8076	
1100- 1500	211111	0.7	0.9	0.79		0.7105	0.7611	
	311111	0.9	1.0	0.95			0.7682	
	312111	1.0	1.3	1.14	0.7678	0.6900	0.7236	
	413111	1.3	1.7	1.49	0.7102	0.6254	0.6740	
	514111	1.7	2.3	1.98		0.5561		
	515111	2.3	5.3	3.49		0.5319	0.6576	
	515221	5.3	5.7	5.50		0.4740	0.5950	
	515222	5.7	8.0	6.75	0.4094	0.3954	0.5082	
	515223	8.0	16.0	11.31	0.2992	0.3217	0.4208	
	415223	10.0	25.0	50.00	0.3493	0.3644	0.4008	
	315223	25.0	27.0	25,98	0.4031	U.4094	0.5013	
	315113	27.0	40.0	32.86	0.5043	0.4664	0.5678	
	215113	40.0	50.0	44.72		0.5137	0,6071	
	214113	50.0	66.0	57.45		0.5381	0.6246	
		60.0	40.0	72.66		0.6599	0.735	
	114112		92.0	85.79		3.5789	0.6458	
	124112	80.0		100.60		U.4933	0.5443	
	134112	92.0	110.0	114.69		0.4062	0.4391	
	144112	110.0	120.0			0.3849	0.4261	
	144122	120.0	140.0	129,61		0.3399	0.3954	
	145132	140.0	160.0	149,67		0.2713	0.3097	
	245232	160.0	210.0	163,30			0.2259	
	345342	210.0	560.0	233.67		0.1964	0.1234	
	445443	260.0	300.0	279.29		0.1136		
	454454	300.0	340.0	319.37		0.0618	0.0621	
	545454	340.0	420.0	377.89	0.0185	0.0652	0.073	

Table I.2. Initial performance data, FDC (Concluded).

					FIRE	ORIZONTAL	
DOSE-RANGE	SYMPTOM				DIRECTION	CONTROL	
RADS (CGY)	COMPLEX	TIME	-RANGE	TIME	OFFICER	OPERATOR	COMPUTER
1500- 3000	211111	0.4	0,6	0.52	0.8166	0.7479	0.8076
	311111	0.0	0.8	0.71	0.7800	0.7105	0.7811
	412111	0.8	1.1	0.96	0.7244	0.6480	0.7381
	513111	1.1	1.4	1.24	0.6609	0.5801	0.6900
	514111	1.4	1.8	1.59	0.6451	0.5561	0.6740
	515211	1.8	2.3	2.03	0.5888	0.4963	0.6077
	515321	2.3	2.7	2.49	0.4674	0.4407	0.5425
	515331	2.1	5.4	3.82	0.4276	v.4169	0.5293
	515332	5.4	6.6	5.97	0.3151	0.3415	0.4416
	515333	6.6	8.0	7.27	0.2208	0.2734	0.3574
	515334	8.0	20.0	12.65	0.1486	0.2144	0.2811
	415334	20.0	24.0	21.91	0.1800	0.2481	0.3150
	415324	24.0	32.0	27.71	0.2184	0.2667	0.3266
	315314	32.0	50.0	40.00	0.3090	0.5264	0.3755
	314414	50.0	72.0	60.00	0.2883	0.3184	0.3431
	324513	72.0	86.0	78.69	0.2474	0.2850	0.2620
	334513	86.0	96.0	90.86	0.1626	0.2202	0.2046
	344413	96.0	110.0	102.76	0.1199	0.1862	0.1726
	354523	110.0	140.0	124.10	0.0508	0.1139	0.0946
	355533	140.0	170.0	154.27	0.0377	u.0957	0.0845
	455543	170.0	0.055	193.39	0.0239	0.0735	0.0693
	555554	550.0	270.0	243.72	0.0000	0.0000	0.0000
	555555	270.6	300.0	284.61	0.0000	6.0000	0.0000
3000- 4500	211111	0.3	0.4	0.32	0.8168	0.7479	0.8076
	311111	0.4	0.5	0.42	0.7800	0.7105	0.7811
	411111	0.5	0.6	0.52	0.7381	0.6700	0.7521
	412111	0.6	0.7	0.61	0.7244	0.6480	0.7381
	513111	0.7	0.8	ü.71	0.6609	0.5801	0.6900
	514111	0.8	0.8	0.80	0.6451	0.5561	0.6740
	514211	0.8	0.9	0.87	0.6056	0.5227	0.6252
	515211	0.9	1.1	0.99	0.5486	0.4983	0.6077
	515321	1.1	1.3	1.20	0.48.4	0.4407	0.5425
	515431	1.3	2.7	1.87	0.3870	U.3846	0.4757
	535431	2.7	4.2	3.37	0.1810	0.2387	0.2803
	535432	4.2	5.0	4.58	0.1198	0.1853	0.2150
	535433	5.0	5.6	5.29	0.0773	0.1417	0.1615
	515434	5.6	6.6	6.08	0.1285	0.1927	0.2398
	515435	6.6	26.0	13.10	0.0833	0.1476	0.1816
	515425	26.0	30.0	27.93	0.1036	0.1602	0.1896
	515525	30.0	33.0	31.46	0.0889	0.1430	0.1588
	515515	33.0	55.0	42.60	0.1105	0.1553	0.1660
	535515	55.0	70.0	62.05	0.0417	0.0845	0.0787
	555515	70.0	91.0	79.81	0.0150	0.0442	0.0354
	555525	91.0	110.0	100.05	0.0118	0.0403	0.0336
	555535	110.0	120.0	114.69	0.0000	0.000	0.0000

Table I.3. Initial performance data, tank crew.

DOSE-	RANGE	SYMPTOM				TANK			
RADS		COMPLEX	TIM	E-RANGE	TIME	COMMANDER	GUNNER	LUADER	DRIVE
75-	150	511111	5.0	18.0	9.49	0.8447	0.8853	0.8092	G.874
150-	300	211111	3.4	4.5	3.91	0.8447	0.8853	0.8092	0.0744
		311111	4.5	5.0	4.74	0.2004	0.8501	0.7719	0.849
		312111	5.0	6.0	5.48	0.7597	.0.8252	0.7148	U.8054
		412111	6.0	6.8	6.39	0.6995	0.7762	0.6667	0.770
		413111	6.8	12.0	9.03	9.6477	U.7428	0.5969	0.711
		313111	12.0	16.0	13.86	0.7137	u.7971	0.6498	0.752
		213111	16.0	21.0	18.33	0.7717	0.8424	0.6992	0.789
		113111	21.0	40.0	28.98	0.8209	u.6791	0.7445	0.822
		112111	40.0	540.0	146.97	0.8532	0.8973	0.7974	0.863
		112121	540.0	1060.0	756.57	0.8477	0.4005	0.7964	0.8617
300-	530	211111	1.8	2.7	2.20	0.8447	0.8853	0.8092	0.8744
		311111	2.7	3.5	3.07	0.8004	0.8501	0.7719	0.849
		312111	3.5	3.9	3.69	0.7597	0.8252	0.7148	0.605
		412111	3.9	4.6	4.24	0.6999	0.7762	0.6667	0.770
		413111	4.0	6.6	5,51	0.6477	ú.7428	0.5969	6.711
		414111	6.0	13.0	9.26	0.5917	0.7062	0.5230	0.643
		314112	13.0	22.0	16.91	0.5495	0.6548	0.4495	0.589
		214112	22.0	35.0	27.75	0.6232	0.7207	0.5057	0.639
		114112	35.0	40.0	37.42	0.6916	0.7784	0.5617	0.686
		114111	40.0	45.0	42.43	0.7632	0.8583	0.6832	0.172
		113111	45.0	320.0	120.00	0.8209	0.8791	0.7445	0.822
		114111	320.0	360.0	339.41	0.7832	0.8583	0.6632	0.7720
		114121	360.0	450.0	402.49	0.7757	0.8621	0.6819	0.768
		114131 134131	450.0 780.0	780.0 1080.0	592.45 917.82	0.768U 0.5495	0.6659 0.6660	0.6806 0.4647	U_546
		*34131	100.0	1000.0	-	•			. •
530-	830	211111	1.2	1.7	1.43	0.8447	0.8853	0.8092	0.8744
		311111	1.7	2.4	2.02	0.8004	0.8501	0.7719	0.849
		411111	2.4	2.7	2.55	0.7473	v.6065	0.7290	0.020
		412111	2.7	3.3	2.96	0.6999	0.7762	0.6667	0.770
		512111	3.3	3,5	3.37	0.6323	0.7183	0.6148	0.730
		513111	3.5	4.8	4.10	0.5755	0.6797	0.5417	0.665
		514111	4.8	10.0	6.93	0.5166	0.6385	0.4667	0.593
		414112	10.0	16.0	12,65	0.4735	0.5823	0.3945	v.537
		314112	16.0	26.0	20.40	0.5495	0.6548	0.4495	0.589
		214112	50.0	45.0	34.21	0.6232	0.7207	0.5057	0.6394
		113112	45.0	50.0	47.43	0.7399	0.8084	0.6339	0.7489
		113111	50.0	190.0	97.47	0.8209	0.8791	0.7445	0.822
		113121	190.0	250.0	217.95	0.8143	0.8825	0.7433	0.6200
		114121	250.0	0.085	264.58	0.7757	0.8621	0.6819	0.7704
		114131	280.0	410.0	338.82	0.7680	0.8659	0.6006	0.7682
		214131	410.0	520.0	461.74	0.7094	0.5260	0.6297	0.7286
		314133	520.0	630.0	572.36	0.4095	0.5398	0.3239	0.4744
		424133	630.0	760.0	691.95	0.2369	0.3249	0.1962	
		434143	760.0	910.0	831.62	0.1526	0.2172	0.1341	0.2076
		444153	910.0	1080.0	991.36	0.0949	0.1379	0.0895	0.134

Table I.3. Initial performance data, tank crew (Continued).

DOSE-RANGE RADS (CGY)	SYMPTOM COMPLEX	TIME	-RANGE	TIME	TANK COMMANDER	GUNNER	LOADER	DRIVER
830- 1190	211111	0.9	1.3	1.08	0.8447	0.8853	0.8092	0.5744
• • • • • • • • • • • • • • • • • • • •	211111	1.3	1.4	1.35	0.8004	0.8501	0.7719	U.6494
	312111	1.4	1.8	1.59	0.7597	0.8252	0.7148	J.8054
	413111	1.8	2.5	2.12	0.6477	0.7428	0.5969	6.7110
	514111	2.5	3.2	2.83	0.5166	0.6385	0.4667	0.5938
	515111	3.2	7.6	4.93	0.4573	0.5952	0,3931	0.517e
	5151:2	7.6	9.0	6.27	0.3434	0.4603	0.2780	0.4087
	515113	9.0	14.0	11.22	0.2450	0.3309	0.1862	0.3062
	415113	14.0	22.0	17.55	0.3056	0.4023	0.2228	0.3548
	315113	22.0	35. 0	27.75	0.3737	0.4780	0.2643	0.4644
	215113	35.0	50.0	41.83	0.4473	U.5548	0.3104	0.4560
	214112	50.0	56.0	52.91	0.6232	0.7207	0.5057	0.6394
	114112	56.0	37.0	61.25	0.6910	0.7784	0.5617	0.6864
	114111	67.0	92.0	78.51	0.7632	0.8583	0.6032	U.1726
	124111	92.0	110.0	100.60	0.6868	0.7717	0.5793	0.6718
	134111	110.0	160.0	132.66	0.5711	0.6536	0.4678	U.5521
	134121	160.0	180.0	169.71	0.5603	0.6508	0.4663	0.5491
	234121	180.0	190.0	184.93	0.4845	0.5888	0.4108	0.4915
	235121	190.0	200.0	194,94	0.4250	0.5438	0.3404	0.4199
	235131	200.0	500.0	226.04	0.4147	0.5518	0.3391	0.4169
	325232	260.0	320.0	285.44	0.3089	0.4319	0.2412	0.3348
	315343	320.0	360.0	339.41	0.2677	0.3975	0.1970	0.3113
	415343	360.0	410.0	384.19	0.2124	0.3265	0.1637	0.2680
	415344	410.0	460.0	434.23	0.1434	0.2195	0.1042	0.1909
	515354	460.0	520.0	489.08	0.1056	0.1759	0.0045	0.1508
1100- 1500	211111	0.7	0.9	0.79	0.8447	0.8853	0.8092	0.6744
	311111	0.9	1.0	0.95	0.8004	0.6501	0.7719	0.8494
	312111	1.0	. 1.3	1.14	0.7597	0.8252	0.7148	U.8054
	413111	1.3	1.7	1.49	0.6477	0.7428	0.5969	0.7110
	514111	1.7	2.3	1.98	0.5166	v.6385	0.4667	U.593A
	515111	2.3	5.3	3.49	0.4573	0.5952	0.3931	U.5176
	515221	5.3	5.7	5.50	0.4026	0.5512	0.3494	0.4683
	515222	5.7	8.0	6.75	0.2950	0.4160	0.2419	0.3621
	515223	8.0	16.0	11.31	0.2061	0.2923	0.1594	0.2678
	415223	10.0	25.0	20.00	0.2604	4.3598	0.1920	0.3110
	315223	25.0	27.0	25.98	0.3232	0.4334	0.2294	579د.0
	315113	27.0	40.0	36.06	0.3737	0.4780	0.2543	0.4044
	215113	40.0	50.0	44.72	0.4473	0.5548	0.3104	0,4560
	214113	50.0	66.0	57,45	0.5035	0.5995	0.3781	0.5332
	114112	60.0	80.0	72.66	0.6916	0.7784	0.5617	0,6864
	124112	80.0	65°U	85.79	0.5765	0.6622	0.4500	0.5687
	134112	92.0	110.0	100.60	0.4525	0.5225	0.3431	0.4427
	144112	110.0	120.0	114.69	0.3341	0.5792	0.2501	0.3236
	144122	120.0	140.0	129.61	0.3244	0.3868	0.2489	0.3209
	145132	140.0	160.0	144.67	0.2659	0.3516	0.1960	0.2552
	245232	160.0	210.0	183.30	0.1826	0.2437	0.1397	0.1874
	34534?	0:015	500.0	233.67	0.1164	0.1652	0.0970	0.1329
	445443	260.0	300.0		0.0486	0.0638	0.040a	0.0624
	454454	300.0	340.0	319.57	0.0225	0.0267	0.0212	0.0336
	545454	340.0	420.0	377.09	0.0216	0.0291	0.0195	0.0351

Table I.3. Initial performance data, tank crew (Concluded).

DOSE-RANGE RADS (CGY)	SYMPTOM COMPLEX		E-RANGE	TIME	TANK COMMANDER	GUNNER	LUADER	DRIVER
1500- 3000	211111	0.4	0.6	0.52	0.8447	0.8853	0.8092	0.8744
	311111	0.6	0.8	ũ.71	0.8004	0.6501	0.7719	0.0494
	412111	0.8	1.1	0.96	0.6999	0.7762	0.6667	J.7702
	513111	1.1	1.4	1.24	0.5755	0.6797	0.5417	0.0658
	514111	1.4	1.8	1.59	0.5166	0.6385	0.4667	0.5938
	515211	1.6	2.3	2.03	0.4132	0.5432	0.3508	0.4714
	515321	2.3	2.7	2.49	0.3604	0.4983	0.3094	0.4227
	515331	2.7	5.4	3.62	0.3503	0.5064	0.3081	0.4196
	515332	5.4	6.6	5.97	0.2508	0.3730	5602.0	0.31/8
	515333	0.6	8.0	7.27	0.1720	0.2565	0.1359	0.2309
	515334	8.0	20.0	12.65	0.1142	ú.1667	0.0854	0.1621
	415334	20.0	24.0	21.91	0.1488	0.2140	0.1046	U.1928
	415324	24.0	32.0	27.71	0.1545	0.2086	0.1054	0.1947
	315314	32.0	50.0	40.00	0.2056	0.2578	0.1293	0.2321
	314414	50.0	72.0	60.00	0.2153	0.2524	0.1433	0.2550
	324513	72.0	86.0	78.69	0.1833	0.2081	0.1304	0.2101
	334513	86.0	96.0	90.86	0.1199	U.1279	0.0874	0.1381
	344413	96.0	110.0	102.76	0.0900	0.0919	0.0682	0.1040
	354523	110.0	140.0	124.10	0.0456	0.0451	0.0373	0.0543
	355533	140.6	170.0	154.27	0.0350	0.0390	0.0277	ü. U4Ŭ0
	455543	170.0	220.0	193.39	0.0250	0.0299	0.0221	v.0322
	555554	220.0	270.0	243.72	0.0000	0.0000	0.0000	0.0000
	555555	270.0	300.0	284.61	0.0000	0.0000	0.0000	0.0000
3000- 4500	211111	0.3	0.4	9.32	0.8447	0.8853	0.8092	0.8744
	311111	0.4	0.5	0.42	0.8004	0.8501	0.7719	0.8494
	411111	0.5		0.52	0.7473	0.8065	0.7298	0.8204
	412111	0.6	0.7	0.61	0.6999	4.7762	0.6667	0.7702
	513111	0.7	0.8	0.71	0.5755	0.6797	0.5417	0.6658
	514111	0.8	5.0	0.80	0.5166	0.6385	0.4667	0.5938
	514211	0.8	0.9	0.87	0.4718	0.5883	0.4219	0.5466
	515211	0.9	1.1	0.99	0.4132	0.5432	0.3508	0.4714
	515321	1.1	1.3	1.20	0.3604	0.4983	0.3094	0.4227
	515431	1.3	2.7	1.87	0.3107	0.4535	0.2708	0.3754
	535431	2.7	4.2	3.37	0.1425	0.2054	0.1315	0.1740
	535432	4.2	5.0	4.58	0.0935	0.1304	0.0825	0.1232
	535433	5.0	5.6	5.29	0.0602	9.0800	0.0507	0.0830
	515434	5.6	6.6	6.08	0.0973	0.1393	0.0723	0.1365
*	515435	6.6	26.0	13.10	0.0627	0.0858	0.0443	0.0939
	515125	26.0	30.0	27.93	0.0653	0.0833	0.0445	0.0949
•	315525	30.0	33.0	31.46	0.0552	0.0645	0.0374	0.0802
	515515	33.0	55.0	42.60	0.0575	0.0665	0.0376	0.0811
	535515	55.0	70.0	62.05	0.0220	0.0217	0.0157	0.0310
	555515	70.0	91.0	79.81	0.0082	0.0069	0.0065	0.0115
	555525	91.0	110.0	100.05	0.0079	U.0007	0.0064	
	555535	110.0	120.0	114.89		0.0071		0.0113
			154.0	117,07	0.0000	V.VUU	0.0000	0.0000

Table I.4. Initial performance data, TCW crew.

DOSE-R Rads (SYMPTOM COMPLEX		E-RANGE	TIME	SQUAD LEADER	GUNNER	DRIVER	LOADE
75-	150	211111	5.0	18.0	9.49	0.8714	0.8306	0.9456	0.882
150-	300	21:111	3.4	4.5	3.91	0.8714	0.8306	0.9456	0_8821
•		311111	4.5	5.0	4.74	0.8435	0.7937	0.9315	0.853
		312111	5.0	6.0	5.48	0.7884	0.7251	0.8932	0.7759
		412111	6.9	6.8	6.39	0.7477	0.6742	0.8676	0.7238
		413111	6.8	12.0	9.03	0.6721	0.5865	0.8012	0.6146
		313111	12.0	16.0	13.66	0.7205	0.6439	0.8373	0.6718
		213111	16.0	21.0	18.33	0.7045	0.6475	0.8579	0.7247
		113111	21.0	40.0	20.98	0.8030	0.7461	0.8935	0.771
		11211!	40.0	540.0	146.97	0.8550	0.8108	0.9317	0.8514
		112121		1060.0	756.57	0.7987	0.7418	0.8913	0.1944
300-	530	211111	1.8	2.7	2.20	0.8714	0.8306	0.9456	0.882.
		311111	2.7	3.5	3,07	0.8435	0.7937	0.9315	0.053
		312111	3.5	3.9	3.69	0.7884	0.7251	0.8932	0.7739
		412111	3.9	4.6	4.24	0.747?	U.6742	0.8676	0.7288
		413111	4.6	6.6	5.51	0.6721	0.5865	0.8012	0.614
		414111	6.6	13.0	9.26	0.5864	0.4930	0.7125	0.4854
		314112	13.0	22.0	16.91	0.5177	J. 4334	0.6317	0.3943
		214112	22.0	35.0	27.75	0.5744	0.4937	0.6065	0.4556
		114112	35.0	40.0	37.42	0.6293	0.5542	0.7366	V. 5163
		114111	40.0	45.0	42.43	0.7382	0.6653	0.8376	0.0572
		113111	45.0	320.0	120.00	0.8030	0.7461	0,8935	0.7719
		114111	320.0	360.0	339.41	0.7382	v.6683	0.8376	0.6678
		114121	360.0	450.0	402.49	0.6549	0.5746	0.7562	0.5756
		114131	450.0	760.0	592.45	0.5608	U.4751	0.6509	0.47 15
		134131	780.0	1080.0	917.82	0.4272	0.3620	0.5061	V.3505
530-	830	211111	1.2	1.7	1.45	0.8714	0.4306	0.9456	0.6823
		311111	1.7	2.4	2.02	0.8435	0.7937	0.9315	6.8536
		411111	2.4	2.7	2.55	0.8198	0.7511	0.9142	0.0193
		412111	2.7	3.3	2,96	0.7477	0.6742	0.5576	0.7288
		512111	3.3	3.5	3.37	0.7021	0.6188	0.5.10	0.6764
		513111	3.5	4.8	4.10	0.6195	0.5267	0.7594	9.5533
		514111	4.8	10.0	6.93	0.5299	0.4327	0.6599	0.4252
		414112	10.0	16.0	12,65	0.4605	0.3750	9.5733	0.3362
		314112	10.0	26.0	20.40	0.5177	0.4334	0.6317	0.3943
		214112	26.0	45.0	34.21	0.5744	0.4937	0.6866	V.4556
		113112	45.0	50.C	47.43	0.7105	0.6445	0.8198	0.6449
		113111	50.0	190.0	97.47	0.8030	0.7461	0.8935	0.7719
		113121	190.0	250.0	217.95	0.7329	0.6633	0.8345	0.6959
			250.0	280.0	264.58	0.6549	0.5746	0.7562	0.5756
		_	280.0	410.0	336.82	0.5606	0.4751	0.6509	0,4765
			410.0	520.0	461.74	0.5038	0.4152	0.5936	0.4164
			520.0	630.0	572.36	0.2264	0.1749	0.2516	0.1379
			630.0	760.0	691.95	0.1510	0.1163	0.1633	0.0871
			760.U 9i0.0	910.0	831.62 991.36	0.0636 0.0449	0.0653 0.0358	0.0800 0.0373	0.0471

Table I.4. Initial performance data, TOW crew (Continued).

DOSE-R		SYMP")				SQUAD			
RADS (CGY)	COMPLE	a TIM	E-RANGE	TIME	LEADER	GUNNER	DRIVER	LOADER
830-	1100	211111	0.9		1 00			A A	
030-	1100	311111	1.3	• .		0.8714	0.8306	0.9456	0.8823
		312111	1.4		1.35 1.59	0.8435	0.1937	0.9315	0.8536
		413111	1.6			0.7884	J.7251	0.8932	0.7755
		514111	2.5		2.12 2.83	0.6721 0.5299	0.5865	0.8012	0.6142
		515111	3.2		4.93	0.4381	0.4327 0.3434	0.6599	0.4232
		515112	7.0		5.27	0.3194	0.2439	0.5441 0.3929	0.3030
		515113	9.0		11.22	0.2203	0.1660	0.2597	0.1892 U.1113
		415113	14.0		17.55	0.5655	0.2024	0.3094	0.1367
		315113	22.0	35.0	27.75	0.3089	0.2444	0.3639	0.1715
		215113	35.0	50.0	41.83	0.3598	0.2920	0.4221	v.2102
		214112	50.0	56.0	52.91	0.5744	0.4937	0.6866	0.4556
		114112	. 56.0	67.0	61.25	0.6293	0.5542	0.7366	0.5103
		114111	67.0	92.0	78.51	0.7382	0.6683	0.8376	0.6672
		124111	92.0	110.0	100.60	0.6830	0.6147	0.7927	0.6059
		134111	110.0	160.0	132.66	0.6222	0.5581	0.7392	0.5411
		134121	160.0	180.0	169.71	0.5257	0.4584	0.6302	0.4437
		234121	180.0	190.0	184.93	0.4685	0.3990	0.5717	0.3829
		235121	190.0	200.0	194.94	0.3787	0.3128	0.4508	0.2688
		235131	200.0	260.0	228.04	0.2409	0.2338	0.3304	0.1992
		325232 315343	260.0	320.0	288.44	0.2130	0.1574	0.2430	U.1254
		415343	320.0 360.0	360.0 410.0	339.41	0.1312	0.0890	0.1382	0.0671
		415344	410.0	460.0	384.19 434.28	0.1072	0.0712	0.1116	0.0529
		515354	460.0	520.0	489.08	0.0674 0.0373	0.0452	0.0637	0.0291
		313354	700.0	.76040	407.00	11.03/3	0.0243	0.0311	0.0155
1100- 1	500	211111	0.7	0.9	0.79	0.8714	0.8306	0.9456	0.8823
		311111	0.9	1.0	û.95	0.8435	0.7937	0.9315	0.8536
		312111	1.0	1.3	1.14	0.7884	0.7251	0.8932	0.7755
		413111	1.3	1.7	1.49	0.6721	0.5865	0.8012	0.6142
		514111	1.7	5.3	1.98	0.5299	0.4327	0.6599	0.4232
		515111	2.3	5.3	3.49	0.4581	0.3434	0.5441	0.3030
		515221 515222	5.3	5.7	5.50	0.3559	0.2591	0.0490	0.2375
		515223	5.7 8.0	8.0 16.0	6.75 11.31	0.2496	0.1780	0.3064	0.1432
		415223	16.0	25.0	20.00	0.1668 0.2012	0.1179 0.1456	0.1933	0.0823
		315223	25.0	27.0	25.98	0.2405	0.1784	0.2342	0,1054
		315113	27.0	40.0	32.86	0.3089	0.2444	0.2809 0.3639	0.1292 0.1715
		215113	40.0	50.0	44.72	0.3598	0.2920	0.4221	0.2102
		214113	50.0	66.0	57.45	0.4483	G.3756	0.5429	0.3100
		114112	66.0	80.0	72.66	0.6293	6.5542	0.7366	0.5163
		124112	80.0	92.0	85.79	0.5647	0.4960	0.6746	0.4521
		134112	92.Ü	110.0	100.60	0.4979	0.4379	0.6058	ú.3876
		144112	110.0	120.0	114.89	0.4311	0.3815	0.5326	0.3267
,		144122	120.0	140.0	124.61	0.3377	4.2925	0.4065	0.2472
		145132	140.0	160.0	149.67	0.1918	0.1597	0.2021	U.1163
		245232	150.0	210.0	183.30	0.1656	0.1299	0.1838	0.0978
		345342 445443	210.0	260.0	233.67	0.1007	0.0729	0.1075	0.0570
		454454	260.0 300.0	300.0	279.29	0.0534	0.0367	0.0549	0.0560
		545454	340.0	340.0 420.0	319.37	0.0246	0.0179	0.0223	0.0124
				4E0.0	377.89	0.0179	0.0122	0.0146	0.0075

Table I.4. Initial performance data, TOW crew (Concluded).

DOSE-RANGE RADS (CGY)	SYMPTOM COMPLEX	TIME	-RANGE	TIME	SQUAD LEADER	GUNNER	DRIVER	LOADER
1500- 3000	211111	0.4	0.6	0.52	0.8714	0.8306	0.9456	0.8823
	311111	0.6	0.8	0.71	0.8435	0.7937	0.9315	0.0536
	412111	0.8	1.1	0.96	0.7477	0.6742	0.8676	0.7283
	513111	1.1	1.4	1.24	0.6198	0.5267	0.7594	0.5533
	514111	1.4	1.8	1.59	0.5294	0.4327	0.6599	0.4232
	515211	1.8	2.3	2.03	0.4509	0.3437	0.5755	v.3153
	515321	2.3	2.7	2.49	0.3678	0.2601	0.4807	0.2461
	515331	2.7	5.4	3.82	0.2614	0.1907	0.3575	0.1824
	515332	5.4	6.6	5.97	0.1908	0.1269	0.2318	0.10/0
	515333	6.6	8.0	7.27	0.1243	U.0823	0.1406	0.0604
	515334	8.0	20.0	12.65	0.0787	0.0524	0.0615	0.0334
	415334	50.0	24.0	21.91	0.0970	0.0659	0.1017	0.0425
	415324	24.0	32.0	27.71	0.1377	0.0952	0.1585	U.U619
	315314	32.0	50.0	40.00	0.2298	0.1668	0.2857	U.1108
	314414	50.0	72.0	60.00	0.3123	0.2263	0.4249	0.1822
	324513	72.0	86.0	78.69	0.3778	0.2732	0.5343	0.2521
	334513	86.0	96.0	90.86	0.3169	0.2293	0.4596	0.2054
	344413	96.Ú	110.0	102.76	0.2519	0.1904	0.3569	0.1577
	354523	116-0	140.0	124.10	0.1542	0-1111	0.2193	0.093
	355533	140.0	170.0	154.27	0.0782	0.0543	0.0941	0.0396
	455543	170.0	550.0	193.39	0.0435	0.0293	0.0466	0.0212
	555554	220.0	270.0	243.72	0.0000	0.0000	0.0000	0.0000
	555555	270.0	300.0	284.61	0.0000	0.0000	0.0000	0.0000
3000- 4500	211111	0.3	0.4	0.32	0.8714	0.8306	0.9456	0.8823
	311111	0.4	0.5	0.42	0.8435	U.7937	0.9315	0.0536
	411111	0.5	0.6	0.52	0.8198	0.7511	0.9142	0.8193
	412111	0.6	0.7	0.61	0.7477	6.6742	0.8676	0.7268
	513111	0.7	0.9	0.71	0.6198	0.5267	0.7594	0.5533
	514111	0.8	0.8	0.80	0.5299	0.4327	0.6599	0.4232
	514211	0.8	0.9	0.87	0.5428	0.4331	0.6879	0.4373
	515211	0.9	1.1	u.99	0.4509	0.3437	0.5755	0.3153
	515321	1.1	1.3	1.20	0.3678	0.2601	0.4807	0.2481
	515431	1.3	2.7	1.87	0.2919	0.1910	0.3872	0.1912
	535431	2.7	4.2	3.37	0.1941	0.1289	0.2578	0.1220
	535432	4.2	5.0	4.58	0.1266	0.0836	0.1584	0.0694
	535433	5.0	5.6	5.29	0.0803	0.0533	0.0926	0.0369
	515434	5.6	6.6	6.08	0.0825	0.0525	0.0915	0.0353
	515435	6.6	26.0	13.10	0.0514	0.0331	0.0518	0.0192
	515425	26.0	30.0	27.93	0.0745	0.0485	0.0833	0.0282
	515525	30.0	33.0	31.46	0.0781	0.0486	0.0935	0.0298
	515515	33.0	55.0	42.60	0.1118	0.0708	0.1465	0.0434
	535515	55.0	70.0	62.05	0.0085	U.0456	0.0862	0.0260
	555515	70.0	91.0	79.81	0.0412	0.0291	0.0493	0.0155
	555525	91.0	110.0	100.05	0.0281	0.0197	0.0302	0.0105
	555535	110.0	120.0	114.89	0.0000	0.0000	0.0000	0.0000

Appendix J

CREWMEMBER DOSE/TIME PERFORMANCE DATA

Table J.1. Performance data for gun crew: chief of section.

GRID	ا ا	(3800)						TIME GR	TIME URIO LINES	(HRS)					
	:		0.20	0.25 (-0.6)	0.52 (-0.5)	(40.40)	0.50 (-0.3)	0.63	(-0.1)	1.00	1.26	1.58	(6.00)	2.51	3.16
70 .	4529.93	5.06	1.0000	1.000	960A.0	0.6263	0.4800	2635	.2.	1961.0	0.1378	6060.0	•	150.0	0.000
- 4	27.09.55			3000		742/0	7040	700.0	0.463/	27.50	7872°0	1/62.0	4707	0.1710	0.1502
2	Z118.A1	. ~,	2000	2000	200	2000	0.8463	0.6941	Š	0.56.0	0.4770		381	0.2611	٠.
†	1644.72		1.0000	1.0000	9	1.0000	1.0000	0.9184	.65	0.4154	0.5395		407	0.5345	0.3136
~	1276.71		1.0000	1.0000	900	1.0000	1.0000	1.0000	.155	0.6691	0.6014	•	439	0.3689	0.3604
~ :	オニ・ニテロ		0000	1.0000	0000	1.0000		1.0000	1.0000	0.8155	0.6789	•	545	0.4662	0.4210
= :	70.00	69.7	0000-1	1.000	500	3000	1.000	1.000	3	•	0.Au45	•	.647	0.5653	•
<u> </u>	01./VC	£ 7	00000	0000	3000	9030.		3070-	2000	9000.	3000-	•	0.70.0	4044	0.5740
40	339.86		9000-1	0000		0000	•					•	986	77.69	
~	279.41		9000.1	2000	0000	0000	• •	1.0000	2000	: 0	1.0000	1.000	000	0.9657	0.7925
٠	216.A2		3000.	1.0000	000	1.000	•	0000.	1.0000	C	0000.1	•	000	1.0000	0.9334
ď	168.10		1.0000	1.0000	000	1.0000	1.0000	1.0000	000	1.0000	1.0000	.000	9	ೆ.	
₹ (130.64		1.0000	1.0000	1.0000	1.0000	0	1.0000	1.0000	1.0000	1.0000	9	1.0000	۶.	۹.
~	101.41		1.0000	000	1.0000	1.0000	-	1.0000	_	1.0000	2	S	1.0000	3	1.0000
~	18.72	~	1.0600		1.0000	1.0000	•	1.0000	1.0000	1.0006	1.0000	1.0000	0	1.0000	1.0000
-	1.10	-	0000.	3.000.	1.0000	1.0000	1.0000	1.0000	1.0000	0	0	1.0000	000	0	1.000
GRID	:							TINE GR.	ID LINES	(HRS)					
Į.	3500	Luc(Duse)			,								i		
			(y.v.)	(6.0)	6.31	(0 0 0)	9. 0.1	12.59	(5.85	19.45	25.12 (1.4)	51.62 (1.5)	59.81	50.12	65.10
2	4529.03	3,06	0,000	0,000.0	0.000	0.000	0.000		2	٦		000	00000	000000	7070
-	۳.	3,55	3.101.0	0.0688	0.0707	0.0006	0.0544	0.0468	\sim	~		41	0.0840	0.0741	0.0484
9	2729,55	3.44	0.1561	0.1233	0.1048	0.0762	0.0642	0.0585	59	٠,		150	0.1543	0.1410	0.1190
15	2114.A1		0.2114	0.1780	0.1589	0.0915	0.0750	0.070	9	٠,		121	0.1426	0.2079	0.2134
₹. ! —	1640.72		0866.6	0.2552	0.1845	0.1252	0.1079	0.1051	<u> </u>	∹	•	172	0.2024	0.2690	0.337
~ •	12/4.71	5.11	0.3730	0.3510	0.2476	0.1660	9651.6	0.1530	۲ رو م	0.1455	0.2148	2 4	6.127.9	10/5.0	0.4600
	76.04		0.4.0	0.000	1004.0	0.3194	0.4374	0.1172	2 2	•	•	7	0.4573	0.5434	0.623
: 2	547.16		0.5071	0.4785	0.4004	25.44.0	0.4255	0.3994	=	٠.		9	0.5531	0.6325	0.6654
•	463,54		0.5676	0.5213	0.5027	0.4854	0.4660	0.4393	134	٣.	•	290	0.5835	0.6745	0.6641
•	359.42		0.6225	0.5635	0.5332	9505.0	0.4929	0.4793	4 62	٦.	•	323	0.6157	0.6962	1669.0
~ .	219.41		0.6684	2.505.e	0.5579	0.5248	0.5165	0.5211	2	•	•	266	0.6523	0.7101	0.7154
øv	712.46		2.7145	4444	2000	9646	1045.0	0.564	9 9	٠,	77.0	7 4 6 4 6 4 6 6 4 6 6 6 6 6 6 6 6 6 6 6	2007.0	3474	0.7507
٦ 4	40.4			20.00	0 41 A	7.54	4101.0	7456		; -	25.50	1 9	2040		
r m	10101		2000	2000	0.9531	9.336	0.7752	0.6482	0.9359	0000	0000		0000	1.0000	1.000
~	_	-	9	1.0000	1.0000	0.9729	0.9640	1516.0	5		1,0000	9	1.0006	1.000	1.000
-	= :	:	1.0000	2.000	1.0000		1.0000	•	000	00	1.0000	1.0000	000	=	1.000

Table J.1. Performance data for gun crew: chief of section (Concluded).

GR ID LINF	J.O.S.E.	LOGTUOSE)						TIME OF	TIME GRID LINES	(HRS)					
			79.43	100.06 1	125.89 19	154.49	149.53	251.19	158.49 149.53 241.19 316.24	398.11	501.19	501,19 630,06 794,33 1000,00 1258,93	194.53 1	1 00.000	258.93
			•	•					((a•)		(0.5)	(6.4)	(0.5)	(1.8.)
٦ د	4529.03		0.000.0	0.000.0	0.000	0.000	0.000	9000	0	0	0000	0	6	4	4
17	35.16.24		0.0350	0,000	0.000		0000					3000	0006.0	0000.0	0.000.0
9	2729.53		0.1221	0.041)	75000					0000	00000	00000	000000	2000	0.00
2	7118 R1		9000			•					_	0.000	0000.0	0.000	0.0000
	16.40			2001-0	C/Cn*n	_	0.000	0.000	-		_	0.0000	0.000.0	0.000.0	0.000
	U/ 5701		1 1 2 1 1	20020	0.1209	_	0.025b	0.0056	_	_	_	000000	_	0.000	0.000
2 (17.47.		0.5122	0.3662	0.2547	_	0.1030	0.0547	-			000000		0.0000	
2	30.171	٥,٠٥٥	0.6397	0.5516	0.4705	1045.0	0.2028	0.1557	0.1209	0.0676	0000	0000			
	769.24	-	0.6766	0.6388	0.6281	_	0.4904	46640				9 4			
2	547.10	_	0.589.0	0.6940	1069	_	4777	400						0000	0000
~	403,54		4004	2024	100							0.6660		0.0000	0.00.0
~	C 0 0'12				0360.0	-	נרסי.					0.3784		0.1739	0.091
•		_	3000	מי לי	1464.0	_	0.6972					0.3910		0.3373	0.2714
			1001.0	0.7005	0.7014		0.7069					0.5745		0.4847	0.445
٤	714.AZ		0.7305	0.7509	0.7280	_	0.7166					0.6579		10140	10.7
∽	104.70		0.8624	0.4910	PP49.0	_	1616.0					440		4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	, AUG.
3	150.64		1,0000	1.0000	1.0000		0000					9000		1504.0	0000
M	101,41		1 0000	7000	0000							0000		0000.	10000
٨	78 47						0000					1.0000		0000.	1.0000.1
; -			2000	0000	0000		-000					1.0000		1.0000	1.0000
•			0 : 0 : T	3000	1.0000		1.0000					1.0000		1.0000	1000

Table J.2. Performance data for gun crew: gunner.

01 03				•				;							
11.5	UUSE	LOGIDOSE						7 1 Mr	TIME GRID LINES	(HRS)					
			0.20	(4.0-)	0.32	(-0-4)	0.50	0.63	6.79	1.00	1.26	1.58	2.00	2.51	3,16
9.0	4529,03		1.0000	_	•	2,404.0		72.72							•
~	3514.34	3,55	1,000	000	1000	A 7 4 7	2007	7118	907.0	1961-0	- <	¥040.0	4540	•	0000
9.	2729.55		1.0000	c	. =	5266.0	0.0		2.4			2256	2010	C 2 7 7 0	
₹.	211A.A1		1.0010		۶,	1.0000	9069	-	10.750			20000	176.0		
7	1644.72		1.0000		1.0000	1,0000	1,000		21.0		2	6094			
~	1276.71		1.0000	•	1.0000	3.000	1.0000	-	0.8522		0.74	0.6794	0.60		
7	70.170		1.0000		1,0000	1.000	1.0000	-	1.0000			444			
_	769.29		1.0000	•	1.0000	1.0000	3000	_	1.0000				777		
0	547.16		1.0000	1.0000	1.0000	1.0000	3.000	-	1.0000		0	0.8774	200		
σ.	7 0 0 0		1.0000	1.0000	1.0000	t.aanu	1.000.1	1.0000	1.0000		1.00	1.0000	0.8677		7811
20 r	159. 82	- 1	1.0000	•	1.0000	1.0000	1.0000	-	3.0000	•	1.00	1.0000	0.9917		
•	F		.0000	1.0000	1.0000	S S	1.0000	-	1.0000	1.0000	1.00	1.0000	1.0000	c	
، ۵	712.R2		1.000	_	1.00.1	000	1.0000	1.000	1.0000	1.0000	100	1,0000	1.0002	-	
n :			1.0000	_	1.0000	1.0000	1.0000	1.000	1.0000	1.000.1		1.0000	0000	-	
.	44.00.		1.0000		1.0000	1.0000	1.000c	1.000	1.000	1,0000	1.000	0000-1	1.0000		
m (101.01		1.0000	•	1.0000	300	1.0000	1.000	00001	1.6000	000	0000			•
NJ -	18.72	~	3000.	Ç.	1.0000	1.0000	1.0000	1,600	1.0000		3			•	•
-	61.11	_	1.0000	1.0000	1.0000	000	1.0000	000	1-0000	0000	1,000	0000			
							•	•		: •	•			•	2
4/															
of do										4					
LINE	JSUA	Tuntouse;						THE OK	ID LINES	(HKS)					
			3.94		6.31	7.94	9	12.59	S	6	- ح	_	7	-	-
			(4.6)	(1.0.7)	(8.0)	(0.9)	(0.1)	<u></u>	(2.1.)	(2.1	(4.1.	(5.1.)	(4.1.)	(7:12)	
9	4529.03	4	0000	0000	0										
1.1	5516.34	54.8	0.1845	274	1447	200			•	0000	0.000	000000	000000	00000	0.000
91	27.49.55	5.44	0.2759	9672.0	0.1403	5070	0.020				77.0	2,00.0	8. O. O.	0.0875	0.057
1.5	2118. RI	5,53	0.3662	0.3236	0.2540	0.1761	1448		•		0 0 0 0	3000	201.0	0.10/0	0.15/1
7	1644.72		9.4563	0.4157	0.3195	0.2305	0.2010			0 2 3	2000	4466	0.62.0	20400	0.6457
× •	1274.71		0.5359	1060.0	0.3931	0.3119	0.2724		_	_	0.3175	0.4881	0.00	12.00	2000
21	70.076		0.505.0	0.5380	0.4905	0.4376	0.3599		_	_	2025.0	0.4081	0.4281		4000
	769.29		0.6241	0.6003	14/5.0	0.5343	0.4635		-	-	0.5053	0.5220	0.5570	0.6482	7104
<u> </u>	297.16		0.6893	0.6550	0.6310	0.6072	9085.0		_	~	0.5859	6209.0	0.6536	(1.7253	0.7537
	7		0.7578	0.6896	0.6626	6403	0.6123	.5822	_	_	0.5917	0.6120	0.6735	0.7596	0.7720
۰ د	74.6	۶.5 د . ک	0.7669	0.7234	0.689B	0.6637	8044.0	.6187	_	~	0.6145	0.6344	0.6958	0.7767	0.7838
• ,	•		1972	0.7581	0.7164	0.6851	0.6674	. 660 d	_	_	0.6815	0.6955	0.7323	0.7680	0.7947
0 u	م ا د د	2.54	0.A275	2462.0	9671.0	0.7064	0.6941	1901.	_	_	0.7536	0.7746	0.7860	0.7992	0.8057
n÷	5	6,43	92700	0.4699	0.8124	0.7549	0.7310	.7682	0.8025	•	1758.0	0.8726	0.8859	0.6974	0.9075
.	٠,		3000	0.9517	n.8370	9 . A 1 06	0.7840		0.8776	•	9056.0	0.9712	0.9485	1.0000	1.000
3 0	5 6	10.3	2000.	0000	0 7 0 ° E	D. 8977	0.8649		0,9612	1.000	•	1.0000	1.0000	1.0000	1.0000
. –	20.00	7.0	2000.	0000	0000	0.9846	0.9782	0.9853	1.0000	-	1.0000	1.0000	1.0000	1.0000	1.0000
•	_	F		2	300c*		2000.1		9090	1,000	•	٠.	٠.	1.0000	1.0000

Table J.2. Performance data for gun crew: gunner (Concluded).

THE PROPERTY OF STATEMENT OF ST

	3.1)		
	794,53 1000,00 1258,93 (2.9) (3.0) (3.1)	00000000000000000000000000000000000000	
	(2.9)	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 1.00000 1.0000 1.0000 0.0000	
		60000000000000000000000000000000000000	
	\$6.070 P1.108	00000000000000000000000000000000000000	
(Has)	398.11	00000000000000000000000000000000000000	
TIME CRID LINES	516.23 (2.5)	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	
TIME OR	251,19	0.0000 0.0000 0.0000 0.0000 0.1175 0.7275 0.	
	99.53	00000000000000000000000000000000000000	
	158.49 1	20000000000000000000000000000000000000	
	125.89	00-00-00-00-00-00-00-00-00-00-00-00-00-	
	100.50	1000001	
	14,43	0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.000000	
		44444444444444444444444444444444444444	
		44 X X X X X X X X X X X X X X X X X X	
CRIO.		0~0%4MU~~~~~~~~~	

Table J.3. Performance data for gun crew: assistant gunner.

	3.1	(0.5)	<		· c		Ě	Š (ė,	c	ě	Ċ	Ö	e ·	c	Ö	_	_		-	_			•	01.56															2000		
	14.5	(0.4)	2		-				7 1	0	6	c	P .	9.0	76.0	2.00		1.000	1.0000	1.0000	000			3	7.10		0.000.0	0.0674	4.1607	0.2340	0.4232	0.4153	0.5082	0 . TO	0700.0	7077	4631.0	7,700	5 - 10 2 4 5 - 10 2 4	****	1000	
	2.00	(0.3)		0.3216								0.8170			-	•	1.0000	90.	1.000	1.0000	1.0000			9	9-7-		0.000.0	0.1012	0.1584	0.2157	45.50	0.3758	0.5606	2116.0	*****	0.0674 67.00		101000			0000	
	1.5A	(5.0)	080	169	498	566	40.4			5	9	0.5606	000	00000	000	000	0000	000	Š	3	Õ			4	(53)	•	•	•	•	•		•	•	•	D. U. O.	0 C A C C		1 TO 0	2000	9665	0000	
	1.26	(0.1)	-	3	ŗ			•	•	0.7042	•	2000.	9	• •	0000	0000	0	1.000	_	1.0000	5		•	-	(4)	•	696.	.030	120	.150		200	9.50	505				126	4 × 4	0.0441		
(HRS)	1.00	(0.0)	•	0.5024		•	•	•	•	•	0000	3000.	0000.	٠	0000	1.0000	0000	0000	9090-	1.0000	1.0000		(443)	7	(1,3)		٦.	€.	٦,	٦.	-	÷.	•	,,,		ייי	•	-		0.4988		
TIME GRID LINES	0.0	(-0-1)	0.2706	0.6064	0.7186	7644	0.7871	A 4 4 6	1000			9000		0000	0000-	0000.	0000	0000	1.0000	3.000.	1.000		INC OWIN LINES	20	•		-	0.0		11.0	֓֞֜֜֜֜֜֜֝֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓		7	, . , .			9	5	77	0.8595	. 6	0
TIME LA	63.0	(-0-5)	0.3635	0.7015	0.7485	0.7955	0.9455	1 0006									3000	0000	0000	1.000	3	4114	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	12.59	(1.1)		00000	0.0776	0.000	0.1205	0.17.0		74.40		90%	0.5761	0.6212	0.6730	0.7386	0.8124	0.8951	9832
	0.50	(-9.5)	8	0.7741	. A 5	•	9	1.0000											2000.	000.	-000c			•	(0.1)		00000	0.0830	0.100	777.0		3000	4 4 4 C	44.4	0.5702	0.6003	0.6292	0.65A1	0.5974	0.7555	1444.0	0.9751
	07.0	6.0-	٠.	0.8425	٣.	_	1.000	1,000	0.70										0000.		1.000			7.94	(0.0)															0.7465		
	. 62.0	(c.a-)	POOF.	1.000	3000.	1.0000	1.0000	1,000	1,0000	0000		2000									1.0000			~1	•			1071.0	00110	7.000	7000	0.0474	242	5.65.0	0.6243	6.4541	0.4636	0.7131	17407	0.8779	0.9538	1,000
	0.25	•	1.0000	٠.	۶.	1.0000	٦.	۶.	٦,	. =		1.0400	, =	0000	. 5			•			0.00.			5.61	(0.7)	4	•	• •	•					٠ -	٤	٠.	٠.	٠.		6.9455	٦.	1.9400
	07.0		1.0006	0000.	1.0000	1.0000	1.000.1	1,0000	1.0000	1,0000	1.0000	1.0000	1,0000	1.000	1 0000	1.0000	1000							~	(9.0)				•	7.7	664	5	165	656	707	.738	.770	۴,	.955	600	96.	3.000.
TUCLOUSE)	•		3.b6	۲۷۰۶	P. 44	5.57	5.67	3.11	5.00	6,69	2.18	2.67	2.56	2.45	2.54	2.24	2.12	-	5				LUG(UUSE)			44			, , , , , , , , , , , , , , , , , , ,	C 2 . 2	3.11	2.00	69.7	8.1A	5.67	Ł.56	7.45 F	2.34	2.21	2.12	۲.01	er. 1
DUSE FU			4529,03																				DUSE LO			1529,93	516.24	ار ا		7	214.71	*	7,	9 -	3.0	Ž,	Ę	24.	2	74.	-	A.12
GP IN			20.						~2		3											GRIN	LTGF			4						~		.					s	7	M I	~

のできながらないに対していないとなり、自然のなかののの意味がないなってものです。

Table J.3. Performance data for gun crew: assistant gunner (Concluded).

ことの言いたのならなの言にとい

	58.93		3000	2000	2000	2020	2000	0000	2020	0000	3000	7 - 50	2716	4450	6200	2000	2000		2000	2000	1.000
	2	٠																			
	00.000	•			2000	0000.0	0000.0	0000	000000	0.000	0000	0.2239	0.4172	0.5475	0.6819	986	1 0000		0000	0000.	1.0000
	794.33 1000.00 (2.9) (3.0)	6		00000	2020.0	0000.0	0.000.0	0.0000	000000	0000	0.2134	0.40A3	0.5247	0.6291	0.7334	0.9783	1.0000		0000	3.5000	1.0000
	630.96				30.0	0.0000	0000.0	0.000	0.000.0	0.0654	0 3474	0.5063	0.6053	0.6442	0.7632	0.9314	1.0000	0000			1.0000
	501.19				3335	0000.0	0000.0	900000	0.0000	9.3869	5105.0	0.5128	0.6400	50010	0.7775	0.9647	1.0000	0000			3000
(HRS)	398.11					0000	0000.0	0000.0	0.1214	10040	O. SURB	0.6242	1004.0	0.7065	0.7805	0.9578	3336.1	0000			1.0000
TIME GRID LINES	316.23 (2.5)		0.000			0000	30000	0.0348	0.1848	6.4477	5-54.3	1.6477	0.7178	0.7546	0.7894	0.9506	1.0000	1.0000			3 · 0 · 1
11HE 68	251.19		0.000				> 00 ° 0	0.0921	0.2680	0.5085	4199.0	0.7116	0.7394	0.7648	0.7902	0.9431	1.0000	1.000			0000
	199.53	0000"6	3030.0	0.000			15 70 0	2071.0	0.1549	0.5707	0.7214	0.7325	0.7364	0.7523	0.7850	0.0354	2000.	0000	0000		
	158.49	0000,0	0.00.0	0.000	45.00		7/11		4504	0.6563	0.7470	1477.0	0.7419	7497	1507.0	0.9276	2020.	2000.	1000		
	125.39	0.000	0.000	120000	9 0704	724			957.5	36/96	7 x x /	0.7450	0.7436	0 7483	C-0/"	1616.4	3000	3030.1	1.0000	0000	
	100.00	0.000.0	2000.0	0.0465	0.3459	0 27.13				2000	2 . 4 . 6	2.412	67.07.0	3007	****	7.0	200	2000.	3030.1	1 0000	
	79.43	0.000.0	0.0509	9151.0	0.2245	3445	1 K 1 C	0727	40 C C C	0.77.0	2000	7777.0		2007.0	2000			3000.	2000.	1.0600	
しょいいっとり		3.06	5.55	3.48	5,57	5.22	17.8						ָרָי יִי ער יי		, ,	, . , .		(· ·	55. -	6/1	•
) gc _U n		4529.03	3515.44	2729.55	<114.A1	1649.72	17/6.71	70 570	70007	70.70	200	450	2/0/6	7. 7.6	16.8 24.	7 07 6			/R.72	01.11)
GP IN		8	-	•	<u>.</u>	7	13	2		: :	2 3	• «	~	ء .	y ur	1 4	r M	٠,	V		

2.51 3.16 (0.4) (0.5)		50.12 65.10 0.0000 0.0000 0.0090 0.0000 0.0090 0.1010 0.1508 0.2124 0.3174 0.3212 0.5174 0.3212 0.5174 0.5124 0.5174 0.5124 0.5174 0.5124 0.5174 0.5124 0.5174 0.5124
00.5	0.000 0.0000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.0000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.0000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.0000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.0000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.0000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.0000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.0000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.0000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.0000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.0000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.0000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.0000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.0000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.	6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
1,5A (0.2)		31.62 (1.51) 0.0291 0.0391 0.0176 0.1760 0.1760 0.3872 0.3872 0.3872 0.3872 0.3872
1.26 (0.1)	0.1378 0.34.912 0.34.913 0.46.913 0.64414 0.76411 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	25.12 (1.12) 0.0000 0.0000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000
(HRS) 1.09 (0.0)		19.95 (1.3) 0.0292 0.0248 0.0276 0.0276 0.03291 0.3291 0.3291 0.3291 0.3291 0.3291 0.3291 0.3291 0.3291
TIME LPID LINES U.63 U.79 [-0.2) (-0.1)	0. 345 9 0. 345 9 0. 51111 0. 61111 0. 61111 1. 0000 1. 0000 1. 0000 1. 0000 1. 0000 1. 0000 1. 0000 1. 0000 1. 0000	115. BS (1.2) (1.2) 0.0000 0.0572 0.0573 0.0573 0.1170 0.1170 0.1170 0.3172 0.3172 0.3172 0.3172
11Mt 69 0.63 (-0.2)	50% 60 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	11 ME GR 112.59 (1.1) 0.0000 0.0264 0.0855 0.0085 0.1018 0.1018 0.1018 0.1018 0.1018 0.1018 0.1018 0.1018 0.1018 0.1018 0.1018
0.50 (-0.3)	6,06,000	10.00 (1.00 0.00 0.00 0.00 0.00 0.00 0.0
0,40 (8,0-)	66611111111111	
6.45 (-0.5)		6.31 0.00
0.25 (-0.4)		0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0
0.20		0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
LAG (UNSE))
กกรธ	25.00 20	100 100 100 100 100 100 100 100 100 100
URID LTRF	はてららはまさにはなせてららみまごま	CE

Table J.4. Performance data for gun crew: leader (Concluded).

58 In	DO SE	LOG(DOSE)						TIME 6R	TIME GRID LINES	(HRC)						
			79.43	100.00	125.89	158.49	199.53	251.19	516.23	396.11	501.19	501.19 630.96 (2.7) (2.8)	794.53 1	794.53 1000.00 1258.93 (2.9) (3.0) (3.1	1258.93	
2	4529.93		0000	000000	0.000	0.000	9		9		4					
1.1	3516.74		0.0164	3030	0.000					0000	0000	9000.0	000000	00000	0.00.0	
٥	2729,55	5.44	0.0558	0.0174	0.0074				0000	00000	0.000	0000.0	00000	30000	0.000	
51	2118.A1		0.0352	0.00 A	20.0	30.0				00000	0000.0	0.00.0	0.00.0	00000	0000	
7	1644.72		4050	283.0					0.000	0000	0000		0.000	0000.0	0000.0	
	1216 71			3 7 7 6		0.00.0	- L		0.000	0.000	0.000		000000	000000	0.0000	
2 0			3.00.00	0	A 1 . 0	0.1145	14/0.0	0.0414	0.0150	0.000.0	0.0000		0.000.0	0.000.0	0.000.0	
· :	2 0 0 1		0/05.0	11200	9.47.0	6.4003	2961.0	0.1414	0.0865	0.0445	0.0000		0.000	000000	0.000	
- :	F		0.4440	5 1 2 1 5 C	5065	6.4611	0.4072	0.3380	0.2730	0.2402	0.2119		0.000	0.000.0	0.000	
2	97.765		0.5040	2.17	0.5474	0.5747	0.5462	0.4912	0.4325	0.3030	0.3046		0.1209	00000		
•	464,54		0.5720	1915.0	0.5/84	0.5744	0.5607	0.5345	0.4910	0.4225	0.3702		7220	700	1	
9	359. A.		0.5814	0.5/A1	0.576;	0.57.46	60.570	0.5656	0.5547	0.4616	0 4460		2000	4000	22.0	
7	270.11		0.5910	0.5667	0.5850	0.585.0	0.5871	0.5960	0.5/63	8605.0	400		3000		7 V C	
•	716.AZ		0.6255	0.6322	0.4365	0.6349	0.6276	0.6264	6176	9 4 7 4 0	2000		7 7 7 7	7077	0000	
Ş	154.70		0.8365	1554.0	D. Rof. 5	0.8779	0.8877	1808	0000	2000	920			77600	0020.0	
3	150.64		1.0000	1.0000	1.0000	1.0000	1.0000	0000	0000	1000			1000		0000.	
~	101,41		1,0000	1,000	1.000.3	1.0000	0000	7000					0000		0000	
2	3.8.72		1.0000	0000	0000						0000		0000	1,0000	1.0000	
-								000.1	00000	0000.	2000.		1.0000	- GOOC	1.0000	
•				0 0 0 0 0	0000	9000°.	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	

Table J.5. Performance data for FDC crew: fire direction officer.

u1 85	5504	(10000000000000000000000000000000000000						TIME OR	TIME GRID LINES	(HRS)		-			
			6-0-1	(4.0-)	(3.0-)	0.40	(5.0-)	0,03 (-0,2)	(1.0-)	1.00	1.26	1.58	2.00 (0.3)	(0.4)	3,16
81	4529.03	3.uk 3.25	0000°1	1.0000	9000°.1	0.8120	0.4400	0.71635	0.2796	0.1361	0.1578	0.0909	0.035 0.4035	0.0237	0.0000
<u>a</u> :	6769.55		1.0000	1.0000	1.0000	7066 0	1428.0	5441.0	6451.0	678	0.6015	0.5426	0.5386	0.4145	0.3574
<u>.</u>	2117.41		0000	3030.	0000	2020	3 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	0.7546	0.7619	0.7147	0.6602	0.6455	**************************************	0.4840	5 . 4 . 4 . 6 . 6 . 6 . 6 . 6 . 6 . 6 . 6
	12/4/21		0000	2000.1	0000	2000	0000	1.0000	0. P. S. P. 4	7 80	55570	1000	0.6480	0.6101	0.6092
2	40.166		1.000	1.0000	1.0060	1.0000	1.0000	1.0000	1.0000	877	0.7824	0.7610	0,7162	1999.0	0.6386
=	40,04		0000.	1.0000	1.0000	1.0000	1.0000	•	٠.	000.	0.8674	0.7902	1157.0	0.7149	0.6162
<u>.</u>	527.10		1.0000	1.000	1.0000	3000.	, , 0000	1.0600	•	1.0000	1.0000	0.85.74	1661.0	0.700	0.7151
o r :	2		0000.	0000*;	1.000	0000°	0000	3000	•	000.	0000	0000	0 . T J J E	0 0	0.1040
:o r	75,750	ر د د د د	00000	0000	0000		0000.	2000	20.0	0000	0000.		0000	0070	9404
	`	;	0000	0.000	3000			9 0	. 0	3030	0000	0000	0000	10000	6556.0
	-	2.43	2.000.	0000	0000	0000	0000	2000-	0000	1.000	0000	0000	1.0000	1.0000	1.0000
₹	_	د، ۲	1.0000	1.000	1.0000	1.0000	1.0000	1.000	0	1.0000	000	1.0000	1.0000	1.0000	c
×	-	2.01	o n o	1.0600	1.0000	1.0000	ç	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
น	Œ	1.40	o o	1.0000	1.0000	1.0000	1.0000	1.0000	0000.	1.0000	ာ (၁	1.0000	1.0000	1.0000	0
-	01.11	0	000	1.0000	1.9000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	000	9
6710								TIME GR	RRID LINES	(HRS)					
111	U U o E	LOG(UASE)			;		·	9	4	3		4	14	51 12	4
			(9,0)	7.0	(N. ()	(6,9)	9.	(1.1)	5 (3.5	(2.1.3)	(1,4)	(5.1.)	(9:1)	(1.7)	(8.1
		,	•	,						:	•		:		•
3 0 /		5.66	7070.0	0 0 0 0 0	0.00.0	0.000	0.000.0	0.000	0000*0	0000.0	0000.0	000	000000		3 :
- :	_	در در	20/110	در ا ر . ر در ا ر . ر	0.1545	2,1145	0.1040	916.0	20.00	001.0) ·	012100		~ ~
2 4		, 42 44 44	C801 0	0.27.0	1710	4454	1,1010	900	7051.0	1689	5000	25.5	0.3084	0.3067	. ~!
1 2	77.0741	22.5	47.0	7 K K D . C	0.3074	2000	26.5	0.2197	0.2278	0.2601	5.3007	373	0.4317		0.4690
: 12	12/4.71	3.11	0.6159	0.5748	4464	0.3622	0.3154	0.3036	0.3211	0.3555	0.3994	489	0.5469		0.6506
12	40.160	5.00	0.6332	1874.0	4512 U	0.5040	P. 4230	0,3944	0.4623	0.4518	0.4476	915	6055.0		0.7404
=	160.24	2.49	0.6506	0.6435	0.424.0	9450.0	0.5379	0.5117	0.53AS	0.5456	90,5.0	615	0.6498		0.7775
<u> </u>	597.16	۲,۷	0.6781	0.6661	0.6613	1054.0	0.6324	0.6072	12190	1659.0	0.0530	2 2 4	0.7536		7 00 0
.	400 1		25.00	# P P P P P P P P P P P P P P P P P P P	1744.0	2000	2602.0	2000	6,0040	46.04.0	4104	2 4	747		3 6 6 6
~ ه	0x 67 1	יי טיי	0.7010	0.7481	7184	0.7040	0.7044	0.7091	0.7135	0.7320	2672.0	. 69.	0.8130		0.8379
۵ -	214, A2	2,54	7404.0	0.777	0 7271	0,7070	0,7159	0.7395	0.7694	0.7978	0.8149	827	0.8383		0.8477
s	108.70	2,43	0.9372	A575	0.7998	1542.0	0.7371	0.7801	0.8256	0.8638	0.8485	200	0.9125		0.9253
3	150.64	ج 1°2	1.0000	0.9470	0.8784	1208.0	0.7743	0.8323	0.8831	0.9298	0.3616	0.4780	0.9512		0000
m i	•	ું:	5 6	1.0000	4444 C	3636	2128.0	- X - O	1176.0	2000.	0000.1	3	00000.		2000
u -	14.76	04.	0000.1	0000	0000	1235°C	74/7.0		0000.		0000	0000	0000	0000	
~	•	`.	= = =	=	0405.	•		=	;; •	2		2	>>>>	_	

Table J.5. Performance data for FDC crew: fire direction officer (Concluded).

נומיו								TIME SH	BRID LINES	(485)					
LTITE	3500	LaGrunse)	14.43	40.001	125.89	156.49	14.641	251,19	310.21	396,11	901.19	630.46	194.53 1	794.53 1000.00 1258.93 (2.9) (3.0) (3.1)	158.93
										•	•	•	•		
	40.015		9000	<	_	_			0.000	000000		0.000.0	0.0000	0,000	0.0004
2 ?	7.4.4		41.0	<		_						_	0.000.0	0000.0	0.000
_	P			•	•							_	0.000	000000	0.000
9	27.29.55		0.1250	Š	_	_									0000
5	ZIIA. AI		4646 O	¢.	_	_						_	2000		
	LE 444.		5648	•	_	_							0.00.0		0.0000
- :	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		2204	•	-	-						_	0.000		0.000.0
2 9	1.00		70.00	•									0.0000		0.0000
~	すじ。一ナウ		7 C C	=	_								010		2000
~	109.29		0.A172	c	_										
3	547.15		4619.0	c	_								9.5176		0000
. 0	0 1 2 E U		0 8758	C	_								0.5140		0.0414
٠ ،			0 1 4	6									0.6276		0.2716
9 -	4		27.78										0.7069		0.4450
- 4								0.8355	0.8578	0.8308	0.8276	0.8198	0.7863	0.7.109	0.6200
9 4			200	: <									0.9875		1.0000
n :				•									1.0000		1.0000
7	****			•									1.0000		1.000
~	14.12		2000.	•											
7	14.76		1000	_									3000		2000
-	61.11	1.79	1,000	1,0000	1,000	1.0000	1.000						1.0000		1.0000

Table J.6. Performance cata for FDC crew: horizontal control operator.

GRES	9	40000						TIME GR	TIME GRID LINES	(HRS)				·	
			0.20	0.25 (-0.6)	0.52	(+·0-)	0.50	0.63	0.79	1.00	1.26	1.54	2.00	2.51	3.16
2.	4529.93	3.66	1.0000	0000-1	C	0.6263	0.4800	0.3635	0.2706	1961.0	0.1378	6060-0	0.0535	0.0237	0000.0
9	2729,55					: 6	7070.0	•	0.00.0	י י	•	100	0.5440		0.2020
2	211A. A1		7070.	2000	٠,	1.0000	. "		•	0.5377	5789	0.5564	0.5037	9 4 5 4 5 6	0.427
= :	1644.72		1.0000	1.0000	1.0000	1.0000	٠.		0.7198	0.6723		584	0.5300	•	0.4825
<u>.</u>	12/5,71		1.0000	1.0000	•	1.0000	1.0000	•	0.7776	۲.	•	414	0.5543	C	0.5221
	94.047		0000	2000	2000	3000.	1.000	2000.	1.0000	0.8328	•	583	0.6317	vo.	0.5483
: 2	597.16		0000		•		3000	2020	•	0000.	•	717	0.6823		0.5554
•	463,54		1.0000	0000	1.0000	0000	0000	9000	•	2000	•		0. 4545 0. At 16	٥.	- 04
49 1	159. A2		1.0000	1.0000	900	•	1.0000	1.0000	3.000	1.000		0000	0.9876	٠.	•
~ .	12.6/2		1.0000	1.0000	S	900	1.0000	1,0000	1.0000	000		000	1.0000	~	=======================================
ں م	24.412		1.0000	00001	1.0000	000	1.0000	1.0000	1.0000	000	•	ē.	2	1.0000	2
٦ ٩	2			2020.	900	0000.	1.0000	1.0000	1.000	1.0000	•	1.0600	3	•	3
					0000.	֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓	0000.1	9	0000	ŝ	3	•	0	1.0000	1.000
• 10	76.72				000	0000.	1.0000	000	1.0000	9	~ '	1.0000	.	0	3
	3.00		2000	0000.	0000	0000.		0000	3	3000-1	ē,	3	S	0	Ç,
•	-		0000	200.) ; ;	3000.	C	3.000	3000	1.0000	1.0000	1.0000	1.0000	0000.	1.000
•															
GRID								TIME GR	GRID LINES	(HRS)					
LINE	DUSE	LNG(UNSE)							1						
			85.5 5.48	5.01	6.31	7.94	10.00	12.59	15.85	19.95	25.12	31.62	39.81	50.12	63.10
			G		6.6)	6	(1.0)		(2.1)	-	<u>.</u>		-		•
1.0	4529,93	3.6h	.000	0.000		0.000.0	0.000.0	0.000	0.00.0	9	0000.0	000000	000		0.000
_:	3516.44	3,54	. 237	•		0.1830	0.1682	0.1551	0.1567	-10	0.1664	0.1548	106		0.0980
<u>.</u>	2729.55	5. 44 1.	339			0.2182	0.1955	0.1840	0.1907	25.	0.2125	0.2216	. 246		=
	1544 72		2	•	0.5226	0.7534	0.2278	0.2147	0.2247	0.2415	0.2586	0.2.86	0.3260	0.3296	0.3151
_	1276.71	3.11	527	• •		46.00	417.0	10/0	7077		1555.0	0.12.0			2 5
~	991.04	3.00	539	• •		0.4506	0.3956	0.3797	0.4015	4	0.4510	10.0	564		Š
= ;	769.20	2.89	.562	•		0.5170	0.4619	0.4673	0.4898	.51	0.5345	0.5564	.540		1.7027
2 9	597.16	2.7×	£ 7.	•		0.5646	0.5544	0.5386	1155.0	.51	0.5918	0.6137	.655		9
	405.44	2.67	- 64	•		0.5964	0.5859	0.5714	0.5652	.53	0.5994	0.6252	.679		3
۰ ~	27.000	, u	500	•		0.6117	0. 60 44 0. 60 44	0.5970	0.5853	6	0.6155	0.6420	20.		0.7497
ه .	216.82			•		0 2 2 2 0		1630.0	2120.0	•	20000	# P P P P P P P P P P P P P P P P P P P	721		ል '
'n	168,30	2.23	914	•		0.6668	0.00°C	7016	700.0		0.1.0		֭֓֡֓֞֝֓֡֓֓֓֓֓֓֓֓֓֓֓֡֓֓֓֡֓֓֡֓֓֡֓֡֓֡֓֓֓֡֓֡֓֡֓֡		0.40.0
₹	130.64	2.12	000	• •		0.7424	0.690	0.7699	0.630	86	0.9436	0.9670	986		Ö
M (101.41	2.01	0	1.0000	.958	. 846	0.7957	0.8620	0.9418		1.0000	1.0000	000	1,0030	1,000
~ .	8.7	1.90	000	1.000	1.0000	0.9754	0.9672	0.9779	0	S	5	.000	.000	1.0030	1.0000
-	=	1.79	000.	.000	•	.000	1.0000	1.0000	0000	9	000	10000	000	000001	1.0000

Table J.6. Performance data for FDC crew: horizontal control operator (Concluded).

200 201120 201120 201120 201120 201120 201	L06(00 	79.44 (1.9) 0.0000 0.0000 0.1725 0.7170 0.71440 0.7440 0.7440 0.7440	0.000 0.000 0.0000 0.0000 0.1945 0.3516 0.4543 0.7475 0.7475 0.7475 0.7459	125.89 (2.1) 0.0000 0.00000 0.1133 0.1133 0.5695 0.66993 0.7505 0.7435	156 166 166 166 166 166 166 166	00000000000000000000000000000000000000	1 1	316.24 316.24 11 (2.43) 12 (2.43) 13 (2.43) 13 (2.43) 13 (2.43) 13 (2.43) 13 (2.43) 14 (2.43) 15 (2.43) 16 (2.43) 17 (2.43) 18 (2.	5.69 6.11 6.69 6.00 6.00 6.00 6.00 6.00 6.00 6.00	501.19 (7.7) (7.7) 0.00000 0.0000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.000000	630,96 (2.8) 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	744.33 1400.00 1258.93 (2.9) (3.0) (3.1) 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.5245 0.2637 0.271 0.62795 0.2637 0.271	75 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9
07.80		0.8950	1.0000	0.9111	0.9192	0.9273							1.0000
01.al 78.72			0000	0000		90000							

Table J.7. Performance data for FDC crew: computer,

													-		
1 1 1 1 F	UASE	LOGIDOSE						11ME 68	GRID LINES	(HRS)			•		
		•	0°50 (-u°1)	0.25 (-0.6)	6.32 (-0.5)	(-0.4)	0.50	0.63	6.79	1.00	1.26	1.54	2.00	2.51	3.16
91	4529.03	3.0	1.0una	1.0600	4608.0	0.6263	•	0.3635	270	7	0.1578	S	550	9	0.000
-	5514.14	4,2	3000	1.000	5		0.7673	0.7320	0.7.18	0.6380	0.5695	0.5398	0.4907	0.4079	0.337
<u>.</u>	2729.55		3.00c.	1.000	1.0000	9696.0		0.7616	.745	÷.	0.6457	~	562	٩.	0.458
<u>.</u>	2119.41		3.000	1.0000	2000.	1.0000		0.7918	.767	۲.	2684.0	_	514	ĸ.	0.535
7 1	1544.72		300°.	2000.	5	7000.	1.0000	C 9442	787	۲.	0.7245	•	544	T.	0.602
7 :	17.9761		3030.	3000	1.00°	1.000	•	1.0000	. A 50	۲.	0.7543	_	276	٠.	0.645
2:	40.00		0000.	1.000	0000.	0000	1.000	1.0000	Ş	∝.	0.7635	. А	20	٠.	0.568
= :	A		3030.	•	3000-	2000	1.0000	1.000	•	•	0.9007	~ 1	0,7623	٦.	0.700
2 0	967 540		2606	3000	3636.	30.0	3030.	3030-1	د د د د	••	1.0000		561	٠.'	0.732
* *	7 0						0000.	0000.	5 6	•	3000.	•	7 0	`.'	10.0
-	77.07	, c					2000.	0000		•	0000	9 6	5		961.0
	21.4.4	25.								> <		3 8		٠, ٩	1000
	104.40	2.43	0000			2000				: 0		3 6	3 8)	
4	150.64	۲۰۰۷	1.0000	1.000	000	1.000	2000	0000-	1.900	0000	0000	0000	1.000	? =	1.000
~	101.11	2.01	1.0000	1.0000	500	1.000	1.000	2000-	000	C	1.0000	3	000	000	0
V	-	u6.1	1.000	2020.	900	1.0000	1.0000	1.000	500	c	1.0000	3	3	1.0000	9
-	01.11	1.79	1.0000	1.000	1.000	1.0000	1.000	3	90	1.0000	1.0000	3	000	90	1.000
												•			
CRIO								TIME	101	CSONJ					
LINE	いりらげ	LAGIUMSE						5	1 E 1	•					
	,		3.94	š	ġ	~	10.00	~પ	Š	2.0	5.1	-	39.81	_	3.1
			ر ۲۰۰۸)	r. n. 7.	(o . t)	(6.0)	(0.1)	1.1	(3.1)	(1.3)	(1.4)	(1.5)	(1.6)	(1.7)	f
2	4569.03		0.000	0.0000	90000	0000	•	90000	00000		9	0.000	90		0.000
-	3516.14		A PBAB	0.2145	0.263b	0.22Ab		0.1923	0.192		-	0.1737	5		0.092
2	2729.55		0.4274	1417.0	9645 0	0.7605	•	0.2367	0.244		'n.	0.2591	818	٠,	0.202
<u>.</u>		3, 57	0.5260	0.4692	2010.0	0.3325	•	0.2814	0.25		<u> </u>	0.3447	528	٠.	0.335
	1048.76	2.67	2.00°C	8215°	96/97	2.00	•	122.0	0.367		ď.,	0.4546	9 . 2 :	٠,٠	200
2	40,170	200	6.6674	0.654.0	1819	0.47.00 87.78	•	1074			, r	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	6 4	•	70.0
	7000	2.87	5.6793	0.6770	0.6598	0.6390		0.5765	0.544			0.4200	673	٠.	0.768
2	497.16	2.78	0.7070	1264.0	0.6069	0.6776		9.6459	0.65		•	0.7009	733	Г.	0.788
~ (40.4.54	Z. C.	0.7332	0.71.46	2010	4107.6		0.6719	9.6		٠,	0.7097	154	٦.	0.003
• -	34° 50' C		957.0	0.7545	0.727	0.7146	•	0.6969	Ž;		٦,	0.7227	17.0	٠.	0.9
- 4	78 410	Ç 5	C = 0 = 0	0.1040	7.7515	9517.0	•	102/-0	7.5		~"	0.1375	8 7 6	•	0.015
· •	169.40		0.0480	0.8578	2000	9656	•	1277				0.000	7 0 7 0	•	
•	150.64	2-2	3030.	0.0472	9086	0.9658	0.7737	0.8273	- C	0.9126	0.9578	9.52	. 20	000	1 000
~	101.nl	2.0	3.30.0	7070.	0.95T	0.8828		0.8947	9		٠.	1.0000	9	٠.	1.000
~	18,72	es. 1	1.augu	1.060	1.0000	0.9612		0.9831	3.00		٠.	1.0000	2	٠.	1.000
-	11.14	1.79	1.000	1.0000	1.0000	900.	•	1.0000	1.040		1.0000	1.0000	000	9	1.000

Table J.7. Performance data for FDC crew: computer (Concluded).

and the second s

1117 1118	ษกน	Ln6 (6/13E)						TIME GR	GRID LINES	(HRS)					
			79.43	100.00	175.89 1	56,40 (2,2)	99.53	251.19	516.43 (2.5)	396.11 (2.6)	501.19	630.96	194.33 10	794.33 1000.00 1256.93 { 2.9} { 3.0} { 3.1}	56.93
19	4529.93	3.04	0.000.0	ď	0.000	0.000	0.000	0.000.0	0.0003	0.000	0.000	0.000	0.000	0.000	9000
-	5516.34	۶۲.۶	1550.0	ė	0.000	0.0000	0.000	_	0.0000	0000		0.000.0	0.000	0.000	0000
9	2729,55	3.44	0.1065	ċ	PAU0.0	0.000	0.0000		_	000000		0.000	0.000	0.000	0000
-	2114. M1	5.31	4114.0	0.1608	0.0948	6180.0	0.000	٠	_	000000	0.000	0.000.0	000000	000000	2000
J	1644.72	5.4.¢	0.4919	ċ	0.2591	0.2326						000000	0000-0	000000	000000
~	12/4.71	5.11	0.7013	ċ	0.4416	1285.0							0000-0	000000	2000
~	40°140	2.00	0.7918	ċ	0.6265	0.5469			0.4072		0.0000		0000-0	0.000	000000
= :	769.	69°7	4141	e.	0.7028	0.7533							000000	000000	0.000
2	557.10	£.18	0.9012	ċ	0.A142	0.8128							0.5209	0000	0.000
T	403,54	4.67	0.8048	c.	0.4115	0.8108							0.6549	0.3247	0.0514
10 1	54.067	ک. ع ا	0.A117	Ċ.	0. AU96	4004							0.7039	0.5555	0.2716
~	12.0/2	2.45	C. A157	¢	0.8000	0.8095							0.7541	0.6575	0.4458
۰	716.AL	۲.54	Rolle U	ċ	0.8170	0.8171							0.7982	0.7192	0.6230
'n	169.70	د. د۶	6616.0	Ġ	0.9325	P. 95A5							0.9833	0.9882	1.0000
J	\$ 50.64	۲.12	1.000	-	1.0000	1.0000							1.0000	1.0000	1.0000
M	10.101	۲۰۰۷	1.0000	-	1.0000	1.0000							1.0460	1.0000	1.0000
N.	18.72	٠٠٠	1.0000		1.0000	1.0000							1.0000	1.0000	1.0000
	11.10	1.79	1.0000	<u>.</u>	1.0000	1.0000							1,000	1,000	10000

Table J.8. Performance data for tank crew: tank commander.

	GP 15	4 	į						TIME GRI	TIME GRIN LINES	(HRS)					
	Ė	1000	Loctorist	0.20	(9.0-)	0.32 (-0.5)	(0.40)	0.50	0.63	(1.0-)	1.00	1.26	1.58	(6.00)	2.51 (0.4)	3.16
	2	4529,03	3.uh	1.0000	-	0.8049	0.5265		0.3635	٠,	46	2		0.0535	0.0237	000
	- 1	3516.74	8.55 5.55	1.0000	0000	<u>-</u>	0.8412	A .	Λ:	0.5579	64:40	0.3825	0.1576	0.3133	~ "	20000
	0 1	Cr. 02/5	, to		200		70.00	1074	200	0.0454	7 0	4.0	42120	0.27.17	3605	0.4551
	7 7	1644 72	2	2000	2000	-		1000	415	30.00	0.7567	9	0.5695	0.4693	. 7	
	~	1276.71	3,11	0000	200	: <u>-</u>	0000	9000	000	0.8640		~	0.6265	0.5230		c
	7	40.160	5.00	1.0000	1.0000	_	1.0000	•	0000	1.0000	7	9.	0.7468	0.6589		ė
	=	169.29	5.89	1.0000	1.0000	_	1.0000	1.0000	1.0000		S	Œ.	0.8022	0.7558		-
	2	597.10	۲,14	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0006	1.0000	0.8814	9 5		ċ
	ا	464,64	2.07	1.0000	1.0000		50	1.0000	1.0000	•	000	0	1.0000	E (e (
	2 0 1	359.02	۶. 54 ا	3.00.0	1.0000	1.0000	3.000	3000-	1.0000	1.6000	1.000	0	1.0000	> 9		-
			٠. ٠.	2000	0000	0000.	1.00.00	1.000	0000.	•	900	•	0000.			3 6
	o u	¥. 64.	, , , ,			0000		9 6	0000	0000.	0000.					-
	7 37	37.05.	2.17	0000		: C	2000.1	1,000	9000	1,0000	0000			0000		
	M	101.41	0.0	0000	1.0000	0000	000	9 0	000	0000-1	1.0000	000	•	000	1.0000	
	1.74	18.72	05.	3000	S	000	0000-	000	1.000	0000	000	000	000	000		_
		61.11	1.79	1,000	_	1.000	9	9	000	1.0000	50	1.0000	1.0000	1.0000	1.0000	1:0
2.5	GRID								TIME GR	ID I INFS	(HRS)					
6	LINE	JUNSE	COCCOUSE)													
				3.48	5.01	6.31	1.94	16.00	12.59	15.85	19.95	25.12	31.62	39.61	50.12	63.10
				(0.6)	(0.7)	(0.A)	(5°U)		=======================================	-	(1.3)	-	(1.5)	(1.6)	_	-
	2	4529.93		0000.0	00000	0.000.0		0.000	0.000	0.0000	0.000	0.0000	0.0000	0.0	•	9
	13	3516. 14		6.1383	0.0911	5601.0		2410.0	0.0085	0.0096	0.0705	0.0719	0.0647	•		0.0283
	2 :	2729.55		2.2545	0.1967	0.172B		*660.0	0.0913	0.0440	0.1068	0.1121	0.11.4			
	<u>.</u>	211P. P.		5 744G	2.07.0	0.7286		0.1202	0.1142	0.1646	36.46.00	0.1020	11.0	5 0	•	
	? :	2/* 7/6		*****	2000	C 102 0		20.0	1010	2222	20000	0.4176	0.3672		•	
	2	30,170	, co	0.4777	0.4523	9696	Br. 44.0	0.2/37	0.2534	0.2625	0.3179	0.3540	9.345.0	0.4321	0.5723	0,6951
	7.	700.29		0.5374	4605.0	D. 6784		0.4010	0.3853	0.4200	0.4550	0.4886	0.5230	9.	•	
	2	547.10		1604.0	P-1104	6.5493		9115.0	0.4909	9.5171	0.5498	0.5819	0.6190	0	•	
	•	45.50		0.6824	0.6284	0.5025		0.5625	0.5363	0.5374	0.5598	0.5964	0.6374	0	•	
	3 0 ^	329, 628		0.7448	0.6619	0.6411		0.5960	9.5674	2672.0	9665.0	1959.0	2000	0 0		
	- 4	76 417		79.8.0	727.0	0 0 0 0		0.0044 0.6148	1080.0	0.7308	0.7761	0.8421	0.6191			
	ı ısı	164,40		0.9471	0.8641	0.7872		0.7086	0.7638	0.8109	0.8547	0.8853	0.8982			
	4	153.64		1.0000	0.9495	0.4775		0.7822	.839	0.8868	0.9323	0.9657	0.9170	ċ	1.0000	
	M	101.41	~	1.0000	1.0000	0.9636		1 6 2 9 3 4 1	٠.	0.9641	1.0000	1.0000	1.0000	_	1.0000	
	~ .	18.76	06.1	1.0000	1.0000	1.000	987	9616.0	•	1.0000	•	0	0000	_	1.0000	000.
		61.11	1.19	3.00.	3030°	1.000	1.0000	1.000	-000	0000.1	.0000	•	.0000			:

Table J.8. Performance data for tank crew: tank commander (Concluded).

6818 LTGF	nusE	しいら (ひの3長)						TIME WA	WRID LINES	(HRS)		•			
			74.47	100.60	125.69	150.49	164,51	251.19	516.23	398.11	501.19	630,96	194.33 1	000,000	258.93
				e. ~	(2.1)	(د.ح)	(2.3)	(2.4)	(5.5)	(2.6)	(1.5.1)	(2.8)	(2.9)	(2.9) (3.0) (3.1)	(3.1)
9	4569.95	5.66	20000		2000.0	ם ייטיים	0000	0000	9	9		•	•		
~	3516.34		0.0177		_	0.000								00000	0000
4	2769,55	•	0.0775		0.0020	0.0000					00000	00000	00000	00000	0.000
<u>.</u>	2119.01	·	0.1002			1000			>	3000		00000	0.000	0.00.0	0.000
7	1644.76		70.0						0000			0000.0	9000.0	0000	0.000
-	1276 71					0.11.7			20000	0.000		0.000.0	0000.0	0.000	0.000.0
2 0					_	0.25.0			0.0325	0.00.0	0.000	000000	0.000	0.000	0.000
<u>.</u>	70.07		5///		_	0.5529			0.2524	0.1579	0.0000	000000	0.000	0.000	0.000
= :	, O ,	•	さんりょ。 0		_	0.7489			0.5717	0.5242	0.4905	0.0769	0000	0000	5000
2	347.10	-	0.4123		_	0.8322			0.7732	0.7586	0.6513	0.4275	0.3510		
σ.	40 4 44	•	0.A20b		_	0.8213			0.7815	0.7695	0.7413	0.6540	2000	25.45	4
3 0	429° P.	Ī	6.9205		_	0.8122			0.7901	0.7817	0.7858	0.77.09	0.6785	20.17	27.6
_	770.11		0.A378	0.8276	n.8224	0.A179	0.A145	0.A149	0.4107	0.8064	0.8232	6154	0.7544	4054	2000
۰	714.AC	Ī	0.8464		_	3 A 4 A B			0. A534	0.8553	0.8607	9.00	9770	40% C	2004
'n	168,10	-	1650.0		_	8676.0			0.9067	0.9722	0.9776	0440	9440	2000	2000
#	150.64	Ī	1.0000		-	1.0000			1.0000	1000					
~	101.01	_	1.0000		-	0000					0000	0000	0000	3535.	0000.
^	7 R 7		2000						0000.	0000	1.0000	2000.	1.0000	1.0006	1.0000
٠.									3.000	1.0000	1.0000	1.0000	i. 3000	1.0000	1.0000
•	•	-	••••			2000			1.000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000

Table J.9. Performance data for tank crew: gunner.

	1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	LTUF DO:	Nuse LnG(Unse)	v2•0	ے ع م	. 45	c. 40	95.0	11ME 6H	U.OT U.79	_	1.26	1.54	2.00	2.51	3.16
941-2-3 J. S. 1.0000 1.	\$\frac{1}{2}\frac{1}\frac{1}{2}\f			(-v-)	(-v. h)	(-0-2)	(-0-4)	(-U-J	(-0-5)	(-0-1)		C 9 . C	(2.0)	6.3	(0.0)	(5.0)
			77 S	1.000	1.0000	4604.0	0.4465	0.4600	0.4045	0.2706	1961.0	0.1378	9060.0	0.0575	0.0237	000
					2000		4 C C C C	707K-0	0.7675	2.54.0	1085.0	0.5244	5047	0.4510	1655.0	0.26/4
1744-7.7 3.42 1.0000 1	1744-7.7	•		0000	20.0.	2000	7070	9.564	0.0646	20.00	0.7615	0.6770	067.9	2000	- C- C- C- C- C- C- C- C- C- C- C- C- C-	5034
176,71 3.11 1.000 1.000 1.000 1.000 1.000 1.000 0.0010 0.925 0.525 0.553 0.5752 0.5752 0.5752 29,70 2.40 1.000 1.000 1.000 1.000 1.000 1.000 0.000 0.917 0.5752 0.5	176.7.1 1.10 1.00 1.00 1.00 1.00 1.00 1.00 0.945 0.7515 0.6734 0.6737	_	2	1.0000	1.0000	1.000	1.000	1.000	1496.0	0.8574	0.9037	0.7438	90,49.0	0.5950	0.5503	0.5560
99,174 2.40 1.0000 1.0000 1.0000 1.0000 1.0000 0.9179 0.6552 0.7512 0.7552 0.75	947,174 2.47 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 0.9179 0.6545 0.7512 0.7512 0.7512 0.7513 0.7	_	7	1.0000	۲.	3000-	1.0000	1.0000	1.0000	3444.0	0.8460	0.8016	0,7255	0.6434	0.6024	0.5927
759,75	79.27 2.44 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 0.9194 0.7558		~ T	1.0000	٩.	Jano.	1.0000	1.0000	1.0000	1.0006	0.9426	0.8348	0.8154	0.7512	_	0.6261
79-71	97.7.6 2.74 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 0.9172 0.5257 1.0000 1.0000 1.0000 1.0000 1.0000 0.9172 0.5257 1.0000 1.00		73 ·	3000 ·	ę.	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	0.9179	0.8545	0.9193	_	0.6990
### 1, 1000 1,000	40.5.74 2.5.6 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 0.9944 0.9957 2.5.6 1.0000 1.0000 1.0000 1.0000 0.9944 0.9957 2.5.7 2.5.4 1.0000 1.000		2	1.0000	۹.	1.000	3000.	1.0000	1.0000	1.0000	3000.	1.0000	0.9119	0.8696	_	0.7662
199, 12 2.34 1.0000 1.0	75,71 2 2.54 1.0000 1.0		.	2000	e.	1.0000	3000.	1.000	1.0000	1.0000	1.0000	•	1.0000	0.9172		0.8164
77,9-71 2.45 1.0000 1.0	775-71 2.45 1.0000 1.00		~	5	1000.	1.000	1.0000	3000.1	1.0000	1.0000	1.0000	000	1.0000	9446.0	_	0.8660
1,	1,	ñ.	۲.	S	1.0000	1.0000	J.nun.	1.0000	0000.	1.0000	1.0000	000	1.0000	1.0000	_	0.9168
150, 4 2.15 1.0000 1.00	150, 4 2.15 1.0000 1.00		2	2	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	900	1.0000	1.0000	0000	0.9730
190.4 2.17 1.0000 1.000	1915.44 2.12 1.0000 1.0		3 05.	5	1.0000	1.0060	1.0000	1.000	1.0000	000	1.0000	000	1.0000	1.0000	000	1.0000
101-31 2.01 1.0000 1.00	101.24 2.01 1.0000 1.00	-	.	ç	1.0200	1.0000	1.0000	1.0000	1.0000	90	1.0000	000	1.0000	1.0000	1.0000	1.0000
78.72 1.90 1.000	78.72 1.90 1.000		~u	90	1.0000	Ş	1.0000	1.000	1.0490	000	1.0000	900	1.0000	1.000	1.0000	1.0000
UNSE LAGIUNSE) 3.94 5.01 6.31 7.94 10.00 12.59 15.65 19.95 25.12 31.62 39.81 50.12 6 7.7 (### 1.79 1.0000 1	6 .	.72	Ş	1.000	9	1.0000	1.000	3000	000	500	000	1.0000	1.0000	1.0000	1.0000
#\$\text{TIME GPID LINES (HRS)}\$ 3.94 \$5.01 \$6.31 \$7.94 \$10.00 \$12.59 \$15.65 \$19.95 \$5.12 \$11.62 \$9.81 \$0.12 \$6.12 \$1.65	### PACE CALCIONSE) 3.94 5.01 6.31 7.94 19.00 12.59 15.65 19.95 25.12 31.65 39.81 50.17 6.60 (0.61) (0.61) (0.69) (0.99) (1.10) (1.1) (1.2) (1.2) (1.5) (1.6) (1.7) (1.7) (0.69) (0.99) (0.69) (0.99) (1.10) (1.1	6	:	500	1.0000	000	1.0000	1.000	1.000	000	900	000	000	1.0000	1.0000	1.000
### CAPTIONSE 3.94 5.01 6.31 7.94 10.00 12.59 12.65 19.95 25.12 31.62 39.81 50.12 6.45	### CALCHUSE) 3.94 5.01 6.31 7.94 10.00 12.59 15.65 19.95 25.17 31.67 39.81 50.17 6 1.7) 7 7 7 7 7 7 10.8 7 10.00 17.10 7 1.2) 7 7 7 7 7 7 7 7 10.8 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7															
3.94 5.01 (0.8) (0.8) (1.0) (1.1) (1.2) (1.3) (1.4) (1.5) (1	3.94 5.01 6.31 7.94 10.00 12.59 15.65 11.95 (1.3) (1.3) (1.5		3.00.7.00						TIME GR	ID LINES	(HRS)					
4529-75 3.66 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.000	4520.73 3.66 0.00000 0.00000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000			σ,	5.01	6.31	1.94	00.01	- ru	74,45	3	25.12	31.62	39.81	50.12	63.10
4529.75 3.66 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	4529-05 3.66 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.000			=	=	0	(6.0)	6.	-	-	-	(1, e)		9.	(1.7)	6.1.
5516.74 5.55 0.1971 0.1267 0.1766 0.1105 0.0948 0.0948 0.1502 0.1525 0.1539 0.1643 0.1649 0.1564 0.2567 0.2578 0.1643 0.1649 0.1562 0.1552 0.1539 0.1643 0.1649 0.1564 0.1562 0.1552 0.1539 0.1643 0.1649 0.1649 0.1564 0.1564 0.1568 0.1568 0.1568 0.1568 0.1568 0.1568 0.1568 0.1568 0.1568 0.1648 0.1568 0.1	5516.74 3.55 0.1971 0.1267 0.1591 0.1766 0.1306 0.1978 0.1978 0.1043 0.1978 0.1043 0.1978 0.1043 0.1978 0.1043 0.1978 0.1	0 1/2 18	\$ 6	000	•		0000	9	90	•		9000	9	9	9	9
2720.55 3.44	2729.55 3.44 0.3664 0.2654 0.1766 0.1462 0.1506 0.1552 0.1525 0.1539 0.1643 0.1645 0.1644 0.2659 0.278 0.263 0.1643 0.1644 0.263 0.214 0.2269 0.2278 0.263 0.1643 0.1644 0.263 0.214 0.2269 0.2278 0.263 0.1643 0.1644 0.263 0.264	3516	4	, ,	9		0.1490	5011.0	0.0944	4 70 0	1470-0	0.0946	0.0811	0	0.0594	0.070
2114.41 5.37 0.5021 0.4453 0.3405 0.2247 0.1181 0.1668 0.1665 0.2063 0.2114 0.2259 0.2578 0.2578 0.2638 0.2578 0.2659 0.2578 0.2659 0.2578 0.2659 0.2578 0.2659 0.2578 0.2659 0.2578 0.2659 0.2659 0.2578 0.2659 0.2578 0.2659 0.2	2114.41 5.37	2760	, t		0.7841		0.1766	0.1442	0.1500	0.1398	0.1502	0.1525	0.1539	164	0.1469	0.1115
1644.72 3.22 0.5693 0.541 0.4027 0.7583 0.2415 0.2517 0.2655 0.3214 0.3531 0.3466 0.4250 0.5567 0.5815 0.5999 0.5797 0.4654 0.3584 0.3187 0.3629 0.4260 0.4264 0.5267 0.5815 0.991.04 3.00 0.5417 0.5639 0.56	1644.72 3.22 0.5693 0.5731 0.9027 0.7539 0.2315 0.2517 0.2655 0.3214 0.3531 0.3546 0.4250 0.3547 0.5557 0.3567 0.3567 0.3567 0.3667 0.3671 0.3629 0.3567 0.5681 0.5409 0.5740 0.5740 0.5740 0.5740 0.5740 0.5740 0.5740 0.6741 0.6	Z114	=		0.4453		1025.0	0.1781	0.1668	0.1865	0.2063	0.2114	0.2269	0.2578	c	
1216.71 5.11 0.5999 0.5797 0.4654 0.7584 0.7194 0.3167 0.3167 0.4260 0.4724 0.5267 0.5815 0.4104 3.00 0.5107 0.5495 0.4633 0.4633 0.4634 0.5124 0.5249 0.5175 0.4979 0.5400 0.6723 0.7029 2.60 0.6517 0.6549 0.5175 0.6549 0.5711 0.6547 0.6547 0.6547 0.6547 0.7123 0.4839 0.7723 0.7839 0.7723 0.7839 0.7723 0.7839 0.7723 0.7849 0.7849	1216.71 5.11 0.5999 0.5797 0.4654 0.7584 0.7194 0.7194 0.3167 0.3629 0.4260 0.4724 0.5267 0.5815 0.4713 0.7194 0.5177 0.5410 0.6723 0.4573 0.4573 0.4573 0.5177 0.5412 0.5247 0.5579 0.5410 0.6773 0.7123 0.7	1644	.72	•	0.5331		0.2829	0.2415	0.2315	0.2517	0.2055	0.3214	0.3531	0.3966	o	
941.04 3.00 0.6107 0.5453 0.4633 0.3719 0.3724 0.3786 0.4111 0.4275 0.5409 0.5400 0.6723 0.7623 0.7697 0.5400 0.6723 0.7697 0.5400 0.6713 0.7697 0.5400 0.6713 0.7697 0.5400 0.6713 0.7697 0.5400 0.6713 0.7697 0.7723 0.7697 0.6713 0.7723 0.7697 0.6713 0.7723 0.7723 0.7723 0.7723 0.7723 0.7723 0.7723 0.7723 0.7723 0.7723 0.7723 0.7723 0.7723 0.7723 0.7723 0.7723 0.7723 0.7723 0.7723 0.7646 0.6777 0.6843 0.7723 0.7646 0.7723 0.7646 0.7723 0.7646 0.6777 0.6843 0.7723 0.7646 0.7723 0.7646 0.6777 0.6843 0.7723 0.7646 0.7723 0.7646 0.7723 0.7646 0.7772 0.7723 0.7646 0.7772 0.7777 0.7723 0.7646 0.7772 0.7772 0.7772 0.7772 0.7772 0.7772 0.7777 0.6772 0.77	941.04 3.Un 0.6107 0.5415 0.553 0.463 0.3719 0.3746 0.3746 0.4171 0.4375 0.5400 0.6723 0.7030 0.5470 0.5470 0.5579 0.5579 0.5470 0.6713 0.7030 0.7050 0.6713 0.7050 0.5470 0.6713 0.7050 0.5470 0.6713 0.7050 0.6713 0.7050 0.6713 0.7050 0.6712 0.7050 0.6712 0.7050 0.6712 0.7050 0.6712 0.7050 0.6712 0.7050 0.6712 0.7050 0.6712 0.7050 0.6712 0.7050 0.6712 0.7050 0.6712 0.7050 0.6712 0.7050 0.6712 0.7050 0.6712 0.7050 0.6712 0.7050 0.6712 0.7050 0.6712 0.7050 0.6712 0.7050 0.6712 0.7050	1216	.71	•	1615.0		0.4545	9.3067	1562.0	0.3147	0.3629	0.4260	0.4724	0.5267	Ċ	ė
769,24 2.89	769,24 2.89	70	٠ خ	•	2165.0		0.4633	0.3719	4624	0.3748	0.4171	4744.0	0.4979	0.5400	ě	•
547.16 2.78 0.7056 0.6416 0.6512 0.6531 0.6534 0.6550 0.6457 0.7169 0.7169 0.7723 0.6389 0 0.84716 2.27 0.7169 0.7169 0.7123 0.6389 0 0.84716 0.7169 0.7169 0.7169 0.7123 0.6389 0 0.84716 0.7169 0.7169 0.7123 0.6389 0 0.8472 0.8472 0.8472 0.8472 0.71111 0.71111 0.71111 0.7111 0.71111111111	547.16	769	2	•	0.6548	6.5043		0.5125	1406.0	0.5226	0.5579	0.5711	0.6241	0.6713	e	0
7674 2.67 6.7676 6.7170 6.6986 6.7614 0.7016 0.6986 0.6517 0.6972 0.7329 0.80105 0.8725 0.7014 1.701	7574 2.67 6.7679 6.7120 6.6946 6.6410 6.6441 6.6972 6.7329 6.80105 6.8125 6.723 6.724 6.247 6.6441 6.6972 6.7329 6.80105 6.8125 6.724 6.725 6.724 6.725 6.724 6.725 6.724 6.725 6.724 6.725 6.725 6.724 6.725 6.724 6.725 6.724 6.725 6.725 6.724 6.725 6.724 6.725 6.724 6.725 6.724 6.725 6.724 6.725 6.724 6.725 6.724 6.725 6.724 6.725 6.724 6.725 6.724 6.725 6.724 6.725 6.724 6.724 6.725 6.724 6.724 6.724 6.724 6.724 6.724 6.725 6.724 6.724 6.725 6.724 6.725 6.724 6.725 6.724 6.725 6.724 6.725 6.724 6.725 6.724 6.725 6.724 6.725 6.72	247	4	•	0.6816	9794.0	A.6312	0.6531	0.5077	0.5249	0.6550	0.6857	0.7169	0.7723	0	-
359, 2.56 0.814 0.765 5.7406 0.7214 0.7076 0.6541 0.6961 0.7503 0.7646 0.8287 0.6843 0.794-2 2.56 0.8287 0.8887 0.8889 0.8870 0.8870 0.8870 0.8870 0.8870 0.8870 0.8870 0.8870 0.8870 0.7871 0.7877 0.6870 0.8870 0.78870 0.78870 0.78870 0.78870 0.8870 0.8870 0.8870 0.78870 0.78870 0.9870 0.9	599.62 2.56	404	3	•	0.7259	0.7120	0.6980	0.6812	0.654	0.6449	0.6641	0.6972	0.7329	0.9005	ē	•
7.3.1 6.4.4 0.744 0.7545 0.7575 0.372 0.7442 0.7717 0.7477 0.6570 0.6570 0.8870 0.77.1 6.6570 0.6570 0.8870 0.75.1 6.6570 0.6570 0.8870 0.75.1 6.6570 0.8870 0.8870 0.8870 0.8870 0.8870 0.8870 0.8870 0.8870 0.8870 0.8870 0.8870 0.8870 0.8870 0.8870 0.8870 0.8870 0.8870 0.9870	71.1 2.4	5 (5) (8) (N .	•	0.7655		0.7214	0.7076	6.555	0.6841	0.6981	0.7503	0.7646	0.8287	•	=
		672	= :	•	201.0		0.7.576	0.7243	0.7372	0.7492	0.7717	0.7977	0.6212	0.6270	ē	-
150.44 2.17 1.0000 0.9584 0.9491 0.851 0.8550 0.8566 0.902 0.9291 0.9333 0.9384 0.9435 0.9350 1.0000 1.0000 0.9938 1.00000 1.00000 1.00000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0	150.44 2.17 1.0000 1.0000 0.9417 0.9417 0.9450 0.8550 0.85540 0.9402 0.9291 0.9333 0.9384 0.9435 0 150.44 2.12 1.0000 0.9424 0.9450 0.9571 0.9971 0.9	٠.	V :	•	0.4574		0.7439	0.7489	0.7784	0. A1 3.5	0.8452	0.8651	0.8778	0.8452	o ·	•
130.44 2.17 1.0000 0.4524 0.9090 0.8571 0.9070 0.8140 0.9143 0.9534 0.9822 0.9856 0.9956 1.0000 1.00	130.44 2.17 1.0000 0.4524 0.9090 0.8571 0.9070 0.8140 0.9143 0.4534 0.9822 0.9938 1.0000 1.00		2 -	•	1878			0.7876	Ş.	0.5566	2005	0.9291	0.9333	0.9384	e .	C
1,000 1,000 1,000 1,000 1,000 1,000 0,450 0,450 1,000	1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 0.457 0.4575 1.0000 1.0	1 20	4.	•	9654			9.6402	30 :	0.9105	0.9534	.986	0.9880	0.9938	1.000	_
.1 0000 1.0000 1.0000 1.0000 0.940 0.940 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000		5 ;	(•	0000.			0.000	٠	0.9745	1.000	ē	1.0000	1.0000	1.0000	1.0004
	1. 10 00 1. 0000 1. 0000 1. 0000 1. 0000 1. 0000 1. 0000 1. 0000 1. 0000 1. 0000 1. 0000 1. 0000 1.		7	•	2000.	2000	•	٠.	٠	٩.	000	Ģ	1.0000	0	9	3000

Table J.9. Performance data for tank crew: gunner (Concluded).

C109								TIME OF	LPID LINES	(5,85)					
	200	Lic (1925)													
			19.44	100.00	175.89	150.40			510.23	30K		40 054	7.4 27		***
			(1.%)	(5.0)	(2.1)	(2.2)	(2,3)	(2.4)	(2.5)	(3.6)	(7.7)	(2.A)	(6.6)	(2.9) (3.0) (3.1	(3.1)
2	4529.03	3.64	0.00.0	4000								;			•
17	4516.34	5	C 210 0							3000	9.00.0	0.00.0	0.00.0	•	0.000
			9. 1.		0000				0000.0	0000	0.000	0.000.0	0000	•	9000
9 :	6,64.43	7.4	0.0793	20.00	9.00.0				0.000					•	
·5	2114.01	5.53	0.2041	0.1003	0.451							00000		•	0000.0
7	1644.72	27.3	A A 2 2 0	4000					3.000	20000	00000	0000.0	0.00.0	•	0.000
	10 7/61				A 0 4 1 0 0				9.96.0	000000	0.000	0000.0	000000	_	9000.0
•		2.1.	2.1.2	0.1453	2.20.0				0.0502	O. Cuna	9080	0000	0000	•	
2	\$ C. F.	2.00	A 505	0.7541	0.6484				1762	40				•	
=	760,29	68.5	0.8641	0 A55	A A > C a				1016 00	Vac	0000	0000.0	00000	_	0.000
9	547.16	2.78	0 8728	*****					9.5.0	9069.0	0.6109	4400	0.000	_	9.000.0
7	46 54	74		****	J. 00 .	1	i	1	0.0019	0.8614	0.1723	0.5527	0.4658	_	0.000
* *	45.0	;		2000	3 0 0 C				0.4613	0.8017	0.8467	0.7807	0.6988	_	0.0914
-	210.16		9574	3. 36.40 3. 36.40	1414.0	2574.0	0.8669	0.8645	0.5004	D. Abil	0.8730	0.8641	0.7867	_	0.2716
			0.44.0	0158.0	0.4/75				0.8096	0.8123	0.8885	O. Adab	0.8335	_	0.4450
ני כ	4	F. 54	2 × 6 × 6	0.3440	0.4443				0.8481	1668.0	1006.0	1506-0	0.8804	•	90040
٠.	200	, v. v	\$ 425¢	1956.0	9000.0				0.976B	0.9807	2010	440	4	•	
7	150.54	۲.15	2000	2020.	1.0000										2000-1
M	101.41	77.01	1 0000							3000	2000.	3000.	2.000	_	1.0000
n)	78.72	5							3.00.	3000	1,000	1.0000	1.0000	_	1.0000
-									1.0000	3.000	1,0000	1.0000	1.0000	_	1,000
•	-		333.	2006.	3535				1.0000	1.0000	1.0000	1.0000	1.000	1.0000	1.0000

Table J.10. Performance data for tank crew: leader.

67.17 L 14F	U.O.O.O.O.O.O.O.O.O.O.O.O.O.O.O.O.O.O.O	136000		,				TIME 6R	TIME GRID LINES	(HHS)					
			0.20 (-0.1)	ار ده. ها (۱۵.۴)	0.52	1-0-40	0.50 (-6.3)	U.63 (-0-5)	0.79	1.00	1.26	1.58 (0.2)	2.00 (0.3)	(0.4)	3.16
87.	4560,03 5516,74		1.0000	1.0000	1.0004	0.6265	c c	0.3635	0.2706	0.1967	0.1378	0.0909	0.0545	0.0247	29
2 -2	C118, 81					94479		0.7174	4677	0.5510	4. R	0.4011	0.5122	1952.0	0.2490
7	1646.72	5.25	1.0000	1.00.	0000	0000	-	0.9431	1712	. 3	٠.	0.5195			36
- 5	1774.71		1.0000	1.00.0	0000	1.0000	-	1,0000	0.8320	5م′	٠.	0.5762	0.4136	•	•
7	341.04	5. UD	1.0004	0000.1	1.00.09	1.000	-	00.	1.0000	.872	۲.	0.7014	0.6082	v.	447
- :	700.09		1,000	1.0000	2.00.0	1.0000	1.0000	•	1.0000	5	٠.	0.7642	0.717	œ :	563
3 1	8		0000	0000.	3000-	1.000		1.000	1.0000	0	0000.	0.8580	1661.0	- 1	-О Г
* =	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7			0000	3000	3000.		•	2000.	000	3000.	1.0000	0.30.00	- 0	500
۰ م	279.21							0000	00000	0000.	0000	0000.	9066.0	C O	
ء .	24 416						•	•						֓֞֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֓֓֓֓֓֡֓֓֡	4 30 0
'n	168, 40		2000	2000	2000	1.0000	0000	•		9000		2000		0000	
4	150.64		0000.	1.0000	1.0006	1.000	-	2000	1.000	000	2000	000	0000		
×	10.10!	٥.03	0000.1	1.0000	10000	2020.1	_	C	0000	000	1.0000	000	1,000	c	7
٦	18.72	1.90	000	1.000	000	1,0000	000	0000-1	1.0000	000	1.0000	000	1.0000	c	0
	01.11	1.79	000	1,0000	1.000	1.0000	000	1.0000	1.0000	1.0000	1.0000	000	1.0000	1.0000	000
0145								TIME GR	GRID LINES	(HRS)					
	,	75	8 7 .	3	*	50		64 61	3	45	21.70	64 15	17		_
			(4.6)	(2)	(n. R)	(0.0)	G	1.1	2:1	(1.3)	3.1	(5.1.)	(4.1.)	(2.1)	3.1.
20	\$0.6754	\$. 0.6	0.000	0000	0.000		0000	9000	5	•	0000	0000	0000	0000	9
1.	75.41.5		0.1249	0.0785	0.0027		0.0571	4840.0		0.0490	0.0493	0.0435	0.40	0.0348	0.0198
10	6769.55		0.2267	0.1093	0.1401		0.0742	0.0672	0/0		0.0773	0.0788	8	0610.0	0.0630
1,2	2114.41		0.3039	0.2600	0.1888	c	0.0913	0.0855	.05	٦.	0.1054	0.1143	2	0.1405	0.1440
7 -	1644.72		0.3443	1612.0	0.2541	ċ	0.1265	0.1230	0.1514	٣,	0.1671	0.1890	7.7	0.2366	0.3031
.	1276.71	5.11	6.3437	4664	70500	9002°0	0.1686	0.1506	0.1705	0.1942	0.2243	0.2596	0.2932	0.3410	0.4599
2 :	7.7	= °	7 7 8 ° 0	5873	0.4550	e (27.00	10.11.0	٠, ٠	Ÿ	0.6316	UC. 7		* C * C * C * C * C * C * C * C * C * C	2695.0
	67.07	70.7	2.54.0	3,400	5.11	•	0.5573	0.0167		• 4	0.3030	10050	 	0.5764	7154
*	40.104	70.2	0.6500	0.064	0.5492	6	0.4682	0.4554	7	٠٦	0.4847	0.5172	2	0.7222	7489
ນ	454.Fe	45.54	0.7068	0.6394	0,5495	c	0.5268	9105.0	0.4874	٠.	0.5202	9.5519	5.36	0.7439	0.7644
~	12.010	7.4°	2027.0	4644.0	0.6282	ċ	6595.0	0.5600	.57	v.	0.6170	0.4380	587	0.7581	0.7721
. و	214.06		0. AC 1 7	0.7415	O. FOFB	ė	1665.0	2956.0	9	٦.	0.7234	0.7412	ž	0.7723	0.7601
Λ:	10 P		4780.0	0.8414	0.7005	e (0.6583	0.7158	٠. د ز	₩,	0.8331	0.8536	~ :	0.8637	0.8947
3 ~	150.44		3030	0.44.0	4544 U	e (PS08.0	£.	٠,	9676	0.4676	96	0000	0000
~ ·	17. 10.		⋤ (3000	9,4246	e (ς.	5 3	0.9559	1.0000	0000	5	50	0000	0000
u -	7	-	0000.	0000	0000.	9 3	25/6"0	500	000	~ (1.0000	2 6		0000	1.0000
-		-	1.0000	0000.	٦.	0000.	٠.	1.000	1.0000	1.0000	1.0000	0000.	0	000	1.0000

きというとう。重要ないのできないとは重要ななのの形を出版できないのできない。

Table J.19. Performance data for tank crew: loader (Concluded).

インス 自然大学の対象を対象を行うというとのないのできることという

	(3.1)	0.00.0	0000.0	0000.0	0.00.0	00000	0000	0.000	0000.0	0.000	9.00.0	0.2710	0.4456	0.6209	1.0000	0000	0000.	1.0000	3000.
	(3.0)			_										0.7967					
	794,33 1000,00 1256.93 (2.9) (3.0) (3.1)	_	_	-	_	_		-						0.7780					
	30.96	0.000.0	0000.0	0000.0	0.000.0	0000.0	0000.0	0000.0	0.0614	0.3495	0.5654	1989.0	0.7475	0.8083	0.9768	1.0000	1.0000	1.0000	1.0000
	501.19 6	0.000	0.00.0																
(HRS)	196.11	0	0,000											0.8045					
FIME URID LINES	316.23													0.8010					
TIME LA	251.19													ナーナー・ロ					
	199.53	0.0000	0.0000	0000.0										0.7937					
	150.49	2000	0.000.0	000000	0.0273	0.0847	1941	0.4394	0.6658	0.7675	0.7415	0.7247	0.7387	0.7900	0.9508	1.0000	1.0000	3000.1	1.0000
	125.89													8.78A1					
	100.30													0.7857					
	79.45	0.000	0.0130	0.0569	0.1245	0.3218	0.5148	45050	0.7115	0.7553	0.7546	0.7670	0.7762	0.7854	1406.0	1.0000	0000	1.0000	1.0000
	LAG(UOSE)																		1.79
	nose .	4529.95	3516. 44	27.49.55	2118.AL	1644.72	12/6.71	30.150	70.007	4. (4.)	45 544	4 5 5 K	279.41	21.6. 42	169.30	130.64	101	18.72	11.10
UR 1P	Liuf	¥.	11	4		4		2	: =	: =	. 7	• 1	۰ د	- 0	ı ve	7		· ~!	l

Table J.11. Performance data for tank crew: driver,

	3.16	, ,	0.000	5 17 5	7	8 6			- 4				֡֓֞֜֝֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֓֓֓֓֡֓֜֓֓֡֓֡֓֡֓֡֓֡֓֡֓֡֓֡֓֡֡֓֡	316	2 6	2 6	9	9	000	000					•	000.	.039	126	.253	459	- 602	689	. 29	90	926	929			75.00			1.0000
	6.51 (0.4)	•	70.50		. ~	· ``	٠,	. ~	•	: -	• •		•	•	•	• •	•	0000.1	0000	1.0000				(1.7)		~	•	-	ſU	₽	₹ 1	•		- 1	ъ.			0 0		3 C) с	1.0000
	2.00 J	3,	0.3065	427	40	558	5.49	7.19					, ,			9 6		3 6	00001	000			14 97	(9,1)	•	000.	₹60•	.162	. 232	337	.437	447	065.	,,,,	77.	200	6 2 2		0.1100	000		1.0000
	1.58	60	0.4268	536	59	74	9	19.		ò	2				3		. (5 6	0000.	000				3.1		Š	3	ç	Š	9	9	_ :	5 :	6	: :	: :	: <	3 3	0.070	9	6	1.0000
	1.26		0.4528															0000	200.1	0000.			5	(4.1.)		٩.	٣.	٦.	7	•	٠,	•	Γ,	•	•	•	•	•	0.000	35		1.0000
(1145)	1.00	196	0.5087	0.6674	0.7545	0.7980	841	0.9162	1.0000	1.0000	1.0000	0000							0000	0000	(30.7)	(1143)	19,95	(2.1)		900	5	144		7	. 514								3 6	000	000	000
TIME GRID LINES	0.7a (-f.1)		4044.0	٠.	~	٦.	٠٠.	٠.	. ``	``	1.0000	1.0000	1.0000				0000			0000	341 1 61	THE LINES	χ,	(1.2)		5	2	37	5	9 1	9 4		١,		9	:	۳,	5	6006.0	=	1.0000	000
TIME UR	(5,0-)	6. 3035	4461.0	0.8070	0.8593	6.96.0	1.0000	1.0000	1.0000	1.0000	1.0000	1.000	1.0000	1.000	1.000	1,0004	1.0000			200	9	ו זיינ	12.59	===	•	=	~	٦.	٦,	•	•	•			•						٠,	
	0.50	0.440	0.8598		٠ د	- 0	1.00	-	30.1	1.00	30.	1.00		00.									- 3	(0.1.															0.8233			
1	0.40	_		_	-		_	_	_	_	_	_	_	_	_	_	_	_					7.94	(6.0)															0.8565			
	(-0.5)	0.AU95	1.0000	0000.	1.0000	? C ? C ?	1.000	1.0000	1.0000	1.0000	1.0000	1.0000	1,0000	1.0000	1.0000	1.0000	1.0000	1,000	000				15.0	(n, n)	•		4000	7,000	01424	9000	0.40.0	5000	6.65	0.6667	0.7425	0.7362	0.7079	1.8557	2406.0	0.070	1.0000	1.0000
	0.25 (-0.6)	1.0000	1.0000	2000	0000	2000	2000.	, oco	0000.	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.000				5	(2.0)	000		00310	1074 0	2000	4465	12150	0.5841	0.6541	0.7036	0.7466	0.7870	0.6290	D. A940	6090.0	1.0000	1.0000	J.0000
	0.20 (-0.7)	1.0000	2020.	0000.	0000.	9000	0000	2000.	0000.	1.0000	3000.	1.0000	3000.	1.0000	1.0000	1,000	3000	1.0000	1.0000				3.94	3.5	0000	4 7 6 6	7412	3, 1, 0	•	2005.0	0.5431				•	•	•	•	0.0	1.000	3.000.	000
LUGENUSE		3.05	, . , .	7 .			- 1 · 1 · 1 · 1 · 1 · 1 · 1 · 1 · 1 · 1	200))	, v	۲۵.۶	٦. ا	. 4.5 . 4.5	۲. 54	٤٠٠٦	۲.12		٠٤.	1.79		-	(35vn)7v7			3.66	64.	2 4 4	15.4	5.22	5.11	3.00	09.7	2.7A	2.67	2.56	N. 45	2.34	2.23	2.12	5.0	6.4	~
nuse		4567.03	# W C C C C C C C C C C C C C C C C C C	7	7	7/ 7/61	17.47.71	7 7 7		91.75	20 . A.	524. P.S	740.21	716.82	10 P . 30	150.64	101.41	18.72	-			Unse.			4529.93	-	2729.55	2118.A1	1644.72	12/6.71	991.04									1.01	`	
6810 L114F		2.																æ			CRID	LTHE			6	11				13	2	=	2	•	73	~	9	ď	3 !	v) /	u .	-

Table J.11. Performance data for tank crew: driver (Concluded).

4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	MASE LAW	LOUGHOUSE						TIME OR	URIO LINES	(HRS)					
2.44 2.44			14.47	100.00	175.89	150.49	199,53	251.19	\$16.61	394.11	501.19	630.46 (2.F)	794.33	794.33 1000.00 1256.93 (2.9) (3.1	N.
2.24 2.24 2.24 2.24 2.24 2.24 2.24 2.24		, O.A.	0.000	0.000	1000		. 0								
2.44 2.11 2.12 2.12 2.13 2.13 2.14 2.44		25.	P. 0.444	0.000							0.00.0	0000.0	9090		
2.23 2.23 2.23 2.24 2.24 2.24 2.24 2.24	_	3	0 1002	47.00				3636.6	3000.0	2000	2000	90000	3030.0	9.9096	
2.44 2.44		**					0000	30000	3000.	3000.0	0.0000	9000.0	3077.0		_
2.11 2.11 2.16 2.18 2.18 2.18 2.18 2.18 2.18 2.18 2.18			***	2011.0	57K8.		0000.0	0.0000	0.000	000000	0.000	0.0000	0.000		_
2.11 2.60 2.76 2.76 2.74 2.44			0024.0	アンパイ	0.1065		450.0	0.0065	0.000	0000	4000				
2,69 2,78 2,78 2,54 2,54 2,54 2,54 2,54 2,54 2,54 2,54			1.6.5.0	9000 U	7 4% 6		7071	411				00000			_
2,18 2,18 2,18 2,18 2,18 2,18 2,18 2,18		0 3	0 7611	46.74				6/11/0	3.0456	9090	9.500	0.00.0	9000		-
2.45 2.45 2.45 2.45 2.45 2.45 2.45 2.63 2.63 2.63 2.63 2.63 2.63 2.63 2.63		94	7001				01,710	9.1246	9052.0	0.2072	0.000	0000.0	0.000		_
2,44 2,44 2,44 2,44 2,44 2,44 2,44 2,44					40476		0.6631	0.6206	0.5865	0.5501	0.5406	0.0942	000000		_
2.55 2.55 2.54 2.54 2.54 2.54 2.54 2.54			0.11V3	1475.0	0. A 575		0.4256	0.7845	0.7702	0.7631	0.6751	0.4917	0.4372		
2.54 0.8337 2.54 0.845.5 2.54 0.95.4 2.63 0.95.6 6.17 1.0000 1.40 1.0000 1.79 1.0000		.67	D. A 300	O. A.Z.R.D	0.8248		Aug.	0 7860	77.4	7.7.					_
2.44 0.846. 2.43 0.93.8 2.43 0.95.2 6.17 1.00.0 1.40 1.00.0 1.79 1.00.0		44.	0.93.87	A 474	A LA		1010				0 1 1 1 0	7 00 0	0.3045		_
2.54 0.45342 2.23 0.45342 2.23 1.000 2.40 1.000 1.40 1.000 1.79 1.000		4	A 444.4	A 4 4 4	7			606790	0.1013	0.116	0.7864	0.1/28	6.29.0		
1.47 1.000 1 1.40 1.10 1.10 1.10 1.10 1.10 1			100		00000		7572.5	0.41.75	0.5117	0.8105	0.8311	0.4238	0.7596		
1,40 1,0000 1,40 1,0000 1,40 1,0000	•		0.00	4000	5. KUP4		2108.0	0.8640	0.8666	6.8693	0.8757	0.8747	0.8406		Ī
1, 40 1 1, 00.00 1, 40 1 1, 00.00 1, 40 1 1, 00.00		\$ V *	2454	5170.0	0.9475		3,9500	0.9645	9699	0.9751	4040	0.80			
1,7000		2	1,000	1.0000	1,000										
1.40			1,000					2000	2000	0000.	20000.	20000	00000.		
1.79					0000.		2000.1	3036.	2000:	1.0000	1.0000	1.0000	1.0600		
1.79 1.0000		٠.	9000.	1.0000	2000.		1.0000	1.0000	1 0000	1000	4				
		.79	1,000	1000	4000										_
									2000.	2000.	1,000	1.0000	1.0000		1.0000

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Table J.12. Performance data for TOW crew: squad leader.

	3.15	6.0000 6.2658 6.3194 6.3194 6.3194 6.3194 6.3194 6.374 6.	63.10	6.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
	2.51	0.0237 0.3498 0.3498 0.3465 0.4231 0.7215 0.7215 0.8229 0.8462 0.	50.12	0.0000 0.2750 0.2750 0.3455 0.3455 0.5100 0.5100 0.5400 0.5450 0.
	2.00 (0.3)	0.05%5 0.4438 0.4438 0.4438 0.4438 0.4438 0.7588 0.7938 0.9106 0.9106 1.0000 1.0000 1.0000 1.0000	39,41	0.1142 0.1142 0.2284 0.2284 0.2867 0.3483 0.5194 0.6484 0.6484 0.6484 0.7504 0.7504 0.7504 0.7504 0.7504 0.7504
	1.5A (0.2)	0.9909 0.3475 0.5307 0.5307 0.5874 0.6857 0.6857 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	31.62 (1.5)	0.0000 0.0000 0.1235 0.2346 0.2346 0.3209 0.3209 0.3209 0.3209 0.3209 0.3209 0.3214 0.5268 0.7129 0.7129 0.7129 0.7129
	1.24	00000000000000000000000000000000000000	25.12	0.0000 0.0750 0.0750 0.0958 0.1188 0.2378 0.2412 0.54412 0.54412 0.54412 0.54412 0.54412 0.54412 0.544112 0.544112 0.544112 0.544112 0.544112 0.6403
(nRs)	1.00	1,467 1,467 1,648 1,648 1,768 1,768 1,760 1,	(HPS) 19.95 (1.3)	0.0000 0.00661 0.00778 0.00778 0.00778 0.00784 0.00784 0.0000 0.0000 0.0000
TIME GRID EIMES	(1.0-1	0.7556 0.7556 0.7556 0.7556 0.7556 0.7556 0.7556 0.7556 0.7556 0.7566 0.		0.0000 0.0548 0.0578 0.0770 0.1627 0.3411 0.3427 0.5427 0.5427 0.5423 0.5423 0.5423 0.5423 0.5423 0.5423 0.5423 0.5423 0.5423 0.5423 0.5524 0.
TIME GRI	0.63 (-0.2)	6.00 6.00	TIME GRJ 12.59 (1.1)	0.0000 0.0051 0.0051 0.11994 0.11994 0.11994 0.1261 0.1684 0.5875 0.5875 0.6875 0.6875 0.985 0.9
	05.0	6 C C C C C C C C C C C C C C C C C C C	10.00	0.000000000000000000000000000000000000
	(-0.40	######################################	(6°0)	C . C C C C C C C C C C C C C C C C C C
	0.32	7 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2		C.C.C.C.C.C.C.C.C.C.C.C.C.C.C.C.C.C.C.
	4.25 (-0.6)		5.01	00000000000000000000000000000000000000
	(-0-7)		3.98 (0.6)	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
Casudinua - Indinuas		44444459444444444444444444444444444444	LOG (DASE)	
וויינ		2515, 24 2515, 24 2515, 24 2515, 24 2515, 25 2515, 25 25 25 25 25 25 25 25 25 25 25 25 25 2	n doe	6 4 5 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6
6810 LTMF		またれる はっぱい はっちょう はっぱい はっぱい はっぱい はっぱい はっぱい はっぱい はっぱい はっぱい	464	

Table J.12. Performance data for TOW crew: squad leader (Concluded).

CRIO LIUF	UUSE	LOG (DOSE)						TIME GR	TIME GRID LINES (HRS)	(HRS)					
			79.43	100.00	125.89	156.49	199.53	251.19		393,11	501.19	40.05	1 65.461	1 00.000	56.93
			(0.1)	(2.0)	(2.1)	(2,2)	(2.3)	(2.4)	(5.5)	(9.5)	(7.5)	(8.8)	(6.5)	(2.9) (3.0) (3.1)	(3.1)
2	4567.93	3.66	0.000			0.000		0.000	0.000	000000	0.0000	0.000	0.000	0.000	0.0000
1.1	3516.24		0.0789		0,000,0	0.000	0.000	0.0000	0.00.0	0.000	0.0000	0.000	0000-4	0.000	0000
2	2729.55		0.5463		_	0.000.0		0.0000	0.000		0.0000	0.000	3070.0	0.0000	0.000
-15	2114.01		0.3758	0.2669	0.1483	0.0744	0.000	0.0000	0.0000	0.000	0.000	0.000	00000	00000	0.000.0
7	1649.76		0.4697		`	0.1514	0.0455	0.0056	0.00.0	000000	0.0000	0.000	0.00.0	000000	0.000
<u>.</u>	17.41.71		0.6640		_	0.2062	0.1528	0.0889	1 < 5 0 . 0	0.0000	0.000	0.0000	0.000	000000	0.000
2	40.146		0.7274		_	0.5279	1557.0	0.2361	0.1440	0.0/68	0.000	000000	0.000.0	0.000	0.000
_	5 C		0.7405		_	0.7262	0.5936	0.5050	0.4117	0.3528	0.3091	0.0461	0000.0	0.000	0000.0
_	7.16		0.7963		•	0.7955	16.7655	0.7160	0.6374	0.5560	0.4417	0.2655	0.2144	0000	0.000
3 r :	7 · ·		P. P. CO.		_	0.7495	0.7574	0.1720	0.7245	0.6206	6042.0	0.4483	0.3973	0.2349	4150.0
3 0 (359.P.		1508.0		_	0.AU45	P 8094	4CO4 0	0.7738	0.6860	0.6395	0.5841	0.5287	0.4520	0.2716
_	12.6/2		0.8167		•	0.A175	A. A312	0.8285	0.6175	0.7581	17377	1207.0	0.6526	0.5090	3.4456
. و	216. AZ		0.8440		•	0.8503	0.8534	0.8546	0.8528	0.8441	0.A358	0.8160	0.7765	0.7061	0.6200
л :	10.9, 40		0.9326		_	5056.0	0.9555	8096°0	0.9658	70/6.0	0.9746	0.9783	0-9850	9819	1.0000
3 :	130.64		0000°		_	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
~	101.03		1.0000		_	1.0000	1.0000	1.0000	1.0003	1.0000	1.0000	1.00.0	1.0000	1.0000	1.0000
~1	18.72		3000		-	1.0000	1.0000	3.0000	1.0000	1.000	1.0000	1.0000	1.0000	0000-1	1.0000
_	11.12		1.0000		-	1.0000	1.0000	1.0000	1.0000	1.0003	1.0000	1.0000	1.0000	1.0000	1.0000

Table J.13. Performance data for TOW crew: gunner.

	0100								TIME GR	IME GRID LINES	(HRS)					
		٠. د د د د د د د د د د د د د د د د د د د	Luciouse	:		:	•	•				•				
				(-0-7)	(4.0-)	(-6.5)	(-0.40	(F)	(-0.2)	ر. ر. ر. و. آ	9.0 0.0 0.0	10.26	1.5A (5.0)	2.60 (0.3)	2.51	3,16
	20	4529.03	•	1.0000	1.0000	4008.0	0.6245	0.4300	4. 46. TO		4	-				
	~	5516.34	٠.	3000	ت	1.000	9.832V	0.7710	0.6532	0.4716	9	•	0.000 0.000	1	1474	
	٥.	2769. K	_	1.0000	c	3.00.	0.9416	0.3582	0.7306		Š	, 7	0.3452	• •	7	1806
	<u> </u>	2 · 1		3000.	•	1.000	Jeor.	0.9062	0.8083		5	٠.	0.4335	350	2.5	
	Z ~	2/******		2000.	•	3000.	0000.	1.0000	0.9489	0.7955	3	್	0.4949	141	3	286
	2	2000		2000		3030	3.000	1.0000	1.0000		0.7419	٠.	0.5621	. 440	3 B	353
	:=	76.97				3000	3030	3030.	0000	1.000	÷		0.7094	\$65°	481	408
	2	537.16	V. 7	2000				3000	00000	0000.	3.000	9.9002	0,7812	0.7510	0.6491	0.5515
	6	103.54	1 2.67	0000		1.000			2000	0000.1	9 6	•	18/8.0		40/	0.6726
	20	34.925	2.56	1.0000	-	0000	. 0	0000			3 3		0000.	900	`. •	1177.0
	_	12.015	54.5	1.0000	_	•	3000	1.0000	1.000			•			֡֓֜֜֜֜֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓	
	. م	716.46	2, 34	1.0000	~	1.0000	1.000	1.0000	1.000	1.000		•				40000
	"	168.74	2.21	1.000	~	1.0000	1.0000	1.0000	1000	0000	0 7 0) =				
	* •	130.64	2.12	1.0000	_	1.0000	1.0000	1.0000	1.0000	3000	000	70001	1.0000	-	3	2000
	1	70.10	2.5	3030.	1.000	1.0000	S	1.0000	1.0000	1.0000	_	, =	1.000	000	9	• •
	u -	`.		•	_	3.000.	3	1.0000	1.000	1.0000	S	3	1.0000	000	1,000	3
	•		7.7	€	_	1.0000	.000.1	1.0000	1.000	1.000	000	•	1.0000	900	3	1.0000
46	0103															
	LTIFE	UOSE	LAGINASE						TIME GR	ID LINES	(HRS)					
			•	5.9A	5.01	6.31	1.94	10,01	12.59		3	,	41.50	19 02	61 03	•
				(0.6)	(10,7)	(n.R)	(6.0)	(0.1)	1.1	2.1.7	(1.3)	(4:1)	(5.1.)	(9:1)	(1.1)	3
	2	4529.03	71	2000.0	=	0,000	9.0000		-	9	9			6		
	1	3516. 44	m	0.1126	٠,	0.0366	0.0478		. =		3 4	•			2000	
	<u>.</u>	<729.55	# M	9.1440	٦.	0.0050	0.0393	•	٠.	2	25.0			0.1200	0.1367	0.1385
	2 :	1	7	1691.0	٦,	0.1145	0.0709	·	٩.	ţ.	950	•		0.1061	5005.0	0.2355
	- M	1276.71	4 141	7072	• •	1547	7070.0	•	٠,	90.	660	•		0.2420	0.2632	0.3449
	2	40.160	. ~1	18/15-0		2001	0.2616	-		- 3	# 1 # 1	•		0.2.0	0.3274	0.4541
	-	700.24	u	0.4746	5.	0. 30 70	3430		. ~	-	7 7 7 7	•			6.475	0.3300
	2 (597.16	~	4578.0	v.	0.4701	0.4390	•		3	5.0			0.5727	0.6816	0.7186
	,	4 0 0 P	70.7	6.555	9.5766	0.5237	0.4692	0.4541	0.4285	0.4247	9075.0	0.4712	0.5061	0.5961	0.7115	0.7351
	>	27.07.6	4 1	0 7 7 0	••	20,27.04	0.7505		₹,	.46	88	•		0.6268	0.7357	0.7519
	و.	216.02	4 4	A > 2 > 2	•	0.50.0	**************************************	9	٠٠	ş.	563	•		0.6655	0.7593	0.7693
	S	15A. 40	• •	0.9426		0.7679	100		5,7	6.5	7	•		0.7625	0.7428	0.7915
	7	トシ・ロデー	•	1.000	٠.	D. Actu	0.8001	0.25	. 5		7 0	•		7.70	C + 0 - 0	10000
	~	101.41	ns.	1.0000	٠.	0.9003	0.8483	0.862	٠,	9	000	•		1000		
	∿ .		_	3000	٦,	1.000	0,9875	0.97A	٣.	0.	0	1.0000	000	1.0000	: 0	1.000
	-	-	-	0000.	ج.	1.0000	1.0000	1.0000	•	90	000	1.0000	000	1.0000	0	1.000

Table J.13. Performance data for TOW crew: gunner (Concluded).

2 = 2	JOUR	LPUCTUOSE						1 181 P	WHID LINES	(SHE)					
				100	125.89	150.49	99.53	61.157	316,23	11,465	501.19		194.53 1	1 00.000	58.93
			(۳۰۱)		(2.1)	(5.2)	(2.3)	(2.4)	(2.5)	(2.6)	(7.7) (2.4)		(6.5)	(1.9) (3.0) (3.1)	(3.1)
9	\$0°625*	•	0,000	0.000		2000	0,000		0.000		0.000	0.000	0.0000	0.000	0.000
-	5°16.74	·	1860.0								0000	0000	0000	0.00.0	0.000
9	6760,53	5.40	0.1600		1,,10.0	0.000	2020.0	0.000	0.000	0.000	0.000	0.000.0	0000-0	0.000	0000.0
<u>.</u>	4119.11		0.7715								0000	0.000	0.000	0.000	0.000
7	1641.72	·	0-00.0								0.000	00000	0.000.0	000000	0.000
~	17.916.11	Ī	0.5323								0.000		0-000	0000	0.000
2	991.04	·	5,6345								7070		0000-0	0.000	0.000
=	700.29	Ī	0.7145								0.2563		0.000	0.000	0.000
2	447.10	•	0.7592								6042.0		0.1620	000000	0.000
5	407.54	Ī	7474 O								0.4584		0.3159	0.2025	9160.0
70	₹29. A∠	•	0.7430								0.5561		0.4519	0.3833	0.2716
-	710.31	•	0.7624								1959.0		0.5676	5550	0.4454
٥	216.AZ	-	621.20								9.7726		0.7221	0.6756	0.6200
5	100.30	•	0.9125								60.9049		9115	0.9466	1,000
7	150.64	Ī	1.000								1.0000		1.0000	1.0000	1,000
~	101.01	•	1.0000								1.0000		1.0000	1.0000	1.0000
Λŧ	18.72		1.0000						•		1,0000		0000	1,0000	1.000
			0000.1								0000		0000		

Table J.14. Performance data for TOW crew: driver.

LOGIDASEJ	0.40 (1.0-)	0.25 (-0.6)	0.52 (2.0-)	0.40	0°20 (-0-3)	11HE 6R3 0.63 (-0.2)	71ME 6RID LINES 0.63 0.79 (-0.2) (-0.1)	(HRS) 1.00 (0.0)	1.24	1.54	2.00 (0.3)	2.51 (0.4)	3.16 (0.5)
				7483033333333333333333333333333333333333	2 1 7 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2						00000000000000000000000000000000000000	00000000000000000000000000000000000000	00000000000000000000000000000000000000
	3.9A	• • •	6.53 (A.6.)	44.7 (9.0)	69.1	11ME 6R2	FINE GRID LINES 12.59 15.85 (1.1) (1.2)		25.12	31.62	39.81 (1.6)	50.12	63.10
	200000000000000000000000000000000000000		CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC	00000000000000000000000000000000000000	0.000000000000000000000000000000000000	CCOCOCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC	11.00000000000000000000000000000000000			00000000000000000000000000000000000000			11.00000000000000000000000000000000000

Table J.14. Performance data for TOW crew: driver (Concluded).

11 an								TIME CR	TIME GRID LIMES (MRS)	(HRS)					
1111	LIBE	LAGCOUSE													
				100.00	175.00	150.47	\$5.661	251,19	516.63	398.11	501.19	96.019	194,53 1	000,000	256.93
			(°.1°)	(0.4)	(3.5)	(4.4)	(2.3)	(2.4)	(7.1) (7.3) (7.3) (7.4) (7.5) (7.6) (7.1) (7.8) (7.9) (3.0) (3.1)	(9.5)	(7,5)	(8.5)	(6.5)	(3.0)	(3.1)
8.	4529.03		0,0000	0,000,0	0.000	0.000	0.0000	00000	0.0000	0.000	0.000	7000	0.000	0.0000	0.000
~	5516.34		0.1012	00000			0.0000		0.000	0.000	0.000	00000	0.000	0.000	0.000
10	27.9.55	5.44	0.3510	0.1702	4.120.0			_	0.000	000000	_	000000	0.000	00000	0000
15	2118.01		0.5324	0.7602		0.00A7			_	0.000	_	0.000.0	0.000.0	0.000	0.000
14	1444.72		1624.0	0.4985			D.0474				_	0.000	0.000	000000	7070 0
- 5	17.4161		0.7143	0.6194							٠	0.0000	0000-0	0000.0	0.000
2	70°166		0.864Z	0.7765								0.000		0.000	0.000
:-	700.24		0.8761	0.8072								0.0510		000000	0.000
2	547.10		0.98.0	0.4978								0.2983		90000	0000
σ	404.54		0.8917	0.8930							0.6515	0.5170		0.2756	0.0914
ဆ	359.AZ		1968.0	376d O								0.6924		6044.0	0.2716
1	210,31		0506.0	0.9050								0.8172		0.6451	0.4450
و.	714.42		6276.0	0.4246								0.9135		0.7552	0.6200
'n	168.20		0.9072	4070.0								0.9928		0.9906	1.000
₹	130.64		1,000	1.0000							_	1.0000		1.0000	1.000
~1	101.11		1.0000	1.0000			_				_	1.0000		1.000	10000
~	18.72		1.0000	1.000c			_	_	1.0000		_	1,0000	1.0000	1.0000	1.000
	61.11		1.0000	1.0000			1.0000	1.0000	1.0000		1.0000	1.0000	1.0000	1,000	1.000
												•			

Table J.15. Performance data for TOW crew: loader.

GR 10 L THF	a	Labelunses						TIME OB	IIME GRIN LIMES	(HRS)					
			0.20	6.0-)	U. 52 (-0.5)	(-0.40	6.50 (-0.4)	6.63 (-0.2)	(1:0-)	1.00	1.26	1.5A (0.2)	2.00	2.51 (0.4)	3.16
97	4569.05	43.4 43.4	0000	1.0000	PUD4.	0.6263	0.4800	6.3635	0.2706	0.1967	•	0.0909	0.0535	10.23	0.000
: 2	27.20.55	3.49	1.000	1,000		1064 °C	1 4 4 4 4 C	0.707.0	404	0.3435	0.2639	•	\$ 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.1638	0.350
<u>.</u> 2∶	2114.A1	5.33	1.0000	1.0000	3000		0.9500	0.8044	0.81.45	0.1019		0.4244	0.3231	0.2470	0.2116
<u> </u>	1641,72	5.47	1.0000	1.0000	1.0000	1.0000	1.0006	0.9640	0.8515	0.777.0		5005.0	0.1740	0.3035	0.2675
2 2	941 04	11.4	C 0	c c	0000	3.000	3000.	0000.	447E.0	0.8402	•	0.5835	0.4347	0.3786	0.32A¢
: =	709.24	7	0000	0000		2000	2000	2000	0000	1125.0	30.00	0.7559	2024.0	0.4662	0.3900
2	547.10	47.7	0.00	_	1000	2000	0000	0000	• •	1.0000	•	0.4112	0.8726	8.224	0.7387
7	163,54	2.b7	1.0000	Ç	1.0000	1.0000	1.0000	900	1.000	1.0000		1.0000	0.9174	0.8563	0. B062
20 (759.A2	2.56	1.0000	_	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	•	•	5446.0	0.9028	0.4630
-	12.016	5**2	1.0000	1.0000	1,0000	1.0000	1.0000	c	1.0000	1.0000	•	000	1.0000	0.9351	6
.	716. RC	6,50	7000.	1.000	1.0000	1.0000	1.0000	_	1.0000	1.0000	•	1.0000	1.0000	1.0000	0.9734
n =	3,04	,,,,	2020.	0000.	3030°	1.000	1.0000	0000	1.0000	Э.	1.0000	0000.	1.0000	1.0000	1.0000
7 4		•	0000		2000	3000.	3000.	ے ت	1.000	1.0000	0	1.0000	1.0000	1.000	1.000
n ^	72 47		000	2020	0000	1.0000	0000	1.0000	1.0000	9	1.0000	0	0000	5	1.0000
<i>,</i>	11 19	67	0000						00000	0000.	000	5 6	000	0000.	0000
•	:	•		•			6000	2000	2000	0000.	_	0000	0000	3	.000
,															
04 th								TIME 6P	IME GRID LINES	(HRS)					
- 114	- 500	L06(005E)	,			•									
			46.4	10.4	0.51	ν6.)	00.01	12,59	15.85	19.45	25.12	31.62	39.81	50.12	63.10
				=	(x.0)	6.0	(0.1.)	= :		1.3)	<u>-</u>	(1.5)	(1.6)	(1.7)	(1.8
9 1	4529,93	3.04	000	•	ď	e,	000000	0.000.0		000000	0.00.0	000000	_	_	0.000
-	3516.34	3.55		•	C	•	0.0250	0.0207	0.0216	4	0.0288	0.0338	0.0459	44	0.0340
2 :	27.29.53	5.40		•	ċ	0.0401	0.0511	0.0271	0.0269	5	0.0400	0.0555	0.0181	3,46	0.1065
2 -	1 x ° x 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1			•	9 0	0.0445	0.0372	0.0333 cc.0333	0.0525	ζ,	0.0526	0.0773	0.1103	147	0.1956
: :	12.4151	7.7				0.115	2000	CCC.0	1/0000	Š	0.030	0.1660	2421.0	2 2	60460
12	40.140	3.00			-	0.1074	0.1529	0.1115	0.1253	: =	0.1600	0.1865	5002.0	5 5	0.5621
=	760.24	۲,43		•	c	0,3155	0.2684	0.2464	0.2687	=	0.3144	0.3381	0.4031	557	0.6495
2 :	91.16	4.18			e.	0.4245	0.3787	0.3535	0.3/01	2	0.4226	0.4525	0.5528	549	0.7361
• .	1 0 0 1 N	79.7			٠,	0.4035	0.4553	0.3987	0.3871		0.4326	0.4685	0.5/70	٤.	0,7577
· ~	2/9/11	7 7 7 7 Y	0.8727	0.01.0	= <	2000	30000	2,427.0	0.44404 0.54404	6.436.5	20.00	9525.0	0.6168	0.7546	3,1795
٥	216.02	Z. 54			c		0.6128	0.6451	0.6867	3	7480	7689	7893	\ =	> ~
S	107.401	4.41			c	۲.	0.7096	0.7446	0.7971	0,8305	0.8675	0.8651	0.8890	. 3	0.9170
₹ '		۲.1۶	1,0000	•	Ċ.	•	O. BURB	0.8441	0.6937	2	σ	0.9819	0.9688	000	
~ ·	101.01	2°01	٥٥٠.	•	216.0	156.	٠.	0.9399	0.9741	000	0	1.0000	_	000	1.0000
u.	7 × 1	C	3000	0000.	3000	0.9928	9	974	٠.	000	0	1.0000	1.0000	1.0000	1.0000
-	11:19	1./,	G O	•	. 0000	3.000	1.000	1.0000	1.0000	1.0000	0000.	0000.	1.0000	0000::	3.000

Table J.15. Performance data for TOW crew: loader (Concluded).

TIME LAID LINES (HRS)

			100.00	125.89	156.49	199.53	251.19	316.21	11.898			794 22 1		10 450
		<u></u>	6.4	1 2.1	(5.5)	(2.3)	(2.4)	(5.5)	(4.6)	(7.5.)	(2.A)	(6.5)	(0.5)	(3,1)
4569.93	3.06	2020.0	3000	e	c	0000	9000		•	4	4:4			
2516.34	5.25	0.0328	0.000.0	ď	•				•		00000	9-00-0	2020.5	9.000
27.49.53	5.44	0.1382	0.55	•	. <			00000		90000	0000	9000	0000	2000.0
7118		1 6 3 6		ě	•	2000	3.00.00	0.00.0	_	0.0000	3000.0	0.0000	0.0000	0.000
	,		100.	5 (-	9000.	3 9 9	3620.3	_	0.000	0.0000	9090.0	0.000.0	0.000
77.00	7.6	0.409	95720	# 0 / 1 · U	0.0756	0.0231	0.0026	0.000	0.000.0	0.000	0000.0	0000	0.000	30000
	2.5	0.4746	7.00.0	ď	_	1050.0	40.0°	6.0165	_	0.0000	0000	9000		
\$0° 1.45	3.00	0.6472	0.5060	Ċ	c	0.22Ab	0.1504	0.070						
709.29	60.2	0.7331	0.7716	C	•	2223			•			9.00.0	00000	90000
597.16	2.78	0 7614	1770	•	: <	70.00	0000	0.3346	_	0.2519	0.0239	0000.0	0.000.0	0000.0
1744				i	•	0.47.0	-	25550	_	0.3505	0.177	0.1544	9090.0	2000.0
				8	=	0.7535	0.7174	2449.0	_	0.4559	0.3537	0.2590	0.1957	0.0914
31.00	£ .	4//	2.7.0	č	c	0.7726	0.7015	0.7145	_	0.5667	0.5184	0.4581	778	0 2218
T 2 . 6 . 7	×**	0.794B	0.7953	ė	c	O. Runa	0. Bu74	0.7651	•	40040	4644	4.4		
216.82	2.34	0.8317	0.8380	e	ح	000	724		. `			2 10 10	2000	0.447
164,70	27.54	0 927	0 9457	•	. <				•	207070	2000	2,1642	101.0	0.6200
130.64	21.0			•	•	2000		1 . 404.	-	0.9744	0.9775	1 695.0	0.9878	1.000
				•	-	0000.	0000.	J.00.	_	1.0000	1.0000	1.0000	1.000	1.0000
			3000	-	-	2000-	10000	3.000		1.0000	1.0000	1.000	1.000	1 0000
14.16	06.1	2000.	3.000.	_	_	1.0000	1.0000	1.0000	_	0000	0000			
11,10	627	1.0000	4.0404	-	•						0000		9000	3000.
	•			•	•	2001.		3000.	_	3000	3000.1	1.0000	1.0000	2000

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                                                                                            ATTN: Nuc Security
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           ATTN: J-22
          ATTN: J-3
                                                                                           Intelligence Ctr. Pacific ATTN: COMIPAC
           ATTN: J-32
           ATTN:
           ATTN:
                    J-634
                                                                                           Interservice Nuc Wpns School
ATTN: TTV
2 cys ATTN: TTV 3416th TTSQ
Defense Industrial Scty Institute
          ATTN: Facilities Protection Dept
                                                                                           Joint Chiefs of Staff

ATTN: ED30, J-3, Strat Ops Div
ATTN: G010, J-5, Nuc & Chem Div
ATTN: J-3, Strat Opns Div
ATTN: J-5, Strat Div, W. McClain
ATTN: JAD/SFD
ATTN: JAD/SSD
Defense Intell Agency
          ATTN: Counterterrorist Threat Branch
ATTN. DB
         ATTN: DB-1, Rsch, Sov Wpn Div, G. Ferrell
ATTN: DB-6, Rsch, Tgt Intell Div, R. Mann
ATTN: DE, Estimates
ATTN: DIA/VPA-2, Fed Res Div
ATTN: ON
                                                                                                      ATTN: JSOA
                                                                                            ATTN: SAGA

3 cys ATTN: J-3, Special Opns
3 cys ATTN: J-5, Nuc Div/Strat Div/FP&P Div
3 cys ATTN: J-5, Plans & Plcy/Nuc Chem Div
           ATTN:
          ATTN: DT, Sci-Tech Intell
ATTN: Ofc of Security
ATTN: CS
           ATTN:
                    0518
                                                                                           Joint Data System Support Ctr
ATTN: C-312
ATTN: C-332
ATTN: C-343
          ATTN: RTS-2B
ATTN: RTS-2C, Tech Svcs & Spt
 5 cys ATTN: DB-4, Rsch, Resources Div
Defense Intell College
          ATTN: DIC/RTS-2
ATTN: DIC-20
                                                                                            Joint Strat Tgt Planning Staff
                                                                                                      ATTN: JLKS
ATTN: JLT
                                                                                                      ATTN: JP
Defense Logistics Agency
                                                                                            ATTN: JPPFO
ATTN: JPTP
2 cys ATTN: JLK, DNA Rep
          ATTN: Command Security Ofc
Defense Nuclear Agency
ATTN: CID
ATTN: NASF
                                                                                           National Defense University
ATTN: ICAF, Tech Lib
ATTN: NWCLB-CR
ATTN: Stop 315, Library
          ATTN: NATE
                    UAIS
RAEE
           ATIN:
                                                                                                      ATTN: Strat Concepts Div Ctr
           ATTN:
           ATTN:
                    STNA
                                                                                           National Security Agency
ATTN: A12, F. Newton
ATTN: Chief, A Group
           ATTN:
                     STRA
           ATTN:
                    STSP
 2 cys ATTN:
4 cys ATTN:
                    OAOP
                    STTI-CA
```

216 CYS ATTN: OPNS

DEPARTMENT OF DEFENSE (Continued) Ofc of the Sec of Def, Net Assessments ATTN: Doc Control Program Analysis & Evaluation ATTN: Naval Forces 2 cys ATTN: Regional Programs 2 cys ATTN: Strategic Programs

US	Eur	opean (Command
		ATTN:	ECJ-LW
		ATTN:	ECJ-2
		ATTN:	ECJ-2-ITD
		ATTN:	ECJ-3
		ATTN:	ECJ-5
		ATTN:	ECJ5-N, Nuc Div
		ATTN:	ECJ-6
		ATTN:	ECJ2-T, Tgts Div
		ATTN:	ECCS/SASM
2	cys	ATTN:	ECJ-7 LW

US	National	Mil	Representa	tive,	SHAPE
	ATTN:	: US	Documents	Offic	cer

Under	Sec o	f Def	for	Policy
	ATTN	l: DU	SP/P	
	ATTN	1: 115	D/P	

Under Secy of	Def for Rsch & Engrg
ATTN:	Tactical Warfare Prog
ATTN:	Chairman, Def Sci Brd
ATTN:	Strat & Space Sys (OS)

ATTM: Strat & Theater Nuc Forces, F. Vajda 2 cys ATTM: C31

10 cys ATTN: Chairman, PSEAG

DEPARTMENT OF THE ARMY

Army Research Institute ATTN: Commander

EMD Program Office ATTN: DACS-BM, J. Kahlas, 13101

Combat Material Eval Element ATTN: Security Analyst

Dep Ch of Staff for Ops & Plans ATTN: DAMO-NC, Nuc Chem Dir ATTN: DAMO-NCN ATTN: DAMO-ROS

ATTN: DAMO-NCN ATTN: DAMO-RQS ATTN: DAMO-ZXA

Dep Ch of Staff for Rsch, Dev & Acq ATTN: DAMA-CSS-N

Dept of the Army
ATTN: DAMA-CSS-N
ATTN: DAMI-CI
ATTN: DAMO-NCZ
ATTN: DAMO-OD
ATTN: DAMO-ODSO
3 cys ATTN: DAPE-HRE

Eighth US Army ATTN: CJ-POX-NS

Harry Diamond Laboratories
ATTN: DELHD-NW-P
ATTN: DELHD-TA-L, 81100, Tech Lib

DEPARTMENT OF THE ARMY (Continued)

Joint Strategic Opns Ctr 2 cys ATTN: J-2 2 cys ATTN: J-5

Military Traffic Mgt Command
ATTN: Ofc of Security & Safety

Seneca Army Depot
ATTN: Provost Marshal
ATTN: SDSSE-P0
ATTN: Surety

Sierra Army Depot ATTN: Security Opns

Southern European Task Force ATTN: AESE-GCT-S

US Army Air Defense School ATTN: Commandant

US Army Armament Rsch Dev & Cmd 2 cys ATTN: DRDAR-LCN-F

US Army Armor School
ATTN: ATSB-CTD
ATTN: Tech Library

US Army Ball'stic Research Lab
ATTN: AMXBR-VLD. Dr. Klopcic
ATTN: DRDAR-BL
ATIN: DRDAR-BLA-S, Tech Lib
ATTN: DRDAR-BLT
ATTN: DRDAR-BLV-R, Dr. Rainis

US Army Delvoir R&D Ctr ATTN: DRCPM-PSE

US Army Comb Arms Combat Dev Acty ATTN: ATZL-CAP

US Army Comd & General Staff College ATTN: Acq Library Div ATTN: ATSW-TA-D ATTN: ATZL-SWJ-CA ATTN: ATZL-SWS-L. D. Dorris

US Army Concepts Analysis Agency ATTN: CSSA-ADL, Tech Lib

US Army Corps of Engineers
ATTN: Security & Law Enforcement

US Army Criminal Investigation Cmd ATTN: Commander

US Army Elct Warfare Lab ATTN: DELEW-I-S

US Army Electronic Proving Ground ATTN: STEEP-PA-I

US Army Europe & Seventh Army
ATTN: AEACC-ND
ATTN: AEAGC
ATTN: Provost Marshal
2 cys ATTN: AEAGD-MM-SW
2 cys ATTN: AEAPM-PS
2 cys ATTN: DCS1
2 cys ATTN: DCSOPS

DEPARTMENT OF THE ARMY (Continued)

US Army Field Artillery School ATTN: ATSF-CD

US Army Forces Command ATTN: AF-OPTS

US Army Human Engineering Lab ATTN. Director

US Army Infantry Ctr & Sch ATTN: ATSH-CD-CSO

US Army Intel Threat Analysis Det 2 cys ATTN: IAX-Z

US Army Intelligence Agency
ATTN: DELEW-I

US Army Material Cmd 2 cys ATTN: DRCPM-NUC

US Army Material Command
ATTN: DRCDE-D
2 cys ATTN: DRCNC
2 cys ATTN: DRCSS

US Army Materiel Sys Analysis Actvy ATTN: DRXSY-DS ATTN: DRXSY-S

US Army Military Police School
2 cys ATTN: ATZN-MP-Library
2 cys ATTN: ATZN-MP-TD
2 cys ATTN: Commandant
2 cys ATTN: Phys Scty Committee

US Army Nuc & Chem Agency ATTN: Library

US Army TRACOC Sys Analysis Actvy
ATTN: ATAA-TAC

US Army Training & Doctrine Command
ATTN: ATCD-AO
ATTN: ATCD-FA
ATTN: ATCD-N, Cbt Dev, Nuc Dir
ATTN: ATOD-NCO

US Army War College ATTN: Library 2 cys ATTN: Strategic Studies

US Military Academy
ATTN: Dept of Behavorial Sci & Leadership
ATTN: Dir Natl Security Studies
ATTN: Dir of Libraries

ilitary Academy

USA Military Academy ATTN: Doc Library USA Missile Command

ATTN: DRSMI-XF

USA Nuclear Biological & Chemical School ATTN: Library

V Corps
ATTN: Commander
ATTN: G-3

DEPARTMENT OF THE ARMY (Continued)

VII Corps

ATTN: G-3

1st Special Operations Cmd ATTN: AFVS-GC-O, Maj Ogden

59th Ordnance Brigade ATTN: AEUSA-Z ATTN: Surety

DEPARTMENT OF THE NAVY

Carrier Airborne Early Warning Wing 12
ATTN: Commander

Carrier Group 1 ATTN: Commander

Carrier Group 2 ATTN: Commander

Carrier Group 3
ATTN: Commander

Carrier Group 4
ATTN: Commander

Carrier Group 5
ATTN: Commander

Carrier Group 6
ATTN: Commander

Carrier Group 7
ATTN: Commander

Carrier Group 8 ATTN: Commander

Cruiser-Destroyer Group One ATTN: Commander

Cruiser-Destroyer Group 12 ATTN: Commander

Cruiser-Destroyer Group 2 ATTN: Commander

Cruiser-Destroyer Group 3
ATTN: Commander

Cruiser-Destroyer Group 5
ATTN: Commander

Cruiser-Destroyer Group 8
ATTN: Commander

David Taylor Naval Ship R&D Ctr ATTN: Code 174

Fighter Airborne Early Warning Wing, US Pacific Fleet ATTN: Commander

Fighter Wing 1 ATTN: Commander

Fleet Intelligence Center, Pacific ATTN: FICPAC, Code 21

DEPARTMENT OF THE NAVY (Continued)

Fleet Intelligence Ctr, Europe & Atlantic ATTN: Library

Naval Material Command

ATTN: MAT 0433 ATTN: MAT-0462 ATTN: PM-23

Light Attack Wing, US Pacific Fleet

ATTN: Commander

Light Attack Wing 1 ATTN: Commander

Marine Corps

ATTN: Code PPO

Marine Corps Dev & Education Command ATTN: Commander

Megium Attack Tactical Electronic Warfare Wing

US Pacific Fleet

ATTN: Commander

Medium Attack Wing 1 ATTN: Commander

Naval Air Force, US Atlantic Fleet ATTN: Commander

Naval Air Force, US Pacific Fleet

ATTN: Commander

Naval Electronic Sys Engineering Center

ATTN: Code 04 ATTN: Code 404HS

Naval Facilities Engineering Command

ATTN: Code 032E

Naval Intelligence Support Ctr

ATTN: NISC-30

Naval Investigative Svcs

ATTN: NISHC-22A ATTN: NOP-009D ATTN: 009/NIS/243

Naval Ocean Systems Center ATTN: Code 4471, Tech Lib

Naval Personnel Res & Dev Ctr ATTN: Code P302

Naval Po iraduate School ATin: Code 1424, Library

Naval Research Laboratory

ATTN: Code 1240 ATTN: Code 2627, Tech Lib

Naval Sea Systems Command ATTN: .SEA-09G53, Lib ATTN: SEA-643

Naval Surface Force, US Atlantic Fleet

ATTN: Commander

Naval Surface Force, US Pacific Fleet ATTN: Commander

DEPARTMENT OF THE NAVY (Continued)

Naval Surfuce Weapons Center

ATTN: Code F31 ATTN: G, G00

Naval War College

ATTN: Code E-11, Tech Svc ATTN: Ctr for Nav Warfare Studies

ATTN: Doc Control

ATTN: Library ATTN: Strategy Dept

Naval Weapons Evaluation Facility

ATTN: Tech Director

Nuc Wpns Tng Group, Atlantic

ATTN: Code 222 ATTN: Doc Control

Nuclear Weapons Tng Group, Pacific ATTN: Code 32 ATTN: Doc Control

Ofc of the Dep Ch of Naval Ops

ATTN: NIS-22

ATTN: NOP CC9D
ATTN: NOP CC9D3
ATTN: NOP C6D
ATTN: NOP C6D
ATTN: NOP 50, Avn Plns & Rqmts Dev

NOP 60 NOP 60D ATTN:

ATTN:

NOP 603 ATTN:

ATIN: NOP 654, Strat Eval & Analysis Br

ATTN: NOP 91 ATTN: NOP 955, AAW Div

ATTN: NOP 981 2 cys ATTN: NOP 403

Ofc of Naval Research

ATTN: Code 713

CNO Exec Panel, Ofc of the Ch of Naval Opns

ATTN: OP-OOK

Operational Test & Eval Force

ATTN: Commander

Operational Test & Eval Force, Pacific

ATTN: Dep Commander

Dep Ch of Staff, Plans, Policy & Opns ATTN: Code-P ATTN: Code-POC-30

Space & Naval Warfare Systems Cmd ATTN: PME 121-3

Strategic Systems Programs, PM-1 AITN: Code SP113

Submarine Force, US Atlantic Fleet ATTN: Commander

Submarine Force, US Pacific Fleet

ATTN: Commander

Submarine Group 2

ATTN: Commander

Submarine Group 5

ATTN: Commander

DEPARTMENT OF THE NAVY (Continued)

Submarine Group 6 ATTN: Commander

Submarine Group 7 ATTN: Commander

Submarine Group 8 ATTN: Commander

Submarine Group 9 ATTN: Commander

Tactical Ing Gp, Pacific ATTN: Commander

Tactical Wings Atlantic ATTN: Commander

Commander in Chief, US Atlantic Fleet

ATTN: J2 ATTN: Physical Security ATTN: Flans & Operations

Commander in Chief, US Naval Forces, Europe ATTN: N54. Nuc Warfare Officer ATTN: Special Opns

US Navy Second Fleet ATTi: Commander

US Navy Seventh Fleet ATTN: Commander

US Navy Sixth Fleet ATTN: Commander

US Navy Third Fleet ATTN: Commander

Commander in Chief, US Pacific Fleet ATTN: J-2 ATTN: Physical Security ATTN: Plans & Opns

DEPARTMENT OF THE AIR FORCE

Aeronautical Systems Division ATTN: XRO/MAF

Air Force ATTN: INA

Air Force ATIN: INT

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Air Force Logistics Command ATTN: Security Police

Air Force Ofc of Special Investigations ATTN: IVS

Air Force Office of Security Police 2 cys ATTN: AFOSP/SPPC 2 cys ATTN: AFOSP/SPPX 2 cys ATTN: SPOS-SPPC

Air Force Systems Command

ATTH: DI

ATTH: SU

ATTH: Security Police

TTH: Ge

DEPARTMENT OF THE AIR FORCE (Continued)

Air Force Weapons Laboratory ATTN: SUL

Air Training Command ATTN: Security Police

Air University

ATTN: AU/SP ATTN: Strategic Studies

Air University Library ATTN: AUL-LSF ATTN: Library

Assist Ch of Staff, Studies & Analysi: 2 cys ATTN: AF/SAMI, Tech Info Div

Assist Ch of the Air Force, Rsch, Dev & Logistics ATTN: SAF/ALR

Dep Ch of Staff, Rsch, Dev & Acq ATTN: AF/RDOI

Den Ch of Staff, Plans & Opns ATTN: AFXOOIR
ATTN: AFXOXFG, Plns, Frc Dev Mun Plns
ATTN: AFXOXFS, Frc Dev, Strat Off Frc

Electronic Systems Division 3 cys ATTN: Physical Security Sys Directorate

Foreign Technology Division

ATIN: CCN ATIN: SDN ATIN: TQTM

Military Airlift Command ATTN: Security Police

Commander in Chief, Pacific Air Forces ATTN: Security Police ATTN: XP

Space Command ATTN: Security Police

Space Division ATTN: YH, DSCS III

Strategic Air Command ATTN: Security Police ATTN: ADWN ATTN: NRI/STINFO ATTN: SPD ATTN: STIC, 544SIW ATTN: XOXO ATTN: XPQ

Tactical Air Command ATTN: Security Police ATTN: TAC/XPJ

ATTN: XPZ

ATTN: TAC/XPS

US Air Force Academy ATTN: Library ATTN: Strategic Studies ATTH: USALA/SP

on, Air Force in Europe 2 CAS ATTA: SAME/SE

DEPARTMENT OF THE AIR FORCE (Continued)

US Air Force Inspector General

3 cys ATTN: ICS 3 cys ATTN: IGT

US Air Forces in Europe ATTN: USAFE/DEX

ATTN: USAFE/DOT ATTN: USAFE/INAT ATTN: USAFE/XPX, Plns

USAF School of Aerospace Medicine ATTN: Radiation Sciences Div

USAF Special Operations School ATTN: Director

1st ACCS

ATTN: DOF

2nd ACCS

ATTN: Doc

3280th Tech Training Sq ATTN: TG1CC

DEPARTMENT OF ENERGY

Department of Energy Albuquerque Operations Office ATTN: CTID ATTN: D. Richmond

Department of Energy Office of Mil Application, GTN ATTN: OMA, DP-22

Department of Energy, GTN ATTN: Ofc of Intelligence ATTN: OMA, DP-22

ATTN: Safeguards & Security ATTN: Tech & Intell Dir

University of California, Lawrence Livermore Natl Lab

ATTN: L-35 ATTN: L-38

ATTN: L-389 ATTN: L-450, W. Hogan

ATTN: Tech Info Dept Lib ATTN: Z Division Library

Los Alamos National Laboratory

ATTN: M/S634, T. Dowler ATTN: MS P364, Reports Library

ATTN: R. Sandoval

Sandia National Laboratories ATTN: Tech Lib, 3141 ATTN: 0333, R. Stratton ATTN: 0334, J. Struve

OTHER GOVERNMENT AGENCIES

Bureau of Allohol, Tobacco & Firearms ATTN: Chief Special Opns Div

US Dept of State, Bureau of Politico Mil Affairs ATTN: PM/STM

Committee on Armed Services ATTN: Staff Dir & Chief Counsel

OTHER GOVERNMENT AGENCIES (Continued)

Central Intell Agency

ATTN: Counter-Terrorist Group

ATTN: Dir of Security ATTN: Medical Svcs

ATTN: NIO-T

ATTN: NIO, Strategic Sys ATTN: Ofc of Global Issues ATTN: R&D Sub Committee Security Committee ATTN:

ATTN: Tech Library

Federal Aviation Admin

ATTN: Dir of Civil Aviation Security

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Federal Bureau of Invest Academy ATTN: Behavioral Rsch Unit 2 cys ATTN: Library

Federal Bureau of Investigation 3 cys ATTN: Terrorist Rsch & Analytical Ctr

Federal Emergency Management Agency

ATTN: Asst Assoc Dir for Rsch, J. Kerr ATTN: Civil Security Division ATTN: G. Orrell, MP-CP

ATTN: Ofc of Rsch/NP, D. Benson

General Sycs Administration ATTN: PS

House Perm Select Committ on Intell ATTN: Staif Director

Interpol, US Natl Central Bureau ATTN: Chief

Metro Transit Police ATTN: Chief

National Bureau of Standards ATTN: Law Enforcement

Dept of Commerce, Natl Bureau of Standards ATTN: Tech A219

Natl Criminal Justice Reference Svc 2 cys ATTN: D. Galarraga Select Committee on Intelligence ATTN: Staff Director

Subcommittee on Sec & Terrorism ATTN: Chief Counsel, Staff Dir

US Capitol Police ATTN: Chief

US Coast Guard ATTN: Port & Environment Safety

US Coast Guard Academy ATTN: Library

US Dept of State

ATTN: A/SY/CC/TAG ATTN: A/SY/DASS ATTN: A/SY/OP/T

ATTN: FAIM/LR ATTN: M/MED 2 cys ATTN: M/CTP

OTHER GOVERNMENT AGENCIES (Continued)

US Nuclear Regulatory Commission
ATTN: Dir Div of Saveguards
ATTN: Ofc of Insp & Enforcement

US Park Police

ATIN: Chief of Police

DEPARTMENT OF DELENSE CONTRACTORS

Advanced International Studies Institute ATTN: M. Harvey

Advanced Rsch & Applications Corp ATTN: Dcc Control

Aerospace Corp ATTN: Library

Analytical Assessments Corp ATTN: A. Wagner

BOM Corp

ATTN: C. Wasaff

ATTN: J. Code

ATTN: J. Braddock

ATTN: J. Conant

ATTN: R. Buchanar.

Boeing Co

ATTN: MS-85-20, D. Choate

ATTN: MS-85-20, J. Russel

Computer Sciences Corp ATTN: F. Eisenbarth

Data Memory Systems, Inc. ATTN: T. Dupuy

Grumman-CTEC, Inc

Horizons Technology, Inc ATTN: J. Palmer

ATIN: S. Shrier

IIT Research Institute ATTN: Doc Library

Institute for Defense Analyses ATTN: Classified ibrary ATTN: J. Grote

IRT Corp

ATTN: W. Macklin

JAYCOR

ATTN: R. Sullivan

Kaman Sciences Corp ATTN: F. Shelton

Kaman Sciences Corp ATTN: E. Conrad ATTN: E. Daugs

Kaman (empo

ATTN: DASIAC

Kaman Tempo ATTN: DASIAC

DEPARTMENT OF DIFENSE CONTRACTORS (Continued)

Martin Marietta Corp ATTN: F. Marion

Martin Marietta Denver Aerospace ATTN: J. Donathan

National Institute for Public Policy ATTN: C Gray

Orion Research Inc ATTN: J. Scholz

Pacific-Sierra Research Corp ATTN: H. Brode, Chairman SAGE 2 cys ATTN: G. Anno

2 cys ATTN: D. Wilson 2 cys ATTN: M. Dore

Pacific-Sierra Research Corp ATTN: D. Gormley

R&D Associates

ATTN: C. Lee

ATTN: C. Knowles
ATTN: D. Simons

ATTN: E. Carson

ATTN: F. Field

ATTN: P. Haas

2 cys ATTN: Doc Control

R&D Associates

ATIN: A. Deverill ATIN: J. Thompson

ATTN: K. Moran ATTN: W. Graham

Ranc Corp

ATTN: P. Davis

ATTN: V. Jackson 2 cys ATTN: Security & Subnation Conflict

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Rand Corp

ATTN: B. Bennett

Rockwell International Corp ATTN: J. Howe

S-CUBED

ATTN: K. Pyatt

Science Applications Intl Corp ATIN: Document Control

ATTN: E. Swick ATTN: J. Beyster

ATTN: J. Martin

ATTN: J. Warner

ATTN: M. Drake

Science Applications Intl Corp

ATTN: B. Bennett

ATTN: Document Control

ATTN: J. Foster

ATTN: J. Peters

J. Shannon ATTN:

ATTN: L. Goure ATTN: M. Fineberg

ATTN: W. Layson

Science Applications Intl Corp

ATTN: D. Kaul

DEPARTMENT OF DEFENSE CONTRACTORS (Continued)

Science Applications, Inc ATTN: R. Craver

SRI International AITN: R. Tidwell

SRI International ATTN: C. Eulburt

Systems Research & Applications Corp ATTN: S. Greenstein

DEPARTMENT OF DEFENSE CONTRACTORS (Continued)

Tetra Tech, Inc ATTN: F. Bothwell

TRW Electronics & Defense Sector ATTN: D. Scally ATTN: N. Lipner ATTN: R. Burnett

TRW Electronics & Defense Sector ATTN: P. Dai